# Scheduling and Cost Estimation of Underground Work in Hydroelectric Project 

## A Thesis

Submitted in partial fulfilment of the requirements for the award of the degree of

## MASTER OF TECHNOLOGY

IN
CIVIL ENGINEERING
With specialization in
CONSTRUCTION MANAGEMENT
Under the supervision of

Mr. Santu Kar<br>(Assistant Professor)

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HIMACHAL PRADESH, INDIA
May, 2017

## CERTIFICATE

This is to certify that the work which is being presented in the project title "Scheduling and Cost Estimation of Undergroun work in Hydroelectric Project" in partial fulfilment of the requirements for the award of the degree of Master of technology in Civil Engineering with specialization in "Construction Management" and submitted to the Department of Civil Engineering, Jaypee University of Information Technology, Waknaghat is an authentic record of work carried out by Irshad Ahmad(Enrollment no. 152601) M.Tech Construction Management during a period from July 2016 to May 2017 under the supervision of Mr. Santu Kar Assistant Professor, Civil Engineering Department, Jaypee University of Information Technology, Waknaghat.

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## ACKNOWLEDGEMENT

I extend my heartily gratitude to my Project Guide Mr. Santu Kar for his constant guidance and support in pursuit of this Project. He has been a true motivation throughout and helped me in exploring various horizons of this project. Without his guidance, this project wouldn't have been possible. I would also like to thank my colleagues for their co-operation in framing the project.

Also I would like to convey my due gratitude and thanks to Dr. Ashok Kumar Gupta, H.O.D Civil Engineering Dept. for providing us the opportunity and infrastructure required to work on this project. Moreover, his constant vigilance over the progress of project work helped us in rendering sincere efforts to the task.

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## ABBREVIATIONS

RHP Ratle Hydroelectric Project
HE Hydroelectric Energy
DT Diversion Tunnel
PS Pressure Shaft
TRT Tailrace Tunnel
TBM Tunnel Boaring Machine


#### Abstract

The construction of tunnel is important for different purposes. They can be constructed for railways, roadways, pedestrian footways and can be built in hard rock, soft ground, river bed and are also used to convey Hydro electric power, water stream, or as a sewer. The construction of Diversion Tunnel, Pressure Shaft, and Tailrace Tunnel to convey water is considered in this project. To identify different activities and their cycle time is calculated. Scheduling for different activity is carried out with the help of Primavera Software which is shown at result page. Cost Estimation in Diversion Tunnel, Pressure Shaft, and Tailrace Tunnel is also calculated.

Excavation in heading and benching, Rock bolt support work, lining work is considered for cycle time and cost estimation calculation in DT, PS, and TRT. Excavation is carried out by two methods drill and blast method, and by Roadheader. Cost estimation is also carried out by two methods. The comparison of two methods adopted for excavation work and cost estimation has been carried out


Keywords: Heading, Benching, Cycle time, Lining, Rock Bolts, Diversion Tunnel, Pressure Shaft, Tailrace Tunnel.

## CHAPTER 1

## INTRODUCTION

### 1.1 General

The proposed Ratle Hydroelectric Project, in Kishtwar tehsil of Doda District of Jammu and Kashmir, is located downstream of the Dulhsti power house which is in advance stage of construction on Chenab river as identified by Central Electricity Authority in their ranking studies. The Chenab River originates at Chandra flows westerly till it meets Bichlari on the right bank and flows continuously up to Akhnoor travels 584 Km and experience total drop of 5430 m . The project envisages harnessing the hydro-power potential of the river from EL 1000 m to EL 887 m . A concrete gravity dam is proposed across the river just downstream of the Ratle village (Latitude $33014^{\prime} 50.15^{\prime \prime} \mathrm{N}$, Longitude $75046^{\prime} 47.17^{\prime \prime} \mathrm{E}$ ) and an underground power house with an installed capacity of 4X140 MW is proposed near Juddi village (Latitude $33009^{\prime} 02^{\prime \prime}$ N, Longitude 75045 ' $00^{\prime \prime}$ E) both in Doda District. The scheme will generate 2483.37 GHz in a $90 \%$ dependable year and 2614.38 GHz in a $50 \%$ dependable year. The tariff from the project at present day cost would be Rs. $1.22 /-\mathrm{KWh}$ (Levelised) The nearest rail head to the project site is Jammu which is about 260 km from dam site is 15 Km South West of Kishtwar. Kishtwar is a important tehsil head quarter of Doda district of Jammu Province and is connected to Jammu (and Srinagar) via Batote an important place on Jammu Srinagar National Highway 1A.

Two nos. of Diversion Tunnel has to be constructed in order to divert the Chenab river water flow during Dam construction. Diversion Tunnels are having 11.0 m finished diameter circular shaped with the slope of 1:94 for DT-1 and 1:102 for DT-2. Invert bottom finished levels at Inlet and Outlet portals are EL926 and EL921 respectively for both the tunnels. Construction work for Diversion tunnels has to be carried out from Inlet and Outlet ends. Diversion Tunnel works includes excavation by conventional method like drilling and blasting or by Roadheader or as directed by Engineer In-charge.

Diversion tunnels are common in the construction of dams. When a dam is built, a tunnel is bored in order to divert water away from the dam construction site so that it essentially bypasses it, hence the term diversion tunnel.

### 1.2 Need of the study of project

1. The need of the study of project is to identify different activities of hydroelectric project construction work in a proper sequence from start to finish work.
2. To be able to have a clear understanding and knowledge of hydroelectric project construction activities in a sequential order.
3. Study of different component in hydroelectric project.

### 1.3 Objective of the project

1. To find out different activities involved and to prepare construction schedule of different underground structures of the Hydroelectric project using drill blast method and mechanical excavation method.
2. To estimate the cost of underground work in hydroelectric project. The excavation in DT, PS, and TRT as well as estimation of cost has been carried out and their comparison in excavation as well as in cost is done.
3. To compare the excavation method by drill \& blast and mechanical excavation as well in their cost.

### 1.4 Project methodology

The first step of the research consists of gathering information about activities and resources used in tunnelling construction. This is mainly done by means of a literature study. In order to identify the main variables of tunnelling construction a deterministic model is constructed. The deterministic model is used to help to understand the processes involved in tunnelling construction, and identify the model variables for which information needs to be collected data about model parameters, probability distributions of time durations of activities, resources and the relationships between model's parameters are examined.

The last step analysing the results. A sensitivity analysis is carried out on real tunnelling case studies, to identify and analyse the most critical tunnelling variables affecting
productivity of tunnelling construction processes. Critical variables are the variables that have major impact on productivity (and cost) of tunnelling construction. On the basis of the results produced, the 'best' excavation method regarding a real tunnelling project is determined also, a comparison will be made between the road header and drill and blast excavation methods. These analyses are done based on productivity (in terms of tunnel advance rate) and cost.

The project methodology described can be graphically represented as shown


Fig 1.1 Project methodology

## CHAPTER 2

## LITERATURE REVIEW

### 2.1 General

From the extensive literature study, it can be observed that the about $26 \%$ of energy is contributed by hydropower to India. For India, the total capacity is more than 2 Lakh MW and so holds the 5 th position for electricity generation in the world

### 2.2 Hydro power plants

Hydro power can be classified as: large hydro power, medium hydro power, Small hydro Power. These are classified according to the power generation capacity.

Large hydro power > 100 MW
Medium hydro power: 30-100 MW
Small hydro power: 1-30MW

### 2.3 Mechanism

The water is stored behind a dam. This reservoir is located very high as, "height of a reservoir decide the force of water flowing to the turbine. Since the height increase the potential energy of water at the reservoir also increase. The gate controls the water flowing into the plants. Depending on the load demand the water is allowed into the turbine. The water flowing from the control gate has both potential and kinetic energy. The water flow through to the turbine through the penstock which is designed to transport water from intake to turbine without any cavitations problem. The water further increases in the penstock due to the height. The height of water at the water reservoir and amount of water into the penstock determine the total power generation by a hydro plant. Then water then allowed into the turbine generator unit. The water strikes the blade of the turbine and the potential and kinetic energy of water is converted to the rotational energy which drives the blades of the turbine. The shaft of the turbine which is enclosed inside a generator start to rotate due to the rotating blades. This rotating shaft produces alternating current in the coils of the generator. This rotating shaft inside the generation is responsible for the production of magnetic field which is further converted to the
electrical energy by electromagnetic field mechanism. Thus shaft connecting the turbine and generator plays a vital role here. Thus, hydroelectric power plants produce electricity from the energy of water. This electric is the transfer to the grid".

### 2.4 Processes of tunnel construction

Before a tunnelling construction project can be analysed. It is important to define the tunnelling system. Decisions have to be made, "concerning the modality of excavation (e.g. drill and blast, road-header), the material handling process, and the tunnel support system. In this chapter the various activities related to the tunnelling construction process will be explored. The purpose of this literature study is to get a general overview of the different construction processes involved in tunnelling, and the interaction of the various processes in the context of tunnelling construction.

In the first paragraph the focus will be on the main excavation methods, namely drill and blast, and road-header".

### 2.5 Excavation methods

At present, "drill and blast and TBM tunnelling can be considered the most common excavation methods used in tunnelling. One of the differences between the use of TBM or drill and blast is that the performance (rate of advance) for drill and blast is lower in most cases. The total labour cost using drill and blast-method is higher, but the investment cost is lower than TBM technology (relatively low capital cost for equipment). According to Girmscheid and Schexnayder, drill and blast technology is cost efficient when the length of the tunnel to be excavated is less than three kilometres. The cost efficiency decreases as tunnel length increases. Comparing both methods there are also other significant differences. Tunnel excavation using TBM requires a predetermined tunnel diameter, which can be excavated accurately. Using drill and blast the cross section can be created to any shape".

### 2.5.1 Drill and blast method

The drill and blast process is a cyclic operation; each round consists of four successive operations, namely: drill, blast, muck and installation of primary support. The drilling operation consists of, "drilling a series of small blast holes in the tunnel face, by a so called "drill jumbo". The number of holes and location are dependent of the type and condition of the rock, the type of explosive and the blasting technique used. After all the required holes are drilled, they will be loaded with explosives. Once the explosives are loaded in the blast holes, the tunnel face is cleared and the explosives are detonated.

Tunnelling construction involves three main processes, namely excavation, dirt removal and tunnel support. The construction of a tunnel (using TBM) begins with the excavation and liner support of the vertical shaft".

### 2.5.2 Roadheader

Road-header machines (partial-face tunneling machine) were," initially developed for the coal mining industry, but are increasingly being used in rock tunneling. The machine consists of a rotating cutting head mounted at the end of the boom to a crawler frame. This crawler frame contains a power system, a muck gathering system, and a conveyor that transports the muck to the back of the machine. The muck is then loaded into the muck handling system and hauled out of the tunnel. Road-headers can achieve a better advance rate than the drill and blast-method, but significant lower than the tunnel boring machine. The advantages of this method are similar to the TBM method, such as continuous operation, limited non-productive time, and quality of the tunnel opening. However, road-headers are more flexible than the tunnel boring machine, because they can be applied to various types, shapes, and sizes of underground excavation Tunneling construction using road-headers involves three main processes, namely: excavation, dirt removal and tunnel support. Excavation is done using road-header for a certain amount of time. In order to start the next process the road-header is pulled back. The removal of dirt from the face of the tunnel can be done by using a conveyor belt, trucks or trains. After
the road-header has excavated for a certain amount of time it gets pulled back, so that scaling and the installation of mechanical bolts can start. Subsequently installation of initial support is done. This operation involves installation of wire mesh or shotcrete at their designed location

The main difference between conventional mechanized drill and blast was given by G.germchied (2002) and TBM tunneling is related to the process cycle and operational continuity. A TBM drive requires a predetermined fixed tunnel diameter. Such a circular profile can be excavated with a high degree of accuracy by the TBM. However, with drill and blast methods the tunnel cross section can be created to any required shape and, most importantly, the tunnel shape can be changed along the length of the drive. The diameter of a circular cross section can be increased or decreased as required, or a circular section can be changed to a horseshoe form when necessary. However, in the most unfavorable drill and blast case, there can be blasting over break amounting to $10-25 \%$ of the design cross-sectional area. This material must be removed and the space may possibility have to be refilled. With drill and blast, considerably more temporary ground support work must be undertaken at the face and in the excavation area than is usually the case for a TBM excavation".

### 2.6 Drilling technology

For achieving the, "required tunnel section and for optimal fragmentation of the rock, accurate drilling is an important prerequisite. Drilling critically impacts blast performance. The drilling cycle includes the positioning of the jumbo, checking that the proper drilling pattern is employed to match the position along the tunnel length station location, positioning the drilling arms booms, and drilling the holes. The latest generation of jumbo drills with two or three booms can attain high production in semi or fully automatic robotic operation. The positioning of the drill jumbo is accomplished manually by means of a tunnel laser, but the drilling pattern for the appropriate location is produced via computer-aided design to the jumbo's process control computer. On the basis of the jumbo positioning data, the on-board computer calculates the positions for the drilling
booms and the specific drill pattern horizontal, angle, depth, and spacing. This can all be done in either a semi or fully automatic mode".

### 2.7 Blast technology

Three factors influence developments in, "tunnel blasting technology safe handling of explosives reduction of accidental detonation risk reduction in toxicity post blast gases, nitrous oxides, and carbon monoxide and rapid and straightforward loading/charging of the bore holes".

### 2.8 Mucking technology

Mucking denotes the gathering together of, "material from where it has been deposited after the blast. The size of the individual rock fragments and the volume excavated per length of advance are essential criteria for selecting a mucking process. Muck haulage can be undertaken via mucking trains, belt conveyors, or dumpers".

### 2.9 Tunnel ground support technology

Tunnel rock supports are, "installed in one, two, or three stages depending on the type of tunnel cross section in the face area in the excavation area; and in the rear area. Bolting operations i.e. drilling, placing, and prestressing of the rock bolts are in most cases completely automated. Two types of rock bolting are utilized:
System bolting pattern: This means rock bolts are installed according to a systematical predetermined pattern spacing that depends on the rock support class; and Local bolting of single fracture blocks: This refers to the means used for holding back and preventing the falling of fractured rock".

## CHAPTER

## 3 WORK DONE

### 3.1 Equipment required

Two boom drill jumbo, Dumpers, Excavators, Loaders, Shotcrete machine, Concrete pump, Gantry with shutter Hydra crane, Batching plant, Scissor Lift, etc.

### 3.2 Excavation

### 3.2.1 Open excavation

This work shall consist of excavation by mechanical means in all types of strata, in rock by blasting or line drilling using pneumatic equipment and expanding agents, chiselling including dressing to final line, level, grades including hauling of excavated materials to site, also disposal of unsuitable cut materials in specified manner.

### 3.2.2 Job procedure

Rock excavation by blasting includes all solid rock in place which cannot be removed until loosened by blasting, barring or wedging, removal of all boulders or detached pieces of solid rock larger than 1 cum in volume, as well as any existing structural foundation made of concrete or masonry placed in mortar which cannot be removed during common excavation or by ripping.

The blasting operations shall be prepared or made by the competent and experienced personnel and workmen who are thoroughly acquainted with details of handling explosives and blasting operations.

Diameter and spacing of blast holes shall be constantly adapted to the actual site conditions. The charge holes shall be drilled by using jack hammer drill. All the excavated rock shall be removed from the bench toe before the next shot.

If a misfire is due to a defective detonator or dynamite the whole quantity or box from the defective article was taken must be thoroughly inspected.

Blasting shall be carried out in fixed hours as ordered in writing by the Engineer and kept known to the people, public and authorities in the vicinity sufficiently in advance.

Red flags shall be displayed in all directions during blasting operations. People except those who actually light the fuse shall be prohibited from the area and all persons including workmen shall be excluded from the flagged area at least 10 minutes before firing, a warning alarm or siren sounded for this purpose.

### 3.3 Underground excavation

### 3.3.1 Job procedure

1. The underground excavation of Diversion Tunnel will be carried out in 2 stages namely Heading: Excavation of top arch shaped area of Diversion Tunnel and providing required support systems
2. Benching: Excavation of bottom area of Diversion Tunnel
3. Drill holes shall be cleaned for dust \& rock cutting by air flushing before charging.
4. After charging operation, Mining Engineer/ Shift In-charge along with Engineer Incharge shall note down charge concentration per hole, positioning of delay detonators, and capacity of blasting device in prescribed format.
5. Dewatering of seepage water shall be removed to avoid water logging in the tunnel

### 3.4 Blasting pattern

Drilling and blasting pattern i.e. the number of holes; depth of holes, quantity, quality and distribution of explosives shall be decided as to suit the rock conditions encountered.

Drilling and Blasting shall be carried out as per the pattern proposed and approved by Engineer In-charge and shall be changed or modified as per the rock conditions encountered.


Fig 3.1 Drilling Pattern


Fig 3.2 Charging explosive

Open excavation time at Inlet portal $=\frac{\text { Excavated Quantity }}{\text { Excavator productivity } \times \text { working hour in a day }}$
$=\frac{85764 \mathrm{~m}^{3}}{50 \mathrm{~m}^{3} \text { per hour } \times 24 \text { hour }}$
$=55$ days
Open excavation time at Outlet portal $=\frac{\text { Excavated Quantity }}{\text { Excavator productivity } \times \text { working hour in a day }}$
$=\frac{40427 \mathrm{~m}^{3}}{50 \mathrm{~m}^{3} \text { per hour } \times 24 \text { hour }}$
$=28$ days
No. of Dumpers required:
Cycle time of dumpers $=($ Hauling + Tipping + Turning + Loading $)$
Loading time $=$ no of bucket required to fill a bucket $\times$ time taken by a loader in a single bucket to fill dumper $=7 \times 1.2=8.4$ minute

Time for hauling $=\left(\frac{\text { dumping yard distance }}{\text { avg.speed of dumper truck }}\right) \times$ time per hour $=\left(\frac{2 \times 4}{20}\right) \times 60 \mathrm{~min}=24$ minute
Turning time $=4$ minute
Tipping time $=1$ minute

Total cycle time $=(8.4+24+4+1)$ minute $=37.4 \mathrm{~min}$
No. of dumpers required $=\frac{\text { Cycle time }}{\text { Loading time }}$
$=\frac{37.4}{8.4}=4.45=5$ nos. dumper
Table 3.1 Major Quantities

| S.N | Description | Location | Quantity | Unit |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Open Excavation | Inlet Portl | 85764 | cum |
| 2 | Concrete | Inlet Portl | 10601 | cum |
| 3 | Open Excavation | Outlet Portal | 40427 | cum |
| 4 | Concrete | Outlet Portal | 152 | cum |
| 5 | Heading | DT -1 | 42042 | cum |
| 6 | Benching | DT -1 | 21595 | cum |
| 7 | Concrete lining | DT -1 | 11798 | cum |
| 8 | Heading | DT -2 | 49134 | cum |
| 9 | Benching | DT -2 | 25237 | cum |
| 10 | Concrete lining | DT -2 | 13635 | cum |

### 3.5 Heading in Diversion tunnel

Heading excavation will be carried out by Drilling \& Blasting methodology. Heading work will be carried out continuously in a cyclic process along with the supporting work. Types of supporting work will depend on the rock classes encountered.

## Sequence of operation in tunnel excavation without rib supporting:

1. Profile marking by surveyor
2. Drilling by Two boom drill jumbo
3. Charging \& blasting by professional blaster
4. Mucking by wheel loader and dumpers
5. Scaling/Trimming to the required excavation line
6. Supporting by Steel Fiber Reinforced Shotcrete
7. Fixing of Rock Bolts
8. Extension of ventilation duct

## Sequence of operation in tunnel excavation with rib supporting

1. Profile marking by surveyor
2. Drilling by Two boom drill jumbo
3. Charging \& blasting by professional blaster
4. Mucking by wheel loader and dumpers
5. Scaling/Trimming to the required excavation line
6. Supporting by Steel Fiber Reinforced Shotcrete
7. Fixing of Rock Bolts
8. Supporting by steel Ribs
9. Precast RCC lagging fixing
10. Back fill concreting
11. Extension ventilation duct

## EXCAVATION BY DRILL \& BLAST METHOD



Fig 3.3 Cross-sectional view of Diversion Tunnel

### 3.6 Cycle time calculation for different activities for heading work of DT by Drill \& Blast method <br> $1^{\text {st }}$ Activity: Survey -0.5 hours

$2^{\text {nd }}$. Activity: Time required for drilling
$=\frac{\text { Tot drilling length }}{\text { length per hour achieved by drilled jumbo }}=\frac{\text { no of drill holes } \times \text { length of each hole }}{\text { length per hour achieved by drilled jumbo }}=\frac{165 \times 3.2}{100 \mathrm{~m} / \mathrm{hr}}$
$=5.0$ hours
$3^{\text {rd }}$. Activity: Charging $=1.0$ hour
$4^{\text {th }}$.Activity: Blasting \& Defuming $=0.5$ hours
$5^{\text {th }}$. Activity: Time required for Mucking $=\frac{\text { Mucking Quantity }}{\text { productivity of loader }}$
Excavated quantity $=\mathrm{c} / \mathrm{s}$ area of tunnel $\times$ length of drill $=\left(\frac{\pi \times d^{2}}{4}\right) \times$ length of drill
$=\frac{\pi \times 8.0225^{2}}{4} \times 3=151.6458 \boldsymbol{m}^{3}$
Mucking quantity $=151.6458 \times 1.2(20 \%$ as over-break quantity $)$
$=182.0 \mathrm{~m}^{3}$ (mucking quantity will be more than the excavated quantity because there wil be some voids in the quantity)

Time required for mucking quantity $=\frac{\text { Mucking quantity }}{\text { Productivity of loader }}=\frac{182 \mathrm{~m}^{3}}{65 \mathrm{~m}^{3}}$ per hour $=3.0$ hour
$6^{\text {th }}$. Activity: Scaling time -1.0 hours
$7^{\text {th }}$. Activity: Time required for shotcreting $=\frac{\text { Quantityty of shotcrete }}{\text { productivity of shotcret machine }}$
Quantity of shotcrete $=$ Circumference of tunnel $\times$ thickness of shotcrete $\times$ length per cycle

1. For Good Rock Shotcreting $(5 \mathrm{~cm})=2 \pi \mathrm{r} \times 5 \mathrm{~cm} \times 3 \mathrm{~m}$

$$
\begin{aligned}
& =2 \pi \times 4.01125 \times 0.05 \times 3 \\
& =3.7805 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound })
\end{aligned}
$$

$$
=4.1585 \mathrm{~m}^{3}
$$

Time required for shotcreting $=\frac{\text { quantity of shotcrete }}{\text { productivity of shotcrete machine }}=\frac{4.1585 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=0.5$ hour
2. For Fair Rock Shotcreting $(10 \mathrm{~cm})=2 \pi \times 4.01125 \times 0.1 \times 3$

$$
\begin{aligned}
& =7.5610 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =8.3171 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete machine }}=\frac{8.3171 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=1.0$ hour
3. For Poor Rock Shotcreting $(15 \mathrm{~cm})=2 \pi \times 4.01125 \times 0.15 \times 3$

$$
\begin{aligned}
& =11.4315 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =12.4756 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete machine }}=\frac{12.4756 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=2.0$ hour
4. For Very Poor Rock Shotcreting $(20 \mathrm{~cm})=2 \pi \times 4.01125 \times 0.2 \times 3$

$$
\begin{aligned}
& =15.1220 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =16.6342 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete machine }}=\frac{16.634 \quad 3}{6 \mathrm{~m}^{3} \text { per hour }}=2.5$ hour $8^{\text {th }}$. Activity: Rock bolt drilling \& fixing Time :

## 1. For Good \& Fair Rock:

Circumference of circle $=2 \pi \mathrm{r}$
$=\left(\frac{2 \pi r}{\text { distance of two rock bolt }}+1\right) \times 2=\left(\frac{2 \times \pi \times 4.011}{2.3}+1\right) \times 2$
$=24$ no. in 3 m stretch of tunnel
Total drilling length of Rock bolt= Total nos. of rock bolt $\times$ length of each rock bolt

$$
=24 \times 3 \mathrm{~m}=72 \mathrm{~m}
$$

Time required for drilling $=\frac{\text { total drilling leng }}{\text { productivity of drill jumbo }}=\frac{72 \mathrm{~m}}{100 \mathrm{~m} \text { per hour }}=1.0$ hour

Time required for fixing $\&$ grouting $=($ no. of rock bolt $) \times($ time required for each rock bolt)

$$
=24 \times 3 \mathrm{~min}=72 \mathrm{~min}=1.0 \text { hours }
$$

Total rock bolt drilling fixing time $=(1+1)$ hour $=2.0$ hour

## 2. For Poor \& Very Poor Rock:

Circumference of circle $=2 \pi \mathrm{r}$
$=\left(\frac{2 \pi r}{\text { distance of two rock bolt }}+1\right) \times 2=\left(\frac{2 \times \pi \times 4.011}{1.7}+1\right) \times 2$
$=32$ no. in 3 m stretch of tunnel
Total drilling length of Rock bolt $=$ Total nos. of rock bolt $\times$ length of each rock bolt

$$
=32 \times 3 \mathrm{~m}=96 \mathrm{~m}
$$

Time required for drilling $=\frac{\text { total drilling length }}{\text { productivity of drill jumbo }}=\frac{96 \mathrm{~m}}{100 \mathrm{~m} \text { per hour }}=1.5$ hours
Time required for fixing $\&$ grouting $=($ no. of rock bolt $) \times($ time required for each rock bolt)

$$
=32 \times 3 \mathrm{~min}=96 \text { minute }=1.5 \text { hours }
$$

Total rock bolt drilling fixing time $=(1.5+1.5)$ hour $=3.0$ hour

### 3.7 Cycle time for heading in Diversion tunnel

3 m pull length per cycle to be considered for heading without rib and 1.5 m pull length to be considered for heading with rib.

### 3.7.1 Cycle time for heading without rib support in DT

Excavation without rib support is considered as $90 \%$ of total excavation in Diversion tunnels.

Table 3.2 Cycle time for heading without rib support in DT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 3 | m |
| 2 | Heading c/s area | 82.67 | sqm |
| 3 | Excavation | 248.01 | cum |
| 4 | Survey | 0.5 | Hours |
| 5 | Drilling | 5 | Hours |
| 6 | Chrging | 1 | Hours |
| 7 | Blasting\&defuming | 1 | Hours |
| 8 | Mucking | 3 | Hours |
| 9 | Scaling | 1 | Hours |
| 11 | shotcreting | 1 | Hours |
| 12 | Rockbolt drilling \& fixing | 2 | Hours |
|  | Total cycle time for 3 m pull length | 14.5 | Hours |

### 3.7.2 Cycle time for heading with rib support in DT

Excavation with rib support is considered as $10 \%$ of total excavation in Diversion tunnels.

Table 3.3 Cycle time for heading with rib support in DT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull Length | 1.5 | m |
| 2 | Heading c/s area | 82.67 | sqm |
| 3 | Excavation | 124.005 | cum |
| 4 | Survey | 0.5 | Hours |
| 5 | Drilling | 5 | Hours |
| 6 | Charging | 1 | Hours |
| 7 | Blasting\&defuming | 1 | Hours |
| 8 | Mucking | 3 | Hours |
| 9 | Scaling | 1 | Hours |
| 10 | Shotcreting | 2.5 | Hours |
| 11 | Rockbolt drilling \& fixing | 3 | Hours |
| 12 | Rib erection | 3 | Hours |
| 13 | Lagging fixing | 3 | Hours |
| 14 | Stopper fixing\&Back fill concrete | 4 | Hours |
|  | Total cycle time per 1.5m pull length | $\mathbf{2 7}$ | Hours |
|  | Total cycle time per 3m pull length | 54 | Hours |

## Time Schedule:

Among the total excavation $90 \%$ is considered as without rib support and $10 \%$ as with rib support.

Weighted average cycle time $=(14.5 \times 0.9)+(54 \times 0.1)=18.45$ hours per 3 m pull length
Progress per month $=\frac{26(\text { working day per month }) \times 22(\text { working hours per day }) \times 3 \mathrm{~m}(\text { pull length })}{18.45(\text { weighted cycle time in hours })}$
$=93 \mathrm{~m}$ per month
Time required for completion of heading work $=\frac{\text { Length of Diversion tunnel-1 }}{\text { Work progress per month }}=$ $\frac{472}{93 \mathrm{~m} \text { per month }}$
$=5.0$ month $=150$ Days
Time required for completion of heading work $=\frac{\text { Length of Diversion tunnel-2 }}{\text { Work progress per month }}=$ 552
93 m per month
$=6.0$ month $=180$ Days

### 3.8 Benching in Diversion tunnel

Benching work will be started on completion of heading work. It will be carried out continuously in a cyclic process using Drilling \& Blasting method. Sequences of works are same as mentioned in "Heading" except that no Rock Bolt support is required in Benching work and supporting works are required in both side faces.

### 3.9 Cycle time calculation for benching in Diversion tunnels by Drill \& Blast method

$1^{\text {st }}$. Activity: Surveying time -0.5 hours
$2^{\text {nd }}$. Activity: Drilling time
$=\frac{\text { Total drilling length }}{\text { length per hour achieved by drilled jumbo }}=\frac{(\text { no of drill holes }) \times(\text { length of each hole })}{\text { length per hour achieved by drill jumbo }}=\frac{81 \times 3.2}{100}$
$=2.5$ hour
$3^{\text {rd }}$.Activity: Charging time $=0.5$ hour
$4^{\text {th }}$. Activity: Blasting \& Defuming $=0.5$ hours
$5^{\text {th }}$. Activity: Mucking time $=\frac{\text { Mucking quantity }}{\text { productivity of loader }}$
Mucking quantity $=\mathrm{C} / \mathrm{S}$ area of tunnel $\times$ length of drill
$=\left(\frac{\pi \times d^{2}}{4}\right) \times$ drill length $=\left(\frac{\pi \times 4.3225^{2}}{4}\right) \times 3 \mathrm{~m}=41.4690 \mathrm{~m}^{3}$
Mucking Qty $=41.4690 \times 1.2(20 \%$ as over-break quantity $)$
$=52.8277 m^{3}$ (mucking qty will be more than the excavated quantity because there will be some voids in the quantity)

Time required for mucking quantity $=\frac{\text { Mucking quantity }}{\text { Productivity of loader }}=\frac{52.8277 \mathrm{~m}^{3}}{65 \mathrm{~m}^{3}}$ per hour $=1.0$ hour $6^{\text {th }}$. Activity: Scaling time $=0.5$ hour
$7^{\text {th }}$.Activity: Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcret machine }}$
Quantity of shotcrete $=$ Circumference of tunnel $\times$ thickness of shotcrete $\times$ length per cycle

1. For Good Rock Shotcreting $(5 \mathrm{~cm})=2 \pi r \times 5 \mathrm{~cm} \times 3 \mathrm{~m}=2 \pi \times 2.16125 \times 0.05 \times 3$

$$
\begin{aligned}
& =2.0369 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =2.2406 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete machine }}=\frac{2.2406 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=0.5$ hours
2. For Fair Rock Shotcreting $(10 \mathrm{~cm})=2 \pi \times 2.16125 \times 0.1 \times 3$

$$
\begin{aligned}
& =4.0738 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =4.4812 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete machine }}=\frac{4.4812 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=0.5$ hours
3. For Poor Rock Shotcreting $(15 \mathrm{~cm})=2 \pi \times 2.16125 \times 0.15 \times 3$

$$
\begin{aligned}
& =6.1107 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =6.7218 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete machine }}=\frac{6.7218 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=1.0$ hour
4. For Very Poor Rock Shotcreting $(20 \mathrm{~cm})=2 \pi \times 2.16125 \times 0.2 \times 3$

$$
\begin{aligned}
& =8.1477 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =8.9624 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete machine }}=\frac{8.9624 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=1.5$ hours

### 3.9.1 Cycle time for benching without rib support in DT

Table 3.4 Cycle time for benching without rib support in DT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull Length | 3 | m |
| 2 | Benching c/s area | 40.23 | sqm |
| 3 | Excavation | 120.69 | cum |
| 4 | Survey | 0.5 | Hours |
| 5 | Drilling | 2.5 | Hours |
| 6 | Charging | 0.5 | Hours |
| 7 | Blasting\&defiming | 0.5 | Hours |
| 8 | Mucking | 1 | Hours |
| 9 | Scaling | 0.5 | Hours |
| 11 | Shotcreting | 0.5 | Hours |
| 12 | Total cycle time for 3m pull length | 6 | Hours |
|  |  |  |  |

### 3.9.2 Cycle time for benching with rib support in DT

Table 3.5 Cycle time for benching in DT with rib support

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 1.5 | m |
| 2 | Benching c/s area | 40.23 | sqm |
| 3 | Excavation | 60.435 | cum |
| 4 | Survey | 0.5 | Hours |
| 5 | Drilling | 2.5 | Hours |
| 6 | Chrging | 0.5 | Hours |
| 7 | Blasting\&defuming | 0.5 | Hours |
| 8 | Mucking | 1 | Hours |
| 9 | Scaling | 0.5 | Hours |
| 10 | Shotcreting | 1.5 | Hours |
| 11 | Rib erection | 2 | Hours |
| 12 | Lagging fixing | $\mathbf{1}$ | Hours |
| 13 | Backfill concreting | $\mathbf{1}$ | Hours |
|  | Total cycle time for 1.5 m pull length | 11 | Hours |
|  | Total cycle time for 3 m pull length | 22 | Hours |

## Time Schedule:

Weighted average cycle time $=(6.0 \times 0.9)+(22 \times 0.1)=8.50$ hours per 3 m pull Progress per month $=\frac{(26(\text { working day per month }) \times 22(\text { working hours per day }) \times 3 \mathrm{~m} \text { pull length })}{8.50(\text { weighted average cycle time in hours })}$ $=202 \mathrm{~m}$ per month

Time required for Completion of benching work $=\frac{\text { Tunnel length }-1}{\text { progress per month }}$
$=\frac{472}{202}=2.33$ month $=70$ days
Time required for Completion of benching work $=\frac{\text { Tunnel length }-2}{\text { progress per month }}$
$=\frac{552}{202}=2.73$ month $=82$ days

### 3.10 Rock support work in Diversion tunnels

Rock support works in the tunnel shall be provided as given in the construction drawings in accordance to the rock classification given by the geologists and as per the directions of Engineer in Charge. The Rock Supports are classified depending upon the amount of hindrance it poses for the advancement of excavation work. The details of support system for each class of excavation are given below

For excavation in Good, Fair and Poor rock, support work shall consist of a Shotcrete layer of $5 \mathrm{~cm}, 10 \mathrm{~cm}$ and 15 cm thick respectively, sprayed in layers, followed by fixing of rock bolts. This shall consist of 25 mm diameter, 4 m for Good and Fair Rock and 5.0 meter long rock bolts for Poor Rock to be fixed in staggered manner as mentioned in approved drawings.

For excavation in Very Poor rock, support work shall consist of a shotcrete layer of 20 cm thick, sprayed. The spacing of rock bolt support, in case of good \& fair rock is 2.30 m and in the case of poor \& very poor rock 1.70 m .


Fig 3.4 Rock Bolt supporting

### 3.11 Concrete lining in Diversion tunnel

Concrete lining of tunnel will be taken up when the Heading and Benching excavation of the Diversion tunnel will be completed. Concrete lining for overt will be carried out using 15 m gantry equipped with 2 shutters and 1 traveller. The concrete lining of Diversion tunnel will commence from Inlet end.

## Concrete lining of the tunnel will be carried out in three stages:

1. Kerb Lining
2. Invert Lining
3. Overt Lining

### 3.11.1 Cycle time in kerb lining in Diversion tunnel

1. Surface cleaning should be done before Kerb concreting.
2. Kerb concreting will commence parallel to benching excavation with 1 month lag.
3. Kerb shutters with requisite anchoring in the rock will be used for kerb concreting.

Kerb lining area $=4.0 \mathrm{~m}^{2}$
Concrete quantity in 15 m length $=2 \times 4 \mathrm{~m}^{2} \times 15 \mathrm{~m}=120 \mathrm{~m}^{3}$
The rate of concrete for 2 agitator truck with 50 min per hour working: $3.5 \mathrm{~m}^{3}$ per hour

Time for placing the concrete $=\frac{\text { concrete Quantity }}{\text { concrete quantity in one truck } \times \text { working hour }}=\frac{120 \mathrm{~m}^{3}}{3.5 \times 22}=1.5$ hours

## Shutter panel- 1 ( 15 m length):

Table 3.6 Shutter panel-1 in Kerb lining in DT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :--- |
| 1 | Kerb shutter | 1.5 | Hours |
| 2 | Shutter alignment | 1 | Hours |
| 3 | Concreting | 1.5 | Hours |
| 4 | Concrete setting | 20 | Hours |
| 5 | De- shuttering | 1 | Hours |
| 6 | Miscellaneous | 1.5 | Hours |
|  | Total cycle time for 15 m panel | 26.5 | Hours |

## Shutter panel - 2 ( $\mathbf{1 5 m}$ length):

Table 3.7 Shutter panel-2 in Kerb lining in DT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :--- |
| 1 | Kerb shutter | 1.5 | Hours |
| 2 | Shutter alignment | 1 | Hours |
| 3 | Concreting | 1.5 | Hours |
| 4 | Concrete setting | 20 | Hours |
| 5 | De- shuttering | 1 | Hours |
| 6 | Miscellaneous | 1.5 | Hours |
|  | Total cycle time for 15 m panel | 26.5 | Hours |

## Time Schedule:

Cycle time for 30 m Kerb lining $=53$ Hours
Progress per month $=$
$=\frac{26(\text { working day per month }) \times 22(\text { working hours per day }) \times 30 \mathrm{~m} \text { (length of lining in cycle) }}{53(\text { weighted average cycle time in hours) }}$
$=323.77 \mathrm{~m}$ per month
Kerb lining time $=\frac{\text { Length of the tunnel }-1}{\text { working progress per month }}=\frac{472 \mathrm{~m}}{323.77 \mathrm{~m} \mathrm{per} \text { month }}=1.5 \mathrm{month}$
$=45$ days
Kerb lining time $=\frac{\text { Length of the tunnel }-1}{\text { working progress per month }}=\frac{552 \mathrm{~m}}{323.77 \mathrm{~m} \text { per month }}=1.7$ month
$=52$ days

### 3.11.2 Cycle time in invert lining in Diversion tunnel

1. Invert lining will be done using the invert template.
2. It will be carried out parallel to the overt concreting with a time lag of 1 month.

Invert lining area $=3.1 \mathrm{~m}^{2}$
Concrete quantity in 15 m length $=3.1 \mathrm{~m}^{2} \times 15 \mathrm{~m}=46.5 \mathrm{~m}^{3}$
The rate of concrete for 2 agitator truck with 50 min per hour working: $3.5 \mathrm{~m}^{3}$ per hour
Time for placing the concrete $=\frac{\text { concrete Quantity }}{\text { concrete quantity in one truck } \times \text { working hour }}=\frac{46.5 m^{3}}{3.5 \times 22}=0.5$ hours

Table 3.8 Shutter panel-1 in Invert lining in DT

| S.N | Description | Quantity | Hours |
| :---: | :---: | :---: | :---: |
| 1 | Invert template | 1.5 | Hours |
| 2 | Invert template alignment | 1 | Hours |
| 3 | Concreting | 0.5 | Hours |
| 4 | Concrete setting | 20 | Hours |
| 5 | De-shuttering | 1 | Hours |
| 6 | Miscellaneous | 2 | Hours |
|  | Total cycle time for 15 m panel | 26 | Hours |

Table 3.9 Shutter panel - 2 in Invert lining in DT

| S.N | Description | Quantity | Hours |
| :---: | :---: | :---: | :---: |
| 1 | Invert template | 1.5 | Hours |
| 2 | Invert template alignment | 1 | Hours |
| 3 | Concreting | 0.5 | Hours |
| 4 | Concrete setting | 20 | Hours |
| 5 | De-shuttering | 1 | Hours |
| 6 | Miscellaneous | 2 | Hours |
|  | Total cycle time for 15 m panel | 26 | Hours |

## Time Schedule:

Cycle time for 30 m Invert concreting $=52$ Hours
Progress per month $=$
$\underline{26(\text { working day per month) } \times 22 \text { (working hours per day) } \times 30 \mathrm{~m} \text { (length of lining in cycle) }}$ 52 (weighted average cycle time in hours)
$=330 \mathrm{~m}$ per month

Invert lining time $=\frac{\text { Length of the tunnel }-1}{\text { working progress per month }}=\frac{472 \mathrm{~m}}{330 \mathrm{~m} \text { per month }}=1.5 \mathrm{month}=45$ days
Invert lining time $=\frac{\text { Length of the tunnel }-2}{\text { working progress per month }}=\frac{552 \mathrm{~m}}{330 \mathrm{~m} \text { per month }}=1.67$ month $=50$ days

### 3.11.3 Cycle time for overt lining in Diversion tunnel

1. Overt lining will be carried out using gantry with traveller.
2. Gantry will be erected after completion of benching excavation.
3. After Gantry erection, overt lining will commence.
4. Traveller will be moving on rails fixed on kerb concrete.
5. Shutter will be fixed to the kerb concrete to avoid uplifting due to concreting.
6. Shutter will be properly aligned by adjusting hydraulic jacks.
7. Pneumatic vibrator will be used for regular distribution and compactness.
8. Concreting in the 2 nd shutter position will be carried out parallel to the concrete setting in 1st shutter position and will continue in the cyclic manner.


Fig 3.5 Overt Lining

## Shutter panel - $\mathbf{- 1}$ ( $\mathbf{1 5} \mathbf{m}$ length):

Overt lining area $=16.54 \mathrm{~m}^{2}$
Concrete quantity in 15 m length $=16.54 \mathrm{~m}^{2} \times 15 \mathrm{~m}=248.1 \mathrm{~m}^{3}$
The rate of concrete for 2 agitator truck with 50 min per hour working: $3.5 \mathrm{~m}^{3}$ per hour

Time for placing the concrete $=\frac{\text { concrete Quantity }}{\text { concrete quantity in one truck } \times \text { working hour }}=\frac{248.1 m^{3}}{3.5 \times 22}=3.5$ hours

Table 3.10 Shutter panel-1 in Overt Lining in DT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :--- |
| 1 | Rail fixing | 2 | Hours |
| 2 | Shutter shifting | 3 | Hours |
| 3 | Shutter alignment | 3 | Hours |
| 4 | Bulk had fixing | 2 | Hours |
| 5 | Concreting | 3.5 | Hours |
| 6 | Concrete setting | 20 | Hours |
| 7 | De- shuttering | 2 | Hours |
| 8 | Miscellaneous | 3 | Hours |
|  | Total cycle time for 15 m panel | $\mathbf{3 8 . 5}$ | Hours |

Table 3.11 Shutter panel -2 in overt lining in DT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Rail fixing | 2 | Hours |
| 2 | Shutter shifting | 3 | Hours |
| 3 | Shutter alignment | 3 | Hours |
| 4 | Bulk had fixing | 2 | Hours |
| 5 | Concreting | 3.5 | Hours |
| 6 | Concrete setting | 20 | Hours |
| 7 | De- shuttering | 2 | Hours |
| 8 | Miscellaneous | 3 | Hours |
|  | Total cycle time for 15 m panel | $\mathbf{3 8 . 5}$ | Hours |

## Time Schedule:

Cycle time for 30 m Overt lining $=77$ Hours
Progress per month $=$
$\underline{26(\text { working day per month) } \times 22 \text { (working hours per day) } \times 30 \mathrm{~m} \text { (length of lining in cycle) }}$

$$
77 \text { (weighted average cycle time in hours) }
$$

$=222 \mathrm{~m}$ per month
Overt lining time $=\frac{\text { Length of the tunnel }-1}{\text { working progress per month }}=\frac{472 \mathrm{~m}}{222 \quad \text { per month }}=2$ month $=60$ days
Overt lining time $=\frac{\text { Length of the tunnel }-2}{\text { working progress per month }}=\frac{552 \mathrm{~m}}{222 \mathrm{~m} \text { per month }}=2.5 \mathrm{month}=75$ days

Table 3.12 Length of DT- 1 in different rock conditions

| Diversion Tunnel-1 $(472 \mathrm{~m})$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Good(15\%) | $\operatorname{Fair}(60 \%)$ | $\operatorname{Poor}(15 \%)$ | $\operatorname{V.Poor}(10 \%)$ |
|  |  | 70.8 m | 283.2 m | 70.8 m | 47.2 m |
|  | Inlet | 35.4 m | 141.6 m | 35.4 m | 23.6 m |
|  | Outlet | 35.4 m | 141.6 m | 35.4 m | 23.6 m |

Time duration for different rock conditions:
Table 3.13 Time Duration in DT - 1

|  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Activity | Source | Good | Fair | Poor | V.Poor | Total days |
| Heading | Inlet | 11 | 45 | 11 | 8 | 75 |
| Heading | Outlet | 11 | 45 | 11 | 8 | 75 |
| Benching | Inlet | 5 | 21 | 5 | 3 | 34 |
| Benching | Outlet | 5 | 21 | 5 | 3 | 34 |
| Invert lining | Inlet | 3 | 13 | 3 | 2 | 21 |
| Invert lining | Outlet | 3 | 13 | 3 | 2 | 21 |
| Kerb lining | Inlet | 3 | 13 | 3 | 3 | 22 |
| Kerb lining | Outlet | 3 | 13 | 3 | 3 | 22 |
| Overt lining | Inlet | 15 | 19 | 15 | 3 | 52 |
| Overt lining | Outlet | 15 | 19 | 15 | 3 | 52 |
|  |  |  |  |  |  |  |

Length in DT- $\mathbf{2}$ for different rock conditions:

Table 3.14 Length of DT - 2

| Diversion Tunnel -2 (552 m) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Source | Good(15\%) | Fair(60\%) | Poor(15\%) | V.Poor $(10 \%$ |
|  |  | 82.8 m | 331.2 m | 82.8 m | 55.2 m |
|  | Inlet | 41.4 m | 165.6 m | 41.4 m | 27.6 m |
|  | Outlet | 41.4 m | 165.6 m | 41.4 m | 27.6 m |

Time duration for different rock conditions:
Table 3.15 Time duration in DT- 2

| Activity | Source | Good | Fair | Poor | V.Poor | Total Days |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | Inlet | 14 | 55 | 14 | 9 | 88 |
| Heading | Outlet | 14 | 55 | 14 | 9 | 88 |
| Benching | Inlet | 6 | 24 | 6 | 4 | 40 |
| Benching | Outlet | 6 | 24 | 6 | 4 | 40 |
| Invert lining | Inlet | 4 | 15 | 4 | 2 | 25 |
| Invert lining | Outlet | 4 | 15 | 4 | 2 | 25 |
| Kerb lining | Inlet | 4 | 15 | 4 | 2 | 25 |
| Kerb lining | Outlet | 4 | 15 | 4 | 2 | 25 |
| Overt lining | Inlet | 5 | 23 | 5 | 4 | 37 |
| Overt lining | Outlet | 5 | 23 | 5 | 4 | 37 |

Table 3.16 Activities duration for Diversion Tunnel

| RHP - DT |  | Classic WBS Layout |  |  |  | 28-Apr-17 18:47 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Activity ID | Activity Name | Original Duration | Remaining Duration | Schedule \% Complete | Start | Finish | Total Float |  |
| RHP - DT |  | 223 | 223 | 0\% | 15-May-17 | 22-Nov-17 | 0 |  |
| A1000 | Mobilisation | 30 | 30 | 0\% | 15-May-17 | 08-Jun-17 | 0 |  |
| DT Portal |  | 55 | 55 | 0\% | 08-Jun-17 | 26-Jul-17 | 0 |  |
| A1020 | Dt portal outlet | 28 | 28 | 0\% | 08-Jun-17 | 03-Jul-17 | 9 |  |
| A1130 | Dt portal inlet | 55 | 55 | 0\% | 08-Jun-17 | 26-Jul-17 | 0 |  |
| DIVERSION TUNNEL 1 |  | 169 | 169 | 0\% | 21-Jun-17 | 14-Nov-17 | 9 |  |
| A1030 | Heading Inlet | 75 | 75 | 0\% | 21-Jun-17 | 24-Aug-17 | 9 |  |
| A1080 | Heading outlet | 75 | 75 | 0\% | 21-Jun-17 | 24-Aug-17 | 9 |  |
| A1040 | Benching Inlet | 34 | 34 | 0\% | 24-Aug-17 | 22-Sep-17 | 9 |  |
| A1090 | Benching outlet | 34 | 34 | 0\% | 24-Aug-17 | 22-Sep-17 | 9 |  |
| A1060 | Kerb inlet | 22 | 22 | 0\% | 12-Sep-17 | 29-Sep-17 | 9 |  |
| A1110 | kerb outlet | 22 | 22 | 0\% | 12-Sep-17 | 29-Sep-17 | 9 |  |
| A1070 | Overt inlet | 52 | 52 | 0\% | 29-Sep-17 | 14-Nov-17 | 9 |  |
| A1120 | overt outlet | 52 | 52 | 0\% | 29-Sep-17 | 14-Nov-17 | 9 |  |
| A1050 | Invert Inlet | 21 | 21 | 0\% | 18-Oct-17 | 03-Nov-17 | 20 |  |
| A1100 | Invert Outlet | 21 | 21 | 0\% | 18-Oct-17 | 03-Nov-17 | 20 |  |
| DIVERSION TUNNEL 2 |  | 178 | 178 | 0\% | 21-Jun-17 | 22-Nov-17 | 0 |  |
| A1170 | Heading Inlet | 88 | 88 | 0\% | 21-Jun-17 | 05-Sep-17 | 0 |  |
| A1220 | Heading outlet | 88 | 88 | 0\% | 03-Jul-17 | 15-Sep-17 | 55 |  |
| A1230 | Benching outlet | 40 | 40 | 0\% | 20-Jul-17 | 23-Aug-17 | 55 |  |
| A1250 | kerb outlet | 25 | 25 | 0\% | 07-Aug-17 | 28-Aug-17 | 55 |  |
| A1260 | overt outlet | 37 | 37 | 0\% | 28-Aug-17 | 28-Sep-17 | 55 |  |
| A1180 | Benching Inlet | 40 | 40 | 0\% | 05-Sep-17 | 10-Oct-17 | 0 |  |
| A1240 | Invert Outlet | 25 | 25 | 0\% | 14-Sep-17 | 05-Oct-17 | 55 |  |
| A1200 | Kerb inlet | 25 | 25 | 0\% | 22-Sep-17 | 13-Oct-17 | 0 |  |
| A1210 | Overt inlet | 37 | 37 | 0\% | 13-Oct-17 | 15-Nov-17 | 0 |  |
| A1190 | Invert Inlet | 25 | 25 | 0\% | 31-Oct-17 | 22-Nov-17 | 0 |  |



Fig 3.6 Network diagram of Diversion Tunnel in case of Drill \& Blast method


Fig 3.7 Cross-sectional view of Pressure shaft

### 3.12 Cycle time calculation for different activities for heading work of Pressure shaft by Drill \& Blast method

$1^{\text {st }}$ Activity: Survey -0.5 hours
$2^{\text {nd }}$. Activity: Time required for drilling
$=\frac{\text { Total drilling length }}{\text { length per hour achieved by drilled jumbo }}=\frac{\text { no of holes } \times \text { length of each hole }}{\text { length per hour achieved by drilled jumbo }}=\frac{68 \times 3.2}{100 \mathrm{~m} / \mathrm{hr}}$
$=2.0$ hours
$3^{\text {rd }}$. Activity: Charging $=0.5$ hour
$4^{\text {th }}$.Activity: Blasting \& Defuming $=0.5$ hours
$5^{\text {th }}$. Activity: Time required for Mucking $=\frac{\text { Mucking Quantity }}{\text { productivity of loader }}$
Mucking quantity $=$ Cross-sectionl area of tunnel $\times$ length of drill $=\left(\frac{\pi \times d^{2}}{4}\right) \times$ length of drill
$=\frac{\pi \times 5.2725^{2}}{4} \times 3=65.5004 \mathrm{~m}^{3}$
$=$ Mucking Quantity $=65.5004 \times 1.2(20 \%$ as over-break quantity $)$
$=78.6005 \mathrm{~m}^{3}$ (mucking quantity will be more than the excavated quantity because there wil be some voids in the quantity)

Time required for mucking quantity $=\frac{\text { Mucking Quantity }}{\text { Productivity of loader }}=\frac{78.6005 \mathrm{~m}^{3}}{65 \mathrm{~m}^{3}}$ per hour $=1.5$ hour
$6^{\text {th }}$. Activity: Scaling time -0.5 hours
$7^{\text {th }}$. Activity: Time required for shotcreting $=\frac{\text { Quantityty of shotcrete }}{\text { productivity of shotcret machine }}$
Quantity of shotcrete $=$ Circumference of tunnel $\times$ thickness of shotcrete $\times$ length per cycle

1. For Good Rock Shotcreting $(5 \mathrm{~cm})=2 \pi \mathrm{r} \times 5 \mathrm{~cm} \times 3 \mathrm{~m}$

$$
\begin{aligned}
& =2 \pi \times 2.6362 \times 0.05 \times 3 \\
& =2.4845 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =2.7330 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{2.7330 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=0.5$ hour
2. For Fair Rock Shotcreting $(10 \mathrm{~cm})=2 \pi \times 2.6362 \times 0.1 \times 3$

$$
\begin{aligned}
& =4.9691 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =5.4660 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{5.4660 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=1.0$ hour
3. For Poor Rock Shotcreting $(15 \mathrm{~cm})=2 \pi \times 2.6362 \times 0.15 \times 3$

$$
\begin{aligned}
& =7.4536 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =8.1990 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{8.1990 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=1.5$ hour
4. For Very Poor Rock Shotcreting $(20 \mathrm{~cm})=2 \pi \times 2.6362 \times 0.2 \times 3$

$$
\begin{aligned}
& =9.9382 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =10.9320 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{10.9320 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=2.0$ hour

## $8^{\text {th }}$. Activity: Rock bolt drilling \& fixing:

## 1. For Good \& Fair Rock:

Circumference of circle $=2 \pi \mathrm{r}$
$=\left(\frac{2 \pi r}{\text { distance of two rock bolt }}+1\right) \times 2=\left(\frac{2 \times \pi \times 2.6362}{2.3}+1\right) \times 2$
$=17 \mathrm{no}$. in 3 m stretch of tunnel
Total drilling length of Rock bolt $=$ Total nos. of rock bolt $\times$ length of each rock bolt

$$
=17 \times 3 \mathrm{~m}=51 \mathrm{~m}
$$

Time required for drilling $=\frac{\text { total drilling length }}{\text { productivity of drill jumbo }}=\frac{51 \mathrm{~m}}{100 \mathrm{~m} \text { per hour }}=0.5$ hour
Time required for fixing \& grouting $=($ no. of rock bolt $) \times($ time required for each rock bolt)

$$
=17 \times 3 \mathrm{~min}=51 \text { minute }=1.0 \text { hours }
$$

Total rock bolt drilling fixing time $=(0.5+1)$ hour $=1.5$ hour

## 2. For Poor \& V. Poor Rock:

Circumference of circle $=2 \pi \mathrm{r}$

$$
\begin{aligned}
& =\left(\frac{2 \pi r}{\text { distance of two rock bolt }}+1\right) \times 2=\left(\frac{2 \times \pi \times 2.6362}{1.7}+1\right) \times 2 \\
& =22 \text { no. in } 3 \mathrm{~m} \text { stretch of tunnel }
\end{aligned}
$$

Total drilling length of Rock bolt $=$ Total nos. of rock bolt $\times$ length of each rock bolt

$$
=22 \times 3 \mathrm{~m}=66 \mathrm{~m}
$$

Time required for drilling $=\frac{\text { total drilling length }}{\text { productivity of drill jumbo }}=\frac{66 \mathrm{~m}}{100 \mathrm{~m} \text { per hour }}=0.5$ hours
Time required for fixing \& grouting $=($ no. of rock bolt $) \times($ time required for each rock bolt)
$=22 \times 3 \mathrm{~min}=66$ minute $=1.0$ hours
Total rock bolt drilling fixing time $=(0.5+1.0)$ hour $=1.5$ hour

### 3.13 Cycle time for heading in Pressure shaft

3 m pull length per cycle to be considered for heading without rib support and 1.5 m pull length to be considered for heading with rib support.

### 3.13.1 Cycle time for heading without rib support in Pressure shaft

Excavation without rib support is considered as $90 \%$ of total excavation in Pressure shaft.
Table 3.17 Cycle time for heading without rib support in PS

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 3 | m |
| 2 | Heading c/s area | 34.0369 | sqm |
| 3 | Excavation | 102.11 | cum |
| 4 | Survey | 0.5 | Hours |
| 5 | Drilling | 2 | Hours |
| 6 | Chrging | 0.5 | Hours |
| 7 | Blasting\&defuming | 0.5 | Hours |
| 8 | Mucking | 1 | Hours |
| 9 | Scaling | 0.5 | Hours |
| 10 | shotcreting | 1 | Hours |
| 11 | Rockbolt drilling \& fixing | 1.5 | Hours |
|  | Total cycle time for 3 m pull length | 7.5 | Hours |

### 3.13.2 Cycle time for heading with rib support in Pressure shaft

Excavation with rib support is considered as 10 \% of total excavation in Pressure Shaft.

Table 3.18 Cycle time for heading with rib support in PS

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull Length | 1.5 | m |
| 2 | Heading c/s area | 34.0369 | sum |
| 3 | Excavation | 51.05 | cum |
| 4 | Survey | 0.5 | Hours |
| 5 | Drilling | 2 | Hours |
| 6 | Charging | 0.5 | Hours |
| 7 | Blasting\&defuming | 0.5 | Hours |
| 8 | Mucking | 1.5 | Hours |
| 9 | Scaling | 0.5 | Hours |
| 10 | Shotcreting | 2 | Hours |
| 11 | Rockbolt drilling \& fixing | 1.5 | Hours |
| 12 | Rib erection | 2 | Hours |
| 13 | Lagging fixing | 2.5 | Hours |
| 14 | Stopper fixing\&Back fill concrete | 2.5 | Hours |
|  | Total cycle time per 1.5 m pull length | $\mathbf{1 6}$ | Hours |
|  | Total cycle time per 3m pull length | 32 | Hours |

## Time Schedule:

Among the total excavation $90 \%$ is considered as without rib supporting and $10 \%$ as with rib supporting

Weighted average cycle time $=(7.5 \times 0.9)+(32 \times 0.1)=10.0$ hours per 3 m pull length
Progress per month $=\frac{(26(\text { working day per month }) \times 22(\text { working hours per day }) \times 3 \mathrm{~m} \text { pull length })}{10.0(\text { weighted cycle time in hours })}$
$=171.6 \mathrm{~m}$ per month
Time required for completion of heading work $=\frac{\text { Length of Pressure Shaft }}{\text { Work progress per month }}$
$=\frac{(211+197+184+172=764 \mathrm{~m})}{(171.6 \mathrm{~m} \text { per month })}=4.5$ month $=135$ days

### 3.14 Cycle time calculation for different activities for benching work in Pressure shaft by Drill \& Blast method

$1^{\text {st }}$. Activity: Surveying time -0.5 hours
2nt. Activity: Drilling time
$=\frac{\text { Total drilling length }}{\text { length per hour achieved by drilled jumbo }}=\frac{(\text { no of drill holes }) \times(\text { length of each hole })}{\text { length per hour achieved by drill jumbo }}=\frac{28 \times 3.2}{100}$
$=1.0$ hour
$3^{\text {rd }}$. Activity: Charging time $=0.5$ hour
$4^{\text {th }}$. Activity: Blasting \& Defuming $=0.5$ hours
$5^{\text {th }}$. Activity: Mucking time $=\frac{\text { Mucking quantity }}{\text { productivity of loader }}$
Mucking quantity $=$ Cross-sectional area of tunnel $\times$ length of drill
$=\left(\frac{\pi \times d^{2}}{4}\right) \times$ drill length $=\left(\frac{\pi \times 2.3725^{2}}{4}\right) \times 3 \mathrm{~m}=13.2624 \mathrm{~m}^{3}$
Mucking quantity $=13.2624 \times 1.2(20 \%$ as over-break quantity $)$
$=15.9149 \mathrm{~m}^{3}$ (mucking quantity will be more than the excavated quantity because there wil be some voids in the quantity)

Time required for mucking quantity $=\frac{\text { Mucking quantity }}{\text { Productivity of loader }}=\frac{15.9149 \mathrm{~m}^{3}}{65 \mathrm{~m}^{3}}$ per hour $=0.5$ hour $6^{\text {th }}$. Activity: Scaling time $=0.5$ hour
$7^{\text {th }}$. Activity: Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcret machine }}$
Quantity of shotcrete $=$ Circumference of tunnel $\times$ thickness of shotcrete $\times$ length per cycle

1. For Good Rock Shotcreting $(5 \mathrm{~cm})=2 \pi \mathrm{r} \times 5 \mathrm{~cm} \times 3 \mathrm{~m}$

$$
=2 \pi \times 1.1862 \times 0.05 \times 3
$$

$=1.1179 \mathrm{~m}^{3} \times(1.1)(10 \%$ as rebound $)$
$=1.2297 \mathrm{~m}^{3}$
Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{1.2297 m^{3}}{6 m^{3} \text { per hour }}=0.5$ hours
2. For Fair Rock Shotcreting $(10 \mathrm{~cm})=2 \pi \times 1.1862 \times 0.1 \times 3$

$$
\begin{aligned}
& =2.2359 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =2.4595 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{2.4595 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=0.5$ hours
3. For Poor Rock Shotcreting $(15 \mathrm{~cm})=2 \pi \times 1.1862 \times 0.15 \times 3$
$=3.3539 \mathrm{~m}^{3} \times(1.1)(10 \%$ as rebound $)$
$=3.6892 \mathrm{~m}^{3}$
Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{3.6892 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=0.5$ hour
4. For Very Poor Rock Shotcreting $(20 \mathrm{~cm})=2 \pi \times 1.1862 \times 0.2 \times 3$

$$
\begin{aligned}
& =4.718 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =4.9190 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{4.9190 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=1.0$ hours

### 3.15 Cycle time for benching without rib support in Pressure shaft

Table 3.19 Cycle time for benching without rib support in PS

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull Length | 3 | m |
| 2 | Benching c/s area | 13.8665 | sqm |
| 3 | Excavation | 41.5995 | cum |
| 4 | Survey | 0.5 | Hours |
| 5 | Drilling | 1 | Hours |
| 6 | Charging | 0.5 | Hours |
| 7 | Blasting\&defuming | 0.5 | Hours |
| 8 | Mucking | 0.5 | Hours |
| 9 | Scaling | 0.5 | Hours |
| 10 | Shotcreting | $\mathbf{0 . 5}$ | Hours |
| 11 | Total cycle time for 3m pull length | 4 | Hours |
|  |  |  |  |

### 3.15.1 Cycle time for benching with rib support in Pressure shaft

Table 3.20 Cycle time for benching with rib support in PS

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 1.5 | m |
| 2 | Benching c/s area | 13.8665 | sqm |
| 3 | Excavation | 20.79 | cum |
| 4 | Survey | 0.5 | Hours |
| 5 | Drilling | 1 | Hours |
| 6 | Charging | 0.5 | Hours |
| 7 | Blasting\&defuming | 0.5 | Hours |
| 8 | Mucking | 0.5 | Hours |
| 9 | Scaling | 0.5 | Hours |
| 11 | Shotcreting | 1 | Hours |
| 12 | Rib erection | 2 | Hours |
| 13 | Lagging fixing | $\mathbf{1}$ | Hours |
| 14 | Backfill concreting | $\mathbf{1}$ | Hours |
|  | Total cycle time for 1.5 m pull length | 8.5 | Hours |
|  | Total cycle time for 3 m pull length | 17 | Hours |

## Time Schedule:

Among the total excavation $90 \%$ is considered as without rib supporting and $10 \%$ as with rib supporting

Weighted average cycle time $=(4.0 \times 0.9)+(17 \times 0.1)=5.3$ hours per 3 m pull length
Progress per month $=\frac{26(\text { working day per month }) \times 22(\text { working hours per day }) \times 3 \mathrm{~m}(\text { pull length })}{5.3 m^{3} / \text { hour }}$
$=323 \mathrm{~m}$ per month
Time required for completion of Benching work $=\frac{\text { Length of Pressure Shaft }}{\text { Work progress per month }}$
$=\frac{(211+197+184+17)}{(323 \mathrm{~m} \text { per month })}$
$=2.5$ month $=75$ days

### 3.16 Cycle time in kerb lining in Pressure shaft:

Kerb lining area $=1.3 \mathrm{~m}^{2}$
Concrete quantity in 15 m length $=2 \times 1.3 \mathrm{~m}^{2} \times 15 \mathrm{~m}=39 \mathrm{~m}^{3}$
The rate of concrete for 2 agitator truck with 50 min per hour working: $3.5 \mathrm{~m}^{3}$ per hour
Time for placing the concrete $=\frac{\text { concrete Quantity }}{\text { concrete quantity in one truck } \times \text { working hou }}=\frac{39 \mathrm{~m}^{3}}{3.5 \times 22}=0.5$ hours

## Shutter panel - 1 ( $\mathbf{1 5} \mathbf{m}$ length):

Table 3.21 Cycle time in kerb lining in Shutter panel-1 in PS

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :--- |
| 1 | Kerb shutter | 1 | Hours |
| 2 | Shutter alignment | 1 | Hours |
| 3 | Concreting | 0.5 | Hours |
| 4 | Concrete setting | 20 | Hours |
| 5 | De- shuttering | 1 | Hours |
| 6 | Miscellaneous | 1.5 | Hours |
|  | Total cycle time for 15 m panel | 25 | Hours |

Shutter panel - 2 ( 15 m length):
Table 3.22 Cycle time in kerb lining in Shutter panel-2 in PS

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :--- |
| 1 | Kerb shutter | 1 | Hours |
| 2 | Shutter alignment | 1 | Hours |
| 3 | Concreting | 0.5 | Hours |
| 4 | Concrete setting | 20 | Hours |
| 5 | De- shuttering | 1 | Hours |
| 6 | Miscellaneous | 1.5 | Hours |
|  | Total cycle time for 15 m panel | 25 | Hours |

## Time Schedule:

Cycle time for 30 m Kerb concreting $=50$ Hours
Progress per month =
$\underline{26(\text { working day per month) } \times 22 \text { (working hours per day) } \times 30 \mathrm{~m} \text { (length of lining in cycle) }}$
50 (weighted average cycle time in hours)
$=343.5 \mathrm{~m}$ per month
Kerb lining time $=\frac{\text { Length of the pressure shaft }}{\text { working progress per month }}=\frac{(211+197+184+172) \mathrm{m}}{343.5 \mathrm{~m} \text { per month }}=2.5$ month $=75$ day

### 3.17 Cycle time in invert lining in Pressure shaft

Invert lining area $=1.3 \mathrm{~m}^{2}$
Concrete quantity in 15 m length $=1.3 \mathrm{~m}^{2} \times 15 \mathrm{~m}=19.5 \mathrm{~m}^{3}$
The rate of concrete for 2 agitator truck with 50 min per hour working: $3.5 \mathrm{~m}^{3}$ per hour
Time for placing the concrete $=\frac{\text { concrete Quantity }}{\text { concrete quantity in one truck } \times \text { working hour }}=\frac{19.5 \mathrm{~m}^{3}}{3.5 \times 22}=0.5$ hours

## Shutter panel - 1 ( 15 m length):

Table 3.23 Cycle time in invert lining for shutter panel-1 in PS

| S.N | Description | Quantity | Hours |
| :---: | :---: | :---: | :---: |
| 1 | Invert template | 1.5 | Hours |
| 2 | Invert template alignment | 1 | Hours |
| 3 | Concreting | 0.5 | Hours |
| 4 | Concrete setting | 20 | Hours |
| 5 | De-shuttering | 1 | Hours |
| 6 | Miscellaneous | 2 | Hours |
|  | Total cycle time for 15 m panel | 26 | Hours |

Shutter panel - 2 ( 15 m length):
Table 3.24 Cycle time in invert lining for shutter panel-2 in PS

| S.N | Description | Quantity | Hours |
| :---: | :---: | :---: | :---: |
| 1 | Invert template | 1.5 | Hours |
| 2 | Invert template alignment | 1 | Hours |
| 3 | Concreting | 0.5 | Hours |
| 4 | Concrete setting | 20 | Hours |
| 5 | De-shuttering | 1 | Hours |
| 6 | Miscellaneous | 2 | Hours |
|  | Total cycle time for 15 m panel | 26 | Hours |

## Time Schedule:

Cycle time for 30 m Invert lining $=52$ Hours
Progress per month =
$\underline{26(\text { working day per month) } \times 22 \text { (working hours per day) } \times 30 \mathrm{~m} \text { (length of lining in cycle) }}$
52 (weighted average cycle time in hours)
$=330 \mathrm{~m}$ per month
Invert lining time $=\frac{\text { Length of the tunnel }-1}{\text { working progress per month }}=\frac{(211+197+184+\quad) \mathrm{m}}{330 \mathrm{~m} \text { per month }}=2.5$ month $=75$ days

### 3.18 Cycle time in invert lining in Pressure shaft

Overt lining area $=9.79 \mathrm{~m}^{2}$
Concrete quantity in 15 m length $=9.79 \mathrm{~m}^{2} \times 15 \mathrm{~m}=146.5 \mathrm{~m}^{3}$
The rate of concrete for 2 agitator truck with 50 min per hour working: $3.5 \mathrm{~m}^{3}$ per hour
Time for placing the concrete $=\frac{\text { concrete Quantity }}{\text { concrete quantity in one truck } \times \text { working hour }}=\frac{146.5 \mathrm{~m}^{3}}{3.5 \times 22}=2.0$ hours

Shutter panel - 1(15m length):
Table 3.25 Cycle time in overt lining for shutter panel - 1 in PS

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Rail fixing | 2 | Hours |
| 2 | Shutter shifting | 3 | Hours |
| 3 | Shutter alignment | 3 | Hours |
| 4 | Bulk had fixing | 2 | Hours |
| 5 | Concreting | 2 | Hours |
| 6 | Concrete setting | 20 | Hours |
| 7 | De- shuttering | 2 | Hours |
| 8 | Miscellaneous | 3 | Hours |
|  | Total cycle time for 15 m pannel | $\mathbf{3 7}$ | Hours |

## Shutter panel - 2 ( 15 m length):

Table 3.26 Cycle time in overt lining for shutter panel-2 in PS

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :--- |
| 1 | Rail fixing | 2 | Hours |
| 2 | Shutter shifting | 3 | Hours |
| 3 | Shutter alignment | 3 | Hours |
| 4 | Bulk had fixing | 2 | Hours |
| 5 | Concreting | 2 | Hours |
| 6 | Concrete setting | 20 | Hours |
| 7 | De- shuttering | 2 | Hours |
| 8 | Miscellaneous | 3 | Hours |
|  | Total cycle time for 15 m pannel | $\mathbf{3 7}$ | Hours |

## Time Schedule:

Cycle time for 30 m Overt lining $=74$ Hours

26 (working day per month) $\times 22$ (working hours per day) $\times 30 \mathrm{~m}$ (length of lining in cycle)
74(weighted average cycle time in hours)
$=232 \mathrm{~m}$ per month
Overt lining time $=\frac{\text { Length of the pressure shaft }}{\text { working progress per month }}=\frac{(211+197+184+172) \mathrm{m}}{232 \mathrm{~m} \text { per month }}=3.29$ month $=100$ days

## Length in Pressure Shaft for different rock conditions:

Table 3.27 Length in Pressure Shaft for different rock conditions

|  | Good Rock(15\%) | Fair Rock(60\%) | Poor Rock(15\%) | V.Poor Rock(10\%) |
| :---: | :---: | :---: | :---: | :---: |
| Pressure Shaft -1 |  |  |  |  |
| 211 m - Length | 31.65 m | 126.6 m | 31.65 m | 21.1 m |
| Pressure Shaft -2 |  |  |  |  |
| 197 m - Length | 29.55 m | 118.2 m | 29.55 m | 19.7 m |
|  |  |  |  |  |
| Pressure Shaft -3 |  | 110.4 m | 27.6 m | 18.4 m |
| 184 m - Length | 27.6 m |  |  |  |
| Pressure Shaft -4 |  | 103.2 m | 25.8 m | 17.2 m |
| 172 m - Length | 25.8 m |  |  |  |

Table 3.28 Duration in Days for different rock conditions in PS - 1

| Pressure <br> Shaft-1 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 6 | 23 | 6 | 4 | 39 |
| Benching | 3 | 12 | 3 | 2 | 20 |
| Kerb | 8 | 11 | 8 | 2 | 29 |
| Overt | 8 | 11 | 8 | 2 | 29 |
| Invert | 8 | 16 | 8 | 3 | 35 |

Table 3.29 Duration in Days for different rock conditions in PS - 2

| Pressure <br> Shaft - 2 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 5 | 22 | 5 | 4 | 33 |
| Benching | 3 | 11 | 3 | 2 | 19 |
| Kerb | 2 | 11 | 2 | 1 | 16 |
| Overt | 2 | 11 | 2 | 1 | 16 |
| Invert | 4 | 15 | 4 | 2 | 25 |

Table 3.30 Duration in Days for different rock conditions in PS - 3

| Pressure <br> Shaft -3 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 2 | 20 | 2 | 1 | 25 |
| Benching | 2 | 11 | 2 | 1 | 16 |
| Kerb | 2 | 10 | 2 | 1 | 15 |
| Overt | 2 | 10 | 2 | 1 | 15 |
| Invert | 4 | 14 | 4 | 2 | 24 |

Table 3.31 Duration in Days for different rock conditions in PS - 4

| Pressure <br> Shaft -4 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 4 | 19 | 4 | 3 | 30 |
| Benching | 2 | 10 | 2 | 1 | 15 |
| Kerb | 2 | 9 | 2 | 1 | 14 |
| Overt | 2 | 9 | 2 | 1 | 14 |
| Invert | 3 | 13 | 3 | 2 | 21 |

Table 3.32 Activities details of Pressure shaft for Drill \& Blast method

| RHP- PS |  | Classic WBS Layout |  |  |  |  |  | 28-Apr-17 18:49 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Activity ID | Activity Name | Original Duration | $\begin{array}{\|r\|} \hline \text { Remaining } \\ \text { Duration } \\ \hline \end{array}$ | Schedule \% Complete | Start | Finish | $\begin{array}{c\|} \hline \text { Total } \\ \text { Float } \end{array}$ |  |
| RHP-PS |  | 137 | 137 | 0\% | 15-May-17 | 08-Sep-17 | 0 |  |
| ps1 |  | 137 | 137 | 0\% | 15-May-17 | 08-Sep-17 | 0 |  |
| A1030 Heading |  | 39 | 39 | 0\% | 15-May-17 | 15-Jun-17 | 0 |  |
| A1040 Benching |  | 20 | 20 | 0\% | 16-Jun-17 | 04-Jul-17 | 0 |  |
| A1060 Kerb |  | 29 | 29 | 0\% | 04-Jul-17 | 28-Jul-17 | 0 |  |
| A1070 Overt |  | 35 | 35 | 0\% | 28-Jul-17 | 28-Aug-17 | 0 |  |
| A1050 Invert |  | 29 | 29 | 0\% | 15-Aug-17 | 08-Sep-17 | 0 |  |
| ps2 |  | 113 | 113 | 0\% | 15-May-17 | 18-Aug-17 | 24 |  |
| A11 Heading |  | 36 | 36 | 0\% | 15-May-17 | 14-Jun-17 | 24 |  |
| A11 Benching |  | 19 | 19 | 0\% | 14-Jun-17 | 29-Jun-17 | 24 |  |
| A12 Kerb |  | 16 | 16 | 0\% | 30-Jun-17 | 14-Jul-17 | 24 |  |
| A12 Overt |  | 25 | 25 | 0\% | 14-Jul-17 | 04-Aug-17 | 24 |  |
| A11 Invert |  | 16 | 16 | 0\% | 04-Aug-17 | 18-Aug-17 | 24 |  |
| ps-3 |  | 98 | 98 | 0\% | 15-May-17 | 07-Aug-17 | 39 |  |
| + Heading |  | 24 | 24 | 0\% | 15-May-17 | 02-Jun-17 | 36 |  |
| + kerb |  | 15 | 15 | 0\% | 15-May-17 | 26-May-17 | 87 |  |
| $t$ overt |  | 24 | 24 | 0\% | 26-May-17 | 15-Jun-17 | 87 |  |
| t Invert |  | 15 | 15 | 0\% | 13-Jun-17 | 26-Jun-17 | 87 |  |
| + Benching |  | 16 | 16 | 0\% | 14-Jun-17 | 27-Jun-17 | 24 |  |
| ps4 |  | 98 | 98 | 0\% | 15-May-17 | 07-Aug-17 | 39 |  |
| Heading |  | 30 | 30 | 0\% | 15-May-17 | 08-Jun-17 | 39 |  |
| Benching |  | 15 | 15 | 0\% | 08-Jun-17 | 21-Jun-17 | 39 |  |
| kerb |  | 14 | 14 | 0\% | 26-Jun-17 | 07-Jul-17 | 39 |  |
| overt |  | 21 | 21 | 0\% | 07-Jul-17 | 26-Jul-17 | 39 |  |
| Invert |  | 14 | 14 | 0\% | 25-Jul-17 | 07-Aug-17 | 39 |  |



Fig 3.8 Network diagram of Pressure shaft in case of Drill \& Blast method


Fig 3.9 Cross-sectional view of Tailrace Tunnel

### 3.19 Cycle time calculation for different activities for heading work of Tailrace tunnel by Drill \& Blast method <br> $1^{\text {st }}$ Activity: Survey -0.5 hours

$2^{\text {nd }}$. Activity: Time required for drilling
$=\frac{\text { Total drilling length }}{\text { length per hour achieved by drilled jumbo }}=\frac{\text { no of holes } \times \text { length of each hole }}{\text { length per hour achieved by drilled jumbo }}=\frac{105 \times 3.2}{100 \mathrm{~m} / \mathrm{hr}}$
$=3.5$ hours
$3^{\text {rd }}$. Activity: Charging $=0.5$ hour
$4^{\text {th }}$.Activity: Blasting \& Defuming $=0.5$ hours
$5^{\text {th }}$. Activity: Time required for Mucking $=\frac{\text { Mucking Quantity }}{\text { productivity of loader }}$
Excavated quantity $=\frac{\mathrm{C} / \mathrm{S} \text { area of tunnel }}{\text { length of drill }}=\left(\frac{\pi \times d^{2}}{4}\right) \times$ length of drill
$=\frac{\pi \times 6.4725^{2}}{4} \times 3=98.7086 \mathrm{~m}^{3}$
$=$ Mucking Quantity $=98.7086 \times 1.2(20 \%$ as over-break quantity $)$
$=118.4503 \mathrm{~m}^{3}$ (mucking quantity will be more than the excavated quantity because there wil be some voids in the quantity)

Time required for mucking quantity $=\frac{\text { Mucking Qty }}{\text { Productivity of loader }}=\frac{118.4503 \mathrm{~m}^{3}}{65 \mathrm{~m}^{3}}$ per hour $=2.0$ hour
$6^{\text {th }}$. Activity: Scaling time -0.5 hours
$7^{\text {th }}$. Activity: Time required for shotcreting $=\frac{\text { Quantityty of shotcrete }}{\text { productivity of shotcret machine }}$
Quantityty of shotcrete $=$ Circumference of tunnel $\times$ thickness of shotcrete $\times$ length per cycle

1. For Good Rock Shotcreting $(5 \mathrm{~cm})=2 \pi \mathrm{r} \times 5 \mathrm{~cm} \times 3 \mathrm{~m}$

$$
\begin{aligned}
& =2 \pi \times 3.2362 \times 0.05 \times 3 \\
& =3.05 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =3.3550 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{3.3550 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=0.5$ hour
2. For Fair Rock Shotcreting $(10 \mathrm{~cm})=2 \pi \times 3.2362 \times 0.1 \times 3$

$$
\begin{aligned}
& =6.1000 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =6.7101 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Qty of shotcrete }}{\text { productivity of shotcrete }}=\frac{6.7101 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=1.0$ hour
3. For Poor Rock Shotcreting $(15 \mathrm{~cm})=2 \pi \times 3.2362 \times 0.15 \times 3$

$$
\begin{aligned}
& =9.1501 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =10.0651 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Qty of shotcrete }}{\text { productivity of shotcrete }}=\frac{10.0651 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=1.5$ hour
4. For Very Poor Rock Shotcreting $(20 \mathrm{~cm})=2 \pi \times 3.2362 \times 0.2 \times 3$

$$
\begin{aligned}
& =9.9382 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =12.2001 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{12.2001 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=2.0$ hour

## $8^{\text {th }}$. Activity: Rock bolt drilling \& fixing:

## 1. For Good \& Fair Rock:

Circumference of circle $=2 \pi \mathrm{r}$

$$
\begin{aligned}
& =\left(\frac{2 \pi r}{\text { distance of two rock bolt }}+1\right) \times 2=\left(\frac{2 \times \pi \times 3.2362}{2.3}+1\right) \times 2 \\
& =20 \text { no. in } 3 \mathrm{~m} \text { stretch of tunnel }
\end{aligned}
$$

Total drilling length of Rock bolt $=$ Total nos. of rock bolt $\times$ length of each rock bolt

$$
=20 \times 3 \mathrm{~m}=60 \mathrm{~m}
$$

Time required for drilling $=\frac{\text { total drilling length }}{\text { productivity of drill jumbo }}=\frac{60 \mathrm{~m}}{100 \text { per hour }}=0.5$ hour
Time required for fixing \& grouting $=($ no. of rock bolt $) \times($ time required for each rock bolt)

$$
=20 \times 3 \mathrm{~min}=60 \text { minute }=1.0 \text { hours }
$$

Total rock bolt drilling fixing time $=(0.5+1)$ hour $=1.5$ hour

## 2. For Poor \& Very Poor Rock:

Circumference of circle $=2 \pi \mathrm{r}$

$$
\begin{aligned}
& =\left(\frac{2 \pi r}{\text { distance of two rock bolt }}+1\right) \times 2=\left(\frac{2 \times \pi \times 3.2362}{1.7}+1\right) \times 2 \\
& =26 \text { no. in } 3 \mathrm{~m} \text { stretch of tunnel }
\end{aligned}
$$

Total drilling length of Rock bolt $=$ Total nos. of rock bolt $\times$ length of each rock bolt

$$
=26 \times 3 \mathrm{~m}=78 \mathrm{~m}
$$

Time required for drilling $=\frac{\text { total drilling length }}{\text { productivity of drill jumbo }}=\frac{78 \mathrm{~m}}{100 \mathrm{~m} \text { per hour }}=1.0$ hours
Time required for fixing \& grouting $=($ no. of rock bolt $) \times($ time required for each rock bolt)

$$
=26 \times 3 \mathrm{~min}=78 \text { minute }=1.0 \text { hours }
$$

Total rock bolt drilling fixing time $=(1.0+1.0)$ hour $=2.0$ hour

### 3.20 Cycle time for heading in Tailrace tunnel

3 m pull length per cycle to be considered for heading without rib and 1.5 m pull length to be considered for heading with rib

### 3.20.1 Cycle time for heading without rib support of Tailrace tunnel

Table 3.33 cycle time for heading without rib support of TRT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 3 | m |
| 2 | Heading c/s area | 52.44 | sqm |
| 3 | Excavation | 157.32 | cum |
| 4 | Survey | 0.5 | Hours |
| 5 | Drilling | 3.5 | Hours |
| 6 | Charging | 0.5 | Hours |
| 7 | Blasting\&defuming | 0.5 | Hours |
| 8 | Mucking | 2 | Hours |
| 9 | Scaling | 0.5 | Hours |
| 10 | shotcreting | 1 | Hours |
| 11 | Rockbolt drilling \& fixing | 1.5 | Hours |
|  | Total cycle time for 3 m pull length | 10 | Hours |
|  |  |  |  |
|  |  |  |  |

### 3.20.2 Cycle time for heading with rib support of Tailrace tunnel

Table 3.34 Cycle time for heading with rib support of TRT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull Length | 1.5 | m |
| 2 | Heading c/s area | 52.44 | sum |
| 3 | Excavation | 78.66 | cum |
| 4 | Survey | 0.5 | Hours |
| 5 | Drilling | 3.5 | Hours |
| 6 | Charging | 0.5 | Hours |
| 7 | Blasting\&defuming | 0.5 | Hours |
| 8 | Mucking | 2 | Hours |
| 9 | Scaling | 0.5 | Hours |
| 10 | Shotcreting | 2 | Hours |
| 11 | Rockbolt drilling \& fixing | 2 | Hours |
| 12 | Rib erection | 2.5 | Hours |
| 13 | Lagging fixing | 2 | Hours |
| 14 | Stopper fixing\&Back fill concrete | 3 | Hours |
|  | Total cycle time per 1.5 m pull length | $\mathbf{1 9}$ | Hours |
|  | Total cycle time per 3m pull length | 38 | Hours |
|  |  |  |  |
|  |  |  |  |
|  |  |  |  |

## Time Schedule:

Among the total excavation $90 \%$ is considered as without rib supporting and $10 \%$ as with rib supporting

Weighted average cycle time $=(10.0 \times 0.9)+(38 \times 0.1)=13$ hours per 3 m pull length
Progress per month $=\frac{(26(\text { working day per month }) \times 22(\text { working hours per day }) \times 3 \mathrm{~m} \text { pull length })}{13.0(\text { weighted cycle time in hours })}$
$=132 \mathrm{~m}$ per month
Time required for completion of Heading work $=\frac{\text { Length of Tail Race Tunnel }}{\text { Work progress per month }}$
$=\frac{(502+490+475+460) \mathrm{m}}{(132 \mathrm{~m} \text { per month })}$
$=14.5$ month $=435$ days

### 3.21 Cycle time calculation for benching of Tailrace tunnel by Drill \& Blast method

$1^{\text {st }}$. Activity: Surveying time -0.5 hours
2nt. Activity: Drilling time
$=\frac{\text { Total drilling length }}{\text { length per hour achieved by drilled jumbo }}=\frac{(\text { no of drill holes }) \times(\text { length of each hole })}{\text { length per hour achieved by drill jumbo }}=\frac{47 \times 3.2}{100}$
$=1.5$ hour
$3^{\text {rd }}$.Activity: Charging time $=0.5$ hour
$4^{\text {th }}$. Activity: Blasting \& Defuming $=0.5$ hours
$5^{\text {th }}$. Activity: Mucking time $=\frac{\text { Mucking quantity }}{\text { productivity of loader }}$
Mucking quantity $=\mathrm{C} / \mathrm{S}$ area of tunnel $\times$ length of drill
$=\left(\frac{\pi \times d^{2}}{4}\right) \times$ drill length $=\left(\frac{\pi \times 3.1735^{2}}{4}\right) \times 3 \mathrm{~m}=23.7294 \mathrm{~m}^{3}$
Mucking quantity $=23.7294 \times 1.2(20 \%$ as over-break quantity $)$
$=28.4753 \mathrm{~m}^{3}$ (mucking qty will be more than the excavated quantity because there wil be some voids in the quantity)

Time required for mucking quantity $=\frac{\text { Mucking quantity }}{\text { Productivity of loader }}=\frac{28.4753 \mathrm{~m}^{3}}{65 \mathrm{~m}^{3}}$ per hour $=0.5$ hour $6^{\text {th }}$. Activity: Scaling time $=0.5$ hour
$7^{\text {th }}$.Activity: Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcret machine }}$
Quantityty of shotcrete $=$ Circumference of tunnel $\times$ thickness of shotcrete $\times$ length per cycle

1. For Good Rock Shotcreting $(5 \mathrm{~cm})=2 \pi \mathrm{r} \times 5 \mathrm{~cm} \times 3 \mathrm{~m}$

$$
\begin{aligned}
& =2 \pi \times 1.5862 \times 0.05 \times 3 \\
& =1.4949 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =1.6444 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{1.6444 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=0.5$ hours
2. For Fair Rock Shotcreting $(10 \mathrm{~cm})=2 \pi \times 1.5862 \times 0.1 \times 3$
$=2.9899 \mathrm{~m}^{3} \times(1.1)(10 \%$ as rebound $)$
$=3.2889 \mathrm{~m}^{3}$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{3.2889 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=0.5$ hours
3. For Poor Rock Shotcreting $(15 \mathrm{~cm})=2 \pi \times 1.5862 \times 0.15 \times 3$

$$
\begin{aligned}
& =4.4848 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =4.9333 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{4.9333 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=1.0$ hour
4. For Very Poor Rock Shotcreting $(20 \mathrm{~cm})=2 \pi \times 1.5862 \times 0.2 \times 3$

$$
\begin{aligned}
& =5.9798 \mathrm{~m}^{3} \times(1.1)(10 \% \text { as rebound }) \\
& =6.5778 \mathrm{~m}^{3}
\end{aligned}
$$

Time required for shotcreting $=\frac{\text { Quantity of shotcrete }}{\text { productivity of shotcrete }}=\frac{6.5778 \mathrm{~m}^{3}}{6 \mathrm{~m}^{3} \text { per hour }}=1.0$ hours

### 3.22 Cycle time for benching without rib support of Tailrace tunnel

Table 3.35 Cycle time for benching without rib support of TRT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull Length | 3 | m |
| 2 | Benching c/s area | 23.21 | sqm |
| 3 | Excavation | 69.63 | cum |
| 4 | Survey | 0.5 | Hours |
| 5 | Drilling | 1.5 | Hours |
| 6 | Charging | 0.5 | Hours |
| 7 | Blasting\&defuming | 0.5 | Hours |
| 8 | Mucking | 0.5 | Hours |
| 9 | Scaling | 0.5 | Hours |
| 10 | Shotcreting | $\mathbf{0 . 5}$ | Hours |
| 11 | Total cycle time for 3m pull length | 4.5 | Hours |
|  |  |  |  |
|  |  |  |  |

### 3.22.1 Cycle time for benching with rib support of Tailrace tunnel

Table 3.36 Cycle time for benching with rib support of TRT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 1.5 | m |
| 2 | Benching c/s area | 23.21 | sqm |
| 3 | Excavation | 34.81 | cum |
| 4 | Survey | 0.5 | Hours |
| 5 | Drilling | 1.5 | Hours |
| 6 | Chrging | 0.5 | Hours |
| 7 | Blasting\&defuming | 0.5 | Hours |
| 8 | Mucking | 0.5 | Hours |
| 9 | Scaling | 0.5 | Hours |
| 10 | Shotcreting | 1 | Hours |
| 12 | Rib erection | 2 | Hours |
| 13 | Lagging fixing | $\mathbf{2 . 5}$ | Hours |
| 14 | Backfill concreting | $\mathbf{2}$ | Hours |
|  | Total cycle time for 1.5 m pull length | 11.5 | Hours |
|  | Total cycle time for 3 m pull length | 23 | Hours |
|  |  |  |  |

## Time Schedule:

Among the total excavation $90 \%$ is considered as without rib supporting and $10 \%$ as with rib supporting

Weighted average cycle time $=(4.5 \times 0.9)+(23 \times 0.1)=6.35$ hours per 3 m pull length
Progress per month $=\frac{26(\text { working day per month }) \times 22(\text { working hours per day }) \times 3 \mathrm{~m}(\text { pull length })}{6.35(\text { Hour per } 3 \mathrm{~m} \text { pull })}$
$=270 \mathrm{~m}$ per month
Time required for completion of Benching work $=\frac{\text { Length of Tail Race Tunnel }}{\text { Work progress per month }}$
$=\frac{(502+490+475+46) \mathrm{m}}{(270 \mathrm{~m} \text { per month })}$
$=7.13$ month $=204$ days

### 3.23 Cycle time in kerb lining of Tailrace tunnel

Kerb lining area $=1.9 \mathrm{~m}^{2}$
Concrete quantity in 15 m length $=2 \times 1.9 \mathrm{~m}^{2} \times 15 \mathrm{~m}=57 \mathrm{~m}^{3}$
The rate of concrete for 2 agitator truck with 50 min per hour working : $3.5 \mathrm{~m}^{3}$ per hour

Time for placing the concrete $=\frac{\text { concrete Quantity }}{\text { concrete quantity in one truck } \times \text { working hour }}=\frac{57 \mathrm{~m}^{3}}{3.5 \times 22}=1.0$ hours

## Shutter panel - 1 ( $\mathbf{1 5} \mathbf{m}$ length):

Table 3.37 Cycle time in kerb lining for shutter panel-1 of TRT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :--- |
| 1 | Kerb shutter | 2 | Hours |
| 2 | Shutter alignment | 2 | Hours |
| 3 | Concreting | 1 | Hours |
| 4 | Concrete setting | 20 | Hours |
| 5 | De- shuttering | 1 | Hours |
| 6 | Miscellaneous | 2 | Hours |
|  | Total cycle time for 15 m panel | 28 | Hours |

## Shutter panel - 2 ( $\mathbf{1 5} \mathbf{m}$ length):

Table 3.38 Cycle time in kerb lining for shutter panel-2 of TRT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :--- |
| 1 | Kerb shutter | 2 | Hours |
| 2 | Shutter alignment | 2 | Hours |
| 3 | Concreting | 1 | Hours |
| 4 | Concrete setting | 20 | Hours |
| 5 | De- shuttering | 1 | Hours |
| 6 | Miscellaneous | 2 | Hours |
|  | Total cycle time for 15 m panel | 28 | Hours |

## Time Schedule:

Cycle time for 30 m Kerb concreting $=56$ Hours
Progress per month $=$
$\frac{26(\text { working day per month) } \times 22(\text { working hours per day) } \times 30 \quad \text { (length of lini } \quad \text { in one cycle) }}{56(\text { weighted average cycle time in hours) }}$
$=306 \mathrm{~m}$ per month
Kerb concreting time $=\frac{\text { Length of the pressure shaft }}{\text { working progress per month }}=\frac{(502+490+475+46) \mathrm{m}}{306 \mathrm{~m} \text { per month }}=6.3$ month $=190$ days

### 3.24 Cycle time in Invert lining in Tailrace tunnel

Invert lining area $=2.2 \mathrm{~m}^{2}$
Concrete quantity in 15 m length $=2.2 \mathrm{~m}^{2} \times 15 \mathrm{~m}=33 \mathrm{~m}^{3}$
The rate of concrete for 2 agitator truck with 50 min per hour working : $3.5 \mathrm{~m}^{3}$ per hour Time for placing the concrete $=\frac{\text { concrete Quantity }}{\text { concrete quantity in one truck } \times \text { working hour }}=\frac{33 \mathrm{~m}^{3}}{3.5 \times 22}=0.5$ hours

## Shutter panel - 1 ( 15 m length):

Table 3.39 Cycle time in invert lining for Shutter panel-1 in TRT

| S.N | Description | Quantity | Hours |
| :---: | :---: | :---: | :---: |
| 1 | Invert template | 1.5 | Hours |
| 2 | Invert template alignment | 1 | Hours |
| 3 | Concreting | 0.5 | Hours |
| 4 | Concrete setting | 20 | Hours |
| 5 | De-shuttering | 1 | Hours |
| 6 | Miscellaneous | 2 | Hours |
|  | Total cycle time for 15 m panel | 26 | Hours |

Shutter panel - 2 ( 15 m length):
Table 3.40 Cycle time in invert lining for Shutter panel - 2 in TRT

| S.N | Description | Quantity | Hours |
| :---: | :---: | :---: | :---: |
| 1 | Invert template | 1.5 | Hours |
| 2 | Invert template alignment | 1 | Hours |
| 3 | Concreting | 0.5 | Hours |
| 4 | Concrete setting | 20 | Hours |
| 5 | De-shuttering | 1 | Hours |
| 6 | Miscellaneous | 2 | Hours |
|  | Total cycle time for 15 m panel | 26 | Hours |

## Time Schedule:

Cycle time for 30 m Invert concreting $=52$ Hours
Progress per month $=$
$\underline{26(\text { working day per month) } \times 22 \text { (working hours per day) } \times 30 \mathrm{~m} \text { (length of lining in one cycle) }}$
52(weighted average cycle time in hours)
$=330 \mathrm{~m}$ per month
Invert concreting time $=\frac{\text { Length of Tailrace Tunnel }}{\text { working progress per month }}=\frac{(502+490+475+\quad \mathrm{m}}{330 \mathrm{~m} \text { per month }}=5.8$ month $=$ 175 days

### 3.25 Cycle time in overt lining in Tailrace tunnel:

Overt lining area $=12.22 \mathrm{~m}^{2}$
Concrete quantity in 15 m length $=12.22 \mathrm{~m}^{2} \times 15 \mathrm{~m}=183.3 \mathrm{~m}^{3}$
The rate of concrete for 2 agitator truck with 50 min per hour working : $3.5 \mathrm{~m}^{3}$ per hour Time for placing the concrete $=\frac{\text { concrete Quantity }}{\text { concrete quantity in one truck } \times \text { working hour }}=\frac{183.3 \mathrm{~m}^{3}}{3.5 \times 22}=2.5$ hours

## Shutter panel - 1 ( 15 m length):

Table 3.41 Cycle time for overt lining for Shutter panel - 1 in TRT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :--- |
| 1 | Rail fixing | 2 | Hours |
| 2 | Shutter shifting | 3 | Hours |
| 3 | Shutter alignment | 3 | Hours |
| 4 | Bulk had fixing | 2 | Hours |
| 5 | Concreting | 2.5 | Hours |
| 6 | Concrete setting | 20 | Hours |
| 7 | De- shuttering | 2 | Hours |
| 8 | Miscellaneous | 3 | Hours |
|  | Total cycle time for 15 m pannel | $\mathbf{3 7 . 5}$ | Hours |

## Shutter panel - 2 ( 15 m length):

Table 3.42 Cycle time for overt lining for Shutter panel-2 in TRT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :--- |
| 1 | Rail fixing | 2 | Hours |
| 2 | Shutter shifting | 3 | Hours |
| 3 | Shutter alignment | 3 | Hours |
| 4 | Bulk had fixing | 2 | Hours |
| 5 | Concreting | 2.5 | Hours |
| 6 | Concrete setting | 20 | Hours |
| 7 | De- shuttering | 2 | Hours |
| 8 | Miscellaneous | 3 | Hours |
|  | Total cycle time for 15 m pannel | $\mathbf{3 7 . 5}$ | Hours |

## Time Schedule:

Cycle time for 30 m Overt concreting $=75$ Hours
Progress per month $=$

26 (working day per month) $\times 22$ (working hours per day) $\times 30 \mathrm{~m}$ (length of lining in one cycle)
75 (weighted average cycle time in hours)
$=228 \mathrm{~m}$ per month
Overt concreting time $=\frac{\text { Length of Tailrace Tunnel }}{\text { working progress per month }}=\frac{(502+490+475 \quad \mathrm{~m}}{228 \mathrm{~m} \text { per month }}=8.5 \mathrm{month}=$ 255 days

Table 3.43 Length of different rock conditions in TRT

|  | $\begin{aligned} & \text { Good Rock } \\ & (10 \%) \end{aligned}$ | Fair Rock (60\%) | $\begin{gathered} \text { Poor Rock } \\ (10 \%) \end{gathered}$ | Very Poor <br> Rock (10\%) |
| :---: | :---: | :---: | :---: | :---: |
| Tailrace <br> Tunnel-1 <br> Length $=502$ <br> m | 75.3 m | 301.2 m | 75.3 m | 50.2 m |
| Tailrace <br> Tunnel-2 <br> Length $=490$ <br> m | 73.5 m | 294 m | 73.5 m | 49 m |
| ```Tailrace Tunnel-3 Length \(=475\) m``` | 71.25 m | 285 m | 71.25 m | 47.5 m |
| Tailrace <br> Tunnel-4 <br> Length $=460$ | 69 m | 276 m | 69 m | 46 m |


| m |  |  |  |  |
| :--- | :--- | :--- | :--- | :--- |

Table 3.44 Time duration for different rock conditions in TRT- 1

| TRT - 1 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 18 | 71 | 18 | 12 | 119 |
| Benching | 8 | 32 | 8 | 6 | 54 |
| Kerb | 7 | 27 | 7 | 5 | 46 |
| Overt | 7 | 27 | 7 | 5 | 46 |
| Invert | 10 | 40 | 10 | 7 | 67 |

Table 3.45 Time duration for different rock conditions in TRT - 2

| TRT - 2 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 17 | 69 | 17 | 11 | 114 |
| Benching | 8 | 33 | 8 | 5 | 54 |
| Kerb | 7 | 27 | 7 | 4 | 45 |
| Overt | 7 | 27 | 7 | 4 | 45 |
| Invert | 10 | 38 | 10 | 6 | 64 |

Table 3.46 Time duration for different rock conditions in TRT - 3

| TRT - 3 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 17 | 67 | 17 | 11 | 112 |
| Benching | 8 | 32 | 8 | 5 | 53 |
| Kerb | 6 | 26 | 6 | 4 | 42 |
| Overt | 6 | 26 | 6 | 4 | 42 |
| Invert | 9 | 37 | 9 | 6 | 61 |

Table 3.47 Time duration for different rock conditions in TRT - 4

| TRT - 4 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 16 | 65 | 16 | 11 | 108 |
| Benching | 8 | 31 | 8 | 5 | 52 |
| Kerb | 6 | 25 | 6 | 4 | 41 |
| Overt | 6 | 25 | 6 | 4 | 41 |


| Invert | 9 | 36 | 9 | 6 | 60 |
| :---: | :---: | :---: | :---: | :---: | :---: |

Table 3.48 Activities details of TRT for Drill \& Blast method

| RHP- TRT |  | Classic WBS Layout |  |  |  | 28-Apr-17 18:50 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Activity ID | Activity Name | $\begin{aligned} & \text { Original } \\ & \text { Duration } \end{aligned}$ | $\begin{array}{\|r\|} \hline \text { Remaining } \\ \text { Duration } \end{array}$ | Schedule \% Complete | Start | Finish | $\begin{aligned} & \hline \text { Total } \\ & \text { Float } \end{aligned}$ |  |
| RHP- TRT |  | 252 | 252 | 0\% | 15-May-17 | 18-Dec-17 | 0 |  |
| TRT1 |  | 252 | 252 | 0\% | 15-May-17 | 18-Dec-17 | 0 |  |
| A1030 Heading |  | 119 | 119 | 0\% | 15-May-17 | 24-Aug-17 | 0 |  |
| A1040 Benching |  | 54 | 54 | 0\% | 24-Aug-17 | 10-Oct-17 | 0 |  |
| A1060 Kerb |  | 46 | 46 | 0\% | 11-Sep-17 | 19-Oct-17 | 0 |  |
| A1070 Overt |  | 67 | 67 | 0\% | 19-Oct-17 | 18-Dec-17 | 0 |  |
| A1050 Invert |  | 46 | 46 | 0\% | 07-Nov-17 | 15-Dec-17 | 1 |  |
| TRT2 |  | 244 | 244 | 0\% | 15-May-17 | 11-Dec-17 | 8 |  |
| A11 Heading |  | 114 | 114 | 0\% | 15-May-17 | 21-Aug-17 | 8 |  |
| A11 Benching |  | 54 | 54 | 0\% | 21-Aug-17 | 05-Oct-17 | 8 |  |
| A12 Kerb |  | 45 | 45 | 0\% | 06-Sep-17 | 16-Oct-17 | 8 |  |
| A12 Overt |  | 64 | 64 | 0\% | 16-Oct-17 | 08-Dec-17 | 8 |  |
| A11 Invert |  | 45 | 45 | 0\% | 01-Nov-17 | 11-Dec-17 | 8 |  |
| TRT3 |  | 238 | 238 | 0\% | 15-May-17 | 05-Dec-17 | 14 |  |
| t Heading |  | 112 | 112 | 0\% | 15-May-17 | 17-Aug-17 | 10 |  |
| + Benching |  | 53 | 53 | 0\% | 21-Aug-17 | 04-Oct-17 | 8 |  |
| + kerb |  | 42 | 42 | 0\% | 06-Sep-17 | 12-Oct-17 | 14 |  |
| $t$ overt |  | 61 | 61 | 0\% | 12-Oct-17 | 04-Dec-17 | 14 |  |
| $t$ Invert |  | 42 | 42 | 0\% | 30-Oct-17 | 05-Dec-17 | 14 |  |
| TRT4 |  | 230 | 230 | 0\% | 15-May-17 | 28-Nov-17 | 22 |  |
| Heading |  | 108 | 108 | 0\% | 15-May-17 | 15-Aug-17 | 22 |  |
| Benching |  | 52 | 52 | 0\% | 15-Aug-17 | 28-Sep-17 | 22 |  |
| kerb |  | 41 | 41 | 0\% | 31-Aug-17 | 05-Oct-17 | 22 |  |
| overt |  | 60 | 60 | 0\% | 06-Oct-17 | 27-Nov-17 | 22 |  |
| Invert |  | 41 | 41 | 0\% | 24-Oct-17 | 28-Nov-17 | 22 |  |



Fig 3.10 Network diagram for Tailrace tunnel in case of Drill \& Blast method

### 3.26 Cost estimation of underground work in Diversion tunnel by Drill \& Blast method

ITEM: Excavation for tunnel in the case of Diversion Tunnel by heading and benching.

| DATA - Size of tunnel assumed (finished section) | 12.345 m dia |
| :--- | :---: |
| Shape of tunnel assumed for excavation | Horse-shoe shaped |
| Height of tunnel assumed (finished section) | 12.345 m dia |
| Length of DT- 1 | 472 m |


| Length of DT- 2 | 552 m |
| :--- | :---: |
| Thickness of lining | 1.0 m |
| Diameter of tunnel upto pay line for excavation | 12.345 m |
| Distance of dump yard from face | Average 1 km |
| Haulage of excavated muck | By dumper |

Consideration for $\mathbf{3} \mathbf{m}$ pull length:

## Checking alignment and marking hole locations:

Use drilling jumbo for 1 hour for marking hole locations.

## Drilling holes.

The depth of hole for 3.0 m pull is considered at 2.0 m

| Heading portion |  |
| :--- | :---: |
| Area of excavation upto payline | $82.6734 \mathrm{~m}^{2}$ |
| Drilling depth | 2.0 m |
| No. of holes considering 2.0 holes per $\mathrm{m}^{2}$ | $(82.6734 \times 2.0)$ |
| Drilling depth for 165 holes | $(165 \times 2.0 \times 1.1)$ |


| Benching portion |  |
| :--- | :---: |
| Area of excavation upto payline | $40.2379 \mathrm{~m}^{2}$ |
| Drilling depth | 2.0 m |
| No. of holes considering 2.0 holes per $m^{2} \quad(40.2379 \times 2.0)$ | 81 Nos |
| Drilling depth for 80 holes $\quad(80 \times 2.0 \times 1.1)$ | 176.0 m |
| Total depth of drilling $\quad(363+176)$ | 593.0 m |
| Average rate of drilling per hour per jack hammer | 5 m |
| Time for 4 jack hammer with pusher leg for drilling | 8 hour |
| Time for 1 air compresser 15 cmm <br> hammer for air supply to 4 jack | 8 hour |
| Time for drilling jumbo for drilling | 8 hour |


| Loading explosive and blasting |  |
| :--- | :--- |
| Total area of excavation | $123 \mathrm{~m}^{2}$ |
| Depth of pull per blast for 2.0 m deep holes $\quad 3.0 \mathrm{~m}$ |  |
| Quantity of in-situ excavation per blast $\mathbf{( 1 2 3 \times 3 . 0 )}$ | $\mathbf{3 6 9} \mathbf{m}^{\mathbf{3}}$ |
| Quantity of explosive small dia per blast $@ 0.8 \mathrm{~kg} \mathrm{per} \mathrm{m}^{3}(369 \times 0.8$ | 295.2 kg |
| Quantity of explosive for secondary blasting @ $10 \%$ | 29.52 kg |
| Quantity of delay detonators per blast $\quad(165+81)$ | 246 Nos. |
| Quantity of electric e detonators for secondary blasting (LS) | 10 Nos. |
| Detonating fuse coil | 175 Rm |
| Time for drilling jumbo for loading explosive. $\quad(1.5+0.5)$ | 2.0 hours |

## Defuming and scaling loose materials:

Ventilation fan required in duct system at 300 m interval and are run for about 1 hour after each blast

| Mucking excavated rock |  |
| :--- | :--- |
| Quantity of muck per blast considering 20 \% bulkage for Heading <br> zone $(82.67 \times 1.2)$ | $99.204 \mathrm{~m}^{3}$ |
| Quantity of muck per blast considering 20 \% bulkage for Benching <br> zone $(40.23 \times 1.2)$ | $48.276 \mathrm{~m}^{3}$ |
| Capacity of dumper per load | $5 \mathrm{~m}^{3}$ |
| Quantity of muck per load considered under tunnel working <br> conditions | $4.5 \mathrm{~m}^{3}$ |


| Loading cycle time |  |
| :--- | :--- |
| Moving from pocket position and spotting | 1 minutes |
| Loading muck by convey mucker and work force | 20 minutes |
| Time for loading dumper to pass waiting point | 1 minutes |


| Cycle time of loading dumper per load of $4.5 \mathrm{~m}^{\mathbf{3}}$ | 22 minutes |
| :---: | :---: |
| Haulage cycle time |  |
| Running time from loading point to dump yard at average 10 km per hour | 6 minutes |
| Turning and unloading | 2 minutes |
| Retur trip to waiting point @ average 15 km per hour | 4 minutes |
| Waiting time for spotting | 9 minutes |
| Cycle time for haulage per load of $4.5 \mathrm{~m}^{\mathbf{3}}$ | 21 minutes |


| Round trip cycle time of dumper | $\mathbf{4 5}$ minutes |
| :--- | :--- |
| Quantity of muck disposal per hour per dumper | $6 \mathrm{~m}^{3}$ |
| Time for 2 dumper for conveying muck @ $12 \mathrm{~m}^{3}$ per hour | 6 hours |
| Time for convey mucker and labour force for loading | 7 hours |


| Overall cycle time |  |
| :--- | :--- |
| Survey | 0.5 hours |
| Drilling | 5.0 hours |
| Charging | 1.0 hours |


| Blasting \& defuming | 0.5 hours |
| :--- | :---: |
| Mucking | 3.0 hours |
| Scaling | 1.0 hour |
| Shotcreting in Good Rock $(5 \mathrm{~cm})$ | 0.5 hour |
| Shotcreting in Fair Rock $(10 \mathrm{~cm})$ | 1.0 hour |
| Rockbolt drilling \& fixing(Good \& Fair Rock) | 2.0 hour |

Total cycle of excavation \& supporting per blast of $\mathbf{3 . 0} \mathbf{m}$ length : $\mathbf{1 4 . 5}$ hours

| Requirement of materials $\quad(295.2+29.5)$ |  |
| :--- | :--- |
| Explosive small dia $\quad(165+81)$ | 324.7 kg |
| Elecic short delay detonators | 246 Nos |
| Electric detonators for secondary blasting | 10 Nos |
| Fuse coil | 175 Rm |


| Requirement of machinery |  |
| :--- | :--- |
| Deploy drilling jumbo for various opetrations of excavation (marking 1 <br> hr + drilling $5 \mathrm{hr}+$ loading explosive 2 hrs + miscellaneous work 1 hrs ) | 9 hours |
| Deploy air compressor 15 cmm for air supply to 4 jack hammers | 8 hours |
| Deploy 10 hp pump for water pusher leg for drilling work | 8 hours |
| Deploy for defuming <br> $; 2$ hours |  |
| Deploy convey mucker for loading excavated rock | 7 hours |
| Deploy 2 dumper for conveying muck | 7 hours |


| Requirement of workforce (other than machinery crew) |  |
| :--- | :--- |
| Surveyer |  |
| For checking alignment and marking hole locations for drilling | 1 Nos |
| Foreman for supervising drilling of holes and other operations | 1 Nos |
| Fitter/Mechanic | 2 Nos |
| For extending air / water lines | 2 Nos |
| Blaster (Licenced) | 2 Nos |
| Helper Blasting | 2 Nos |
| Hammerman foe scaling |  |
| Khalasi | 4 Nos |
| For pushing muck from header portion | 4 Nos |
| Foe mucking shift |  |
| Heavy mazdoor | 8 Nos |
| For mucking shift | 4 Nos |
| Light mazdoor |  |
| For cleaning \& miscellaneous work |  |


| Use rate of materials |  |  |
| :--- | :--- | :--- |
| Cost of drill rod 2.5 m long @ | 7175.0 per Nos | 7175.0 |
| Life of drill rod with reconditioning |  | 150 m |
| Use rate of drill rod per Rm drilling | (cost per life) | 47.83 |
| Length of air and water hose assumed |  | 25 m each |
| Cost of 25 mm dia air hose 25 m @ | 200.0 per Rm | 5000.0 |
| Life of air hose |  | 800 .hours |
| Use rate of air hose per hour | (cost per life) | 6.25 |
| Cost of water hose 25 m each @ | 185.00 per Rm | 4625.00 |
| Life of water hose | (cost per life) | 800 hours |
| Use rate of water hose per hour | (cost per life) | 5.78 |

## RATE ANALYSIS

UNIT
: $\mathbf{3 6 9}$ m $^{3}$

## A. MATERIALS

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| 1 | Small dia explosive | kg | 324.7 | 60 | 19482 |
| 2 | Delay detonators | Nos | 246 | 20 | 4920 |
| 3 | Electric detonator | Nos | 10 | 12 | 120 |
| 4 | Detonating fuse coil | Rm | 175 | 9 | 1575 |
| 5 | Use rate of drill rod 2.0 m long | Rm | 539 | 47.83 | 25780.37 |
|  | Reconditioning charges @ 10\% |  |  |  | 2578.037 |
| 6 | Use rate of air hose | Hour | 32 | 6.25 | 200 |
| 7 | Use rate of water hose | Hour | 32 | 5.78 | 184.96 |
| 8 | Sundries ( paint / template etc ) | LS | 9 | 44 | 396 |
|  |  |  |  | Total | 55236.367 |


| Add for small Tools and Plants | @ 1 | 552.3636 |
| :--- | :--- | :--- |
| Add for Contractor's Profit | @ $10 \%$ | 5523.6367 |
| Add for Contractor's Overheads | @ $5 \%$ | 2761.8183 |
| Total cost of Material |  | $\mathbf{6 4 0 7 4 . 1 8 5 6}$ |

## B. MACHINERY:

| S.N | Description | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Drilling jumbo | Hour | 9 | 370 | 3330 |
|  | Fuel charges | Hour | 9 | 41 | 369 |
| 2 | Air compressor 15 cmm | Hour | 8 | 119 | 952 |
|  | Fuel charges | Hour | 8 | 800 | 6400 |
| 3 | Jack hammer ( $4 \times 8$ hrs $)$ | Hour | 32 | 16 | 512 |
|  | Fuel charges | Hour | 32 | 8 | 256 |
| 4 | Pusher leg | Hour | 32 | 9 | 288 |
|  | Fuel charges | Hour | 32 | 6 | 192 |
| 5 | Convey mucker | Hour | 7 | 740 | 5180 |
|  | Fuel charges | Hour | 7 | 223 | 1561 |
| 6 | Dumper ( 2 x 6.5 hrs ) | Hour | 13 | 548 | 7124 |
|  | Fuel charges | Hour | 13 | 381 | 4953 |
| 7 | Pump 10 hp | Hour | 8 | 5 | 40 |
|  | Fuel charges | Hour | 8 | 64 | 512 |
| 8 | Ventilation fans 20 hp (2 x 1 hr x 2) | Hour | 4 | 6 | 24 |
|  | Fuel charges | Hour | 4 | 128 | 512 |
| 9 | Sundries (explosive van / magazine ) | LS | 10 | 44 | 440 |
|  |  |  |  | Total | 32645 |


| Add for small Tools and Plants | $@$ 1\% | 326.4 |
| :--- | :--- | :--- |
| Add for Contractor's Profit | $@ 10 \%$ | 3264.5 |
| Add for Contractor's Overheads | $@, 5 \%$ | 1632.25 |
| Total hire charges of Machinery |  | $\mathbf{3 7 8 6 8 . 2}$ |

## C. LABOUR:

| S.N | Description | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Crew for Drilling jumbo | Hour | 9 | 101 | 909 |
| 2 | Crew for Air compressor | Hour | 8 | 101 | 808 |
| 3 | Crew for Jack hammer | Hour | 32 | 188 | 6016 |
| 4 | Crew for Convey mucker | Hour | 7 | 101 | 707 |
| 5 | Crew for Dumper | Hour | 13 | 121 | 1573 |
| 6 | Crew for Pump | Hour | 8 | 45 | 360 |
| 7 | Crew for Ventilation fan | Hour | 4 | 16 | 64 |
| 8 | Surveyor | Day | 1 | 284.73 | 284.73 |
| 9 | Foreman | Day | 1 | 276.73 | 276.73 |
| 10 | Fitter / Mechanic | Day | 2 | 254.73 | 509.46 |
| 11 | Blaster ( Licensed ) | Day | 2 | 243.23 | 486.46 |
| 12 | Helper blasting | Day | 4 | 239.73 | 958.92 |
| 13 | Hammerman 2 Nos | Day | 2 | 241.73 | 483.46 |
| 14 | Maistry 1 in each shift | Day | 3 | 243.23 | 729.69 |
| 15 | Khalasi |  |  |  |  |
|  | for pushing muck in heading portion | Day | 4 | 241.23 | 964.92 |
|  | for mucking shift 4 Nos | Day | 4 | 241.23 | 964.92 |
| 16 | Heavy mazdoor |  |  |  |  |
|  | for mucking shift 8 Nos | Day | 8 | 238.73 | 1909.84 |
|  | for other 2 shifts 2 No each shift | Day | 4 | 238.73 | 954.92 |
| 17 | Light mazdoor |  |  |  |  |
|  | for cleaning \& miscellaneous | Day | 3 | 238.23 | 714.69 |
|  | 年 |  |  | Total | 19675.74 |


| Add for small Tools and Plants | @ 1 \% | 196.7574 |
| :--- | :--- | :--- |
| Add for Contractor's Profit | @ 10\% | 1967.574 |
| Add for hidden cost on Labour | @ 15\% | 2951.331 |
| Add for additional hidden cost on labour | @ 10\% | 1967.574 |
| Add for Contractor's Overheads | Qotal cost of labour | 983 |
|  |  | $\mathbf{2 7 7 4 8 7}$ |

3.27 Abstract of cost details for 3 m Pull length in Diversion tunnel by Drill \& Blast method

| A.Cost of Materials | 64074.1856 |
| :--- | :--- |
| B.Hire charges of Machinery | 37868.2 |


| C.Cost of Labour |  | 27742.7634 |
| :---: | :---: | :---: |
| TOTAL |  | 129685.149 |
| Add for Air and Water line | @ 0.80 \% | 1037.4811 |
| Add for Ventilation | @ 6.0 \% | 7781.1089 |
| Add for Lighting | @ 1.80 \% | 2334.3326 |
| Add for Electrical sub-station / Demand charges | ( $3.80 \%$ | 4928.0356 |
| Add for other Enabling works | @ 1.70 \% | 2204.6475 |
| Total cost for | $369 \mathrm{~m}^{3}$ | 47970.7547 |


| Rate per $\boldsymbol{m}^{3}$ | 401.0047 |
| :--- | :--- |
| For 1 cycle ( $\mathbf{3} \mathbf{~ m}$ pull length) rate per $\boldsymbol{m}^{3}$ | $\mathbf{4 0 1 . 0 0 4 7}$ |
| Total length of DT- 1 | $\mathbf{4 7 2} \mathbf{~ m}$ |
| Total length of DT- 2 | $\mathbf{5 5 2} \mathbf{~ m}$ |


| $\mathbf{9 0} \%$ considered without rib support |  |
| :--- | :--- |
| Total length in case of without rib support in DT - 1 | 424.8 m |
| Total length in case of without rib support in DT - 2 | 496.8 m |


| Total cost in DT -1 | $\left(401.0047 \times 424.8 \mathrm{~m} \times 123 \mathrm{~m}^{2}\right)$ | $\mathbf{2 0 9 5 2 6 5 5 . 9 8}$ |
| :--- | :--- | :--- |
| Total cost in DT -2 | $\left(401.0047 \times 496.8 \mathrm{~m} \times 123 \mathrm{~m}^{2}\right)$ | $\mathbf{2 4 5 0 3 9 5 3 . 6}$ |

## Consideration for 1.5 m pull length:

## Checking alignment and marking hole locations:

Use drilling jumbo for 1 hour for marking hole locations.

## Drilling holes.

The depth of hole for 1.5 m pull is considered at 1.0 m

| Heading portion |  |  |
| :--- | :--- | :--- |
| Area of excavation upto payline |  | $82.6734 \mathrm{~m}^{2}$ |
| Drilling depth |  | 1.0 m |
| No. of holes considering 2.0 holes per $\mathrm{m}^{2}$ | $(82.6734 \times 2.0)$ | 165 Nos |
| Drilling depth for 165 holes | $\mathbf{( 1 6 5 \times \mathbf { 1 . 0 } \times \mathbf { 1 . 1 } )}$ | $\mathbf{1 8 1 . 5} \mathbf{~ m}$ |


| Benching portion |  |  |
| :--- | :--- | :--- |
| Area of excavation upto payline |  | $40.2379 \mathrm{~m}^{2}$ |
| Drilling depth |  | 1.0 m |
| No. of holes considering 2.0 holes per $\mathrm{m}^{2}$ | $(40.2379 \times 2.0)$ | 81 Nos |


| Drilling depth for 80 holes | $\mathbf{( 8 1 \times 1 . 0 \times \mathbf { 1 . 1 } )}$ | $\mathbf{8 9 . 1 ~ \mathbf { ~ m }}$ |
| :--- | :--- | :--- |
| Total depth of drilling | $\mathbf{( 1 8 1 . 5 + 8 9 . 1 )}$ | $\mathbf{2 7 0 . 1} \mathbf{~ m}$ |
| Average rate of drilling per hour per jack hammer |  | 5 m |
| Time for 4 jack hammer with pusher leg for drilling |  | 8 hours |
| Time for 1 air compresser 15 cmm for air supply to <br> 4 jack hammer | 8 hours |  |
| Time for drilling jumbo for drilling |  | 8 hours |
| Time for 10 hp pimp for pumping water to storage <br> tank |  | 8 hours |


| Loading explosive and blasting |  |  |
| :--- | :--- | :--- |
| Total area of excavation |  | $123 \mathrm{~m}^{2}$ |
| Depth of pull per blast forl.0 m deep holes | $\mathbf{( 1 2 3 \times 1 . 5 )}$ | 1.5 m |
| Quantity of in-situ excavation per blast | $\mathbf{1 8 4 . 5} \mathbf{m}^{\mathbf{3}}$ |  |
| Quantity of explosive small dia per blast $@$ a 0.8 kg <br> per $\mathrm{m}^{3}$ | $(184.5 \times 0.8)$ | 147.6 kg |
| Quantity of explosive for secondary blasting @ 10 <br> $\%$ |  | 14.76 kg |
| Quantity of delay detonators per blast | $(165+81)$ | 246 Nos. |
| Quantity of electric electric detonators for <br> secondary blasting (LS) |  | $10 \mathrm{Nos}$. |
| Detonating fuse coil |  | 450 Rm |
| Time for drilling jumbo for loading explosive. | $(1.5+0.5)$ | 2.0 hours |


| Overall cycle time |  |
| :--- | :--- |
| Survey | 0.5 hours |
| Drilling | 5.0 hours |
| Charging | 1.0 hours |
| Blasting \& defuming | 0.5 hours |
| Mucking | 3.0 hours |
| Scaling | 1.0 hours |
| Shotcreting in Poor Rock $(15 \mathrm{~cm})$ | 2.0 hours |
| Shotcreting in V.Poor Rock (20cm) | 2.5 hour |
| Rockbolt drilling \& fixing in (Poor \& V.Poor Rock) | 3.0 hour |
| Rib erection | 3.0 hour |
| Lagging fixing | 2.5 hour |
| Stopper fixing \& back fill concrete | 4.0 hour |
| Total cycle of excavation \& supporting per blast of 1.5 m length | $\mathbf{2 8 . 0}$ hour |
| Total cycle of excavation \& supporting per blast of 3.0 m length | $\mathbf{5 6 . 0}$ hours |


| Requirement of materials |  |  |
| :--- | :--- | :--- |
| Explosive small dia | $\mathbf{( 1 4 7 . 6 + 1 4 . 7 6 )}$ | $\mathbf{1 6 2 . 3 6} \mathbf{~ k g}$ |


| Elecic short delay detonators | $\mathbf{( 1 6 5 + 8 1 )}$ | $\mathbf{2 4 6}$ Nos |
| :--- | :--- | :--- |
| Electric detonators for secondary blasting |  | $\mathbf{1 0}$ Nos |
| Fuse coil |  | $\mathbf{4 5 0} \mathbf{~ R m}$ |

## RATE ANALYSIS

UNIT
$184.5 \mathrm{~m}^{3}$

## A. MATERIALS :

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| 1 | Small dia explosive | kg | 162.36 | 60 | 9741.6 |
| 2 | Delay detonators | Nos | 246 | 20 | 4920 |
| 3 | Electric detonator | Nos | 10 | 12 | 120 |
| 4 | Detonating fuse coil | Rm | 450 | 9 | 4050 |
| 5 | Use rate of drill rod 2.0 m long | Rm | 270.1 | 47.83 | 12918.888 |
|  | Reconditioning charges @ | $10 \%$ |  |  |  |
| 6 | Use rate of air hose | Hour | 32 | 6.25 | 1291.888 |
| 7 | Use rate of water hose | Hour | 32 | 5.78 | 184.96 |
| 8 | Sundries (paint / template etc ) | LS | 9 | 44 | 396 |
|  |  |  |  | Total | 33823.336 |

### 3.28 Abstract of cost details for 1.5 m Pull length in Diversion tunnel:

|  |  |  |  |  |
| :--- | :--- | :---: | :---: | :---: |
| A.Cost of Materials | 33823.336 |  |  |  |
| B.Hire charges of Machinery | 37868.2 |  |  |  |
| C.Cost of Labour | 27742.7634 |  |  |  |
| TOTAL |  |  |  | $\mathbf{9 9 4 3 4 . 2 9 9 4}$ |


| Add for Air and Water line | @ $0.80 \%$ | 795.4743 |
| :--- | :--- | :--- |
| Add for Ventilation | @ $6.0 \%$ | 5966.0579 |
| Add for Lighting | @ $1.80 \%$ | 1789.8173 |
| Add for Ele sub-station / Demand charges | @ $3.80 \%$ | 3778.5033 |
| Add for other Enabling works | $@ 1.70 \%$ | 1690.3830 |
| Total cost for | $\mathbf{1 8 4 . 5} \mathbf{m}^{\mathbf{3}}$ | $\mathbf{1 1 3 4 5 4 . 5 3 5 2}$ |


| Rate per $\boldsymbol{m}^{\mathbf{3}}$ | $\mathbf{6 1 4 . 9 2 9 7}$ |
| :--- | :--- |
| For 1 cycle (1.5 $\mathbf{~ m}$ pull length) rate per $\boldsymbol{m}^{\mathbf{3}}$ | $\mathbf{6 1 4 . 9 2 9 7}$ |
| Total length of DT- 1 | $\mathbf{4 7 2} \mathbf{~ m}$ |
| Total length of DT- 2 | $\mathbf{5 5 2} \mathbf{~ m}$ |
|  |  |


| 10 \% considered with rib support |  |
| :---: | :---: |
| Total length in case of with rib support in DT -1 | 47.2 m |
| Total length in case of with rib support in DT -2 | 55.2 m |
| Total cost in DT - $1 \quad\left(614.9297 \times 47.2 \mathrm{~m} \times 123 \mathrm{~m}^{2}\right)$ | 570035.866 |
| Total cost in DT - $2\left(614.9297 \times 55.2 \mathrm{~m} \times 123 \mathrm{~m}^{2}\right)$ | 175126.691 |
| Total cost in Excavation for DT- $1 \quad(\mathbf{2 0 9 5 2 6 5 5 . 9 8}+\mathbf{3 5 7 0 0 3 5 . 8 6 6 )}$ | 4522691.85 |
| Total cost in Excavation for DT- 2 (24503953.6+4175126.691) | 8679080.29 |

### 3.29 Cost calculation in rock bolts support work in Diversion tunnel by Drill \& Blast method <br> ITEM: providing and fixing 25 mm diameter steel rock bolts with the help of resin bond cement capsule Anchorage, and fixing 10 mm thick $180 \times 180 \mathrm{~mm}$ size plate washers and nuts.

| DATA - Diameter of ribbed steel rock | 25 mm |
| :--- | :--- |
| Length of rock bolt including threaded portion | 4.15 m |
| Plate washers $180 \times 180 \times 10 \mathrm{~mm}$ thick | 2 Nos. |
| Resin bond cement grout capsule | 1 No. |
| M S Nuts for bolts | 2 Nos. |
| Diameter of hole for fixing rock bolt | 35 mm |
| Depth of hole for fixing rock bolt | 4.0 m |

For DT - 1

| Rock bolt calculation |  |  |
| :--- | :--- | :--- |
| Distance in Good Rock(15\%) + Fair Rock(60\%) of | 472 m | 354 m |
| In 3 m stretch 24 Nos of Rock bolt is required |  |  |
| So rock bolt only needed in Heading |  |  |
| So 12 Nos of Rock bolt is required | $(354 \mathrm{~m} / 3 \mathrm{~m})$ | 118 Nos |
| Nos of cycle in DT - 1 for rock bolt | $(18 \times 12)$ | 1416 <br> Nos of rock bolt in 354 m |


| For Good and Fair Rock |  |
| :--- | :--- |
| Length of rock bolt excluding threaded portion for 1416 bolts (1416×4) | 5664 m |
| Quantity of drilling for 1416 bolts | 5664 m |
| Rate of drilling for rock bolts including shifting | $4 \mathrm{~m} / \mathrm{hr}$ |
| Time for drilling 5664 m with 4 jack hammers $(5664 / 4 / 4)$ say | 354 hour |


| For Poor and V. Poor Rock |  |
| :--- | :--- |
| Distance in Poor Rock(15\%) + V.Poor Rock(10\%) of $\quad 472 \mathrm{~m}$ | 118 m |
| In 3 m stretch 32 Nos of Rock bolt is required. |  |
| So rock bolt only needed in Heading. $\quad(39.33 \times 16)$ |  |
| So 16 Nos of Rock bolt is required $\quad(118 \mathrm{~m} / 3 \mathrm{~m})$ | 39.33 Nos |
| Nos of cycle in DT - 1 for rock bolt $\quad 629$ Nos |  |
| Nos of rock bolt in $118 \mathrm{~m} \quad 2516 \mathrm{~m}$ |  |
| Length of rock bolt excluding threaded portion for 629 bolts (629×4) | 2516 m |
| Quantity of drilling for 629 bolts | 4 m per hour |
| Rate of drilling for rock bolts including shifting | 157.25 hour |
| Time for drilling 2516 m with 4 jack hammers $(2516 / 4 / 4)$ say |  |


| Requirement of materials (for Good(15\%) And Fair Rock (60\%)) |  |
| :--- | :--- |
| Quantity of 25 mm dia bars for $(1416)$ bolts with $2.5 \%$ wastage <br> $(1416 \times 4.15 \times 3.85 \times 1.025)$ | 23189.7435 kg |
| Quantity of washer for 1416 bolts with $2.5 \%$ wastage <br> $(1416 \times 4 \times 0.2 \times 0.2 \times 78.5 \times 1.025)$$\quad(1416 \times 2 \times 0.2)$ | 18229.584 kg |
| Quantity of nuts for 1416 bolts $\quad(1416 \times 1)$ | 1416 Nos |
| Quantity of grout capsule for 1416 bolts |  |


| Requirement of materials (for Poor (15\%) And V. Poor Rock (10\%)) |  |
| :---: | :---: |
| Quantity of 25 mm dia bars for $(629)$ bolts with $2.5 \%$ wastage <br> $(629 \times 4.15 \times 3.85 \times 1.025)$ | 10301.093 kg |


| Quantity of washer for 629 bolts with $2.5 \%$ wastage <br> $(629 \times 4 \times 0.2 \times 0.2 \times 78.5 \times 1.025)$ | 8097.746 kg |
| :--- | :--- |
| Quantity of nuts for 629 bolts $\quad(629 \times 2 \times 0.2)$ | 251.6 kg |
| Quantity of grout capsule for 629 bolts $\quad(629 \times 1)$ | 629 Nos |

For DT - 2

| Rock bolt calculation |  |
| :---: | :---: |
| Distance in Good Rock(15\%) + Fair Rock(60\%) of 552 m | 414 m |
| In 3 m stretch 24 Nos of Rock bolt is required. |  |
| So rock bolt only needed in Heading. |  |
| So 12 Nos of Rock bolt is required |  |
| Nos of cycle in DT - 2 for rock bolt ( $414 \mathrm{~m} / 3 \mathrm{~m}$ ) | 138 Nos |
| Nos of rock bolt in $414 \mathrm{~m} \quad(138 \times 12)$ | 1656 Nos |
| For Good and Fair Rock |  |
| Length of rock bolt excluding threaded portion for 1656 bolts (1656×4) | 6624 m |
| Quantity of drilling for 1656 bolts | 6624 m |
| Rate of drilling for rock bolts including shifting | 4 m per hour |
| Time for drilling 6624 m with 4 jack hammers (6624/4 / 4) say | 414 hour |
| For Poor And V. Poor Rock |  |
| Distance in Poor Rock(15\%) + V.Poor Rock(10\%) of 552 m | 138 m |
| In 3 m stretch 32 Nos of Rock bolt is required. |  |
| So rock bolt only needed in Heading. |  |
| So 16 Nos of Rock bolt is required |  |
| Nos of cycle in DT - 2 for rock bolt ( $138 \mathrm{~m} / 3 \mathrm{~m}$ ) | 46 Nos |
| Nos of rock bolt in $138 \mathrm{~m} \quad(46 \times 16)$ | 736 Nos |
| Length of rock bolt excluding threaded portion for 736 bolts (736×4) | 2944 m |
| Quantity of drilling for 736 bolts | 2944 m |
| Rate of drilling for rock bolts including shifting | 4 m per hour |


| Time for drilling 2944 m with 4 jack hammers (2944 / 4 / 4) say | 184 hour |
| :--- | :--- |


| Requirement of materials (for Good(15\%) And Fair Rock (60\%)) |  |  |  |
| :--- | :--- | :---: | :---: |
| Quantity of 25 mm dia bars for $(1656)$ bolts with $2.5 \%$ wastage <br> $(1656 \times 4.15 \times 3.85 \times 1.025)$ | 27120.2085 kg |  |  |
| Quantity of washer for 1656 bolts with $2.5 \%$ wastage <br> $(1656 \times 4 \times 0.2 \times 0.2 \times 78.5 \times 1.025)$$\quad(1656 \times 2 \times 0.2)$ | 21319.344 kg |  |  |
| Quantity of nuts for 1656 bolts $\quad 662.4 \mathrm{~kg}$ |  |  |  |
| Quantity of grout capsule for 1656 bolts $(1656 \times 1)$ | 1656 Nos |  |  |


| Requirement of materials (for Poor (15\%) And Very Poor Rock (10\%)) |  |
| :--- | :--- | :--- |
| Quantity of 25 mm dia bars for $(736)$ bolts with $2.5 \%$ wastage <br> $(736 \times 4.15 \times 3.85 \times 1.025)$ | 12053.426 kg |
| Quantity of washer for 736 bolts with $2.5 \%$ <br> $(736 \times 4 \times 0.2 \times 0.2 \times 78.5 \times 1.025)$ | 9475.264 kg |
| Quantity of nuts for 736 bolts $\quad(736 \times 2 \times 0.2)$ | 294.4 kg |
| Quantity of grout capsule for 736 bolts (736 x 1) | 736 Nos |

## Requirement of machinery :

Deploy 1 Air compressor 15 cmm for 1.5 hours with 50 minutes per hour working.
Deploy 4 Jack hammers / Stooper drills for 1.5 hours with 50 minutes per hour working.
Deploy Drilling jumbo for 4 hours including fixing bolts.
Deploy 10 hp pump for 1.5 hour for pumping water to storage tank.

| Requirement of workforce ( other than machinery crew ) |  |
| :--- | :--- |
| Gas cutter for preparing washers and wedges | 0.5 No. |
| Turner for threading bolts | 1 No. |
| Hammerman | 0.5 No. |
| Fitter for fixing bolts | 0.5 No. |


| Khalasis 2 Nos for 0.5 day | 1 No. |
| :--- | :--- |
| Heavy mazdoor for assisting in cutting / fabrication / fixing | 2 Nos. |

## Re-handling lead for materials:

As rock bolts are stored outside tunnel and are to be conveyed inside tunnel after fabrication at workshop re-handling lead of 1 km is considered.

| Use rate of materials |  |  |
| :--- | :--- | :--- |
| Cost of drill rod 2.5 m long | $@ 7175.00 / \mathrm{No}$. | 7175.00 |
| Life of drill rod with reconditioning |  | 150 m |
| Use rate of drill rod per m drilling | (cost / life) | 47.83 |
| Cost of air hose 25 m per jack hammer | $200.00 / \mathrm{Rm}$ | 5000.00 |
| Life of air hose |  | 800 hours |
| Use rate of air hose per hour | (cost / life) | 6.25 |
| Cost of water hose 25m per jack hammer | $185.00 / \mathrm{Rm}$ | 4625.00 |
| Life of water hose |  | 800 hours |
| Use rate of water hose per hour (cost / life) | 5.78 |  |

## RATE ANALYSIS (Good \&Fair Rock) in DT - 1

UNIT
: 5664.0 Rm

## A.MATERIALS:

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rein.Steel with 2.5 \% wastage | kg | 23189.7 | 48.48 | 1124238.789 |
| 2 | Steel plate for washers | kg | 18229.6 | 51.14 | 932260.925 |
| 3 | Resin bond cement grout capsule | Nos | 1416 | 65 | 92040 |
| 4 | M S Nuts for bolts | kg | 566.4 | 90 | 50976 |
| 5 | Use rate of drill rod | Rm | 5664 | 47.83 | 270909.12 |
|  | Reconditioning charges @ 10\% |  |  |  |  |
| 6 | Use rate of air hose 4 Nos | Hour | 6 | 6.25 | 37.5 |
| 7 | Use rate of water hose 4 Nos | Hour | 6 | 5.78 | 34.68 |
| 8 | Sundries(gas for cutting etc) | LS | 5 | 44 | 220 |
|  |  |  |  | Total | 2470717.014 |


| Add for small Tools and Plants | @ $1 \%$ | 24707.1701 |
| :--- | :--- | :--- |


| Add for Contractor's Profit | @ $10 \%$ | 247071.701 |
| :--- | :--- | :--- |
| Add for Contractor's Overheads | $@ 5 \%$ | 123535.8507 |
| Total cost of Materials | $\mathbf{2 8 6 6 0 3 1 . 7 3 6}$ |  |

RATE ANALYSIS (Poor \& V. Poor Rock)
UNIT : 2516.0 Rm

## A.MATERIALS:

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rein.Steel with 2.5 \% wastage | kg | 10301.09 | 48.48 | 499396.988 |
| 2 | Steel plate for washers | kg | 8097.746 | 51.14 | 414118.73 |
| 3 | Resin bond cement grout capsule | Nos | 629 | 65 | 40885 |
| 4 | M S Nuts for bolts | kg | 251.6 | 90 | 22644 |
| 5 | Use rate of drill rod | Rm | 2516 | 47.83 | 120340.28 |
|  | Reconditioning charges @ 10\% |  |  |  |  |
| 6 | Use rate of air hose 4 Nos | Hour | 6 | 6.25 | 37.5 |
| 7 | Use rate of water hose 4 Nos | Hour | 6 | 5.78 | 34.68 |
| 8 | Sundries(gas for cutting etc) | LS | 5 | 44 | 220 |
|  |  |  |  | Total | 1097677.178 |


| Add for small Tools and Plants | @ $1 \%$ | 10976.771 |
| :--- | :--- | :--- |
| Add for Contractor's Profit | @ $10 \%$ | 109767.717 |
| Add for Contractor's Overheads | @ $5 \%$ | 54883.8589 |
| Total cost of Materials |  | $\mathbf{1 2 7 3 3 0 5 . 5 2 5}$ |

Rate analysis (Good \& Fair Rock) in DT - 2 UNIT : 6624 Rm

## A.MATERIALS:

| S.N | Particulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rein. Steel with 2.5\% wastage | kg | 27120.209 | 48.48 | 1314787.708 |
| 2 | Steel plate for washers | kg | 21319.344 | 51.14 | 1090271.252 |
| 3 | Resin bond cement grout capsule | Nos | 1656 | 65 | 107640 |
| 4 | M S Nuts for bolts | kg | 662.4 | 90 | 59616 |
| 5 | Use rate of drill rod | Rm | 6624 | 47.83 | 316825.92 |
|  | Reconditioning charges @ 10\% |  |  |  | 31682.592 |
| 6 | Use rate of air hose 4 Nos | Hour | 6 | 6.25 | 37.5 |
| 7 | Use rate of water hose 4 Nos | Hour | 6 | 5.78 | 34.68 |
| 8 | Sundries(gas for cutting) | LS | 5 | 44 | 220 |
|  |  |  |  | Total | 2921115.652 |

Add for small Tools and Plants @ 1\% 29211.156

| Add for Contractor's Profit on Energy | @ $10 \%$ | 292111.5652 |
| :--- | :--- | :--- |
| Add for Contractor's Overheads | @ $5 \%$ | 146055.782 |
| Total cost of Materials |  | $\mathbf{3 3 8 8 4 9 4 . 1 5 5}$ |

## RATE ANALYSIS (Poor \& Very Poor Rock) <br> UNIT <br> : 2944 Rm

## A.MATERIALS:

| S.N | Particulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rein. Steel with 2.5\% wastage | kg | 12053 | 48.48 | 584335.5485 |
| 2 | Steel plate for washers | kg | 9475.3 | 51.14 | 484565.001 |
| 3 | Resin bond cement grout capsule | Nos | 736 | 65 | 47840 |
| 4 | M S Nuts for bolts | kg | 294.4 | 90 | 26496 |
| 5 | Use rate of drill rod | Rm | 2944 | 47.83 | 140811.52 |
|  | Reconditioning charges @ 10\% |  |  |  |  |
| 6 | Use rate of air hose 4 Nos | Hour | 6 | 6.25 | 37.5 |
| 7 | Use rate of water hose 4 Nos | Hour | 6 | 5.78 | 34.69 |
| 8 | Sundries(gas for cutting) | LS | 5 | 44 | 220 |
|  |  |  |  | Total | 1284340.26 |


| Add for small Tools and Plants | @ 1\% | 12843.4026 |
| :--- | :--- | :--- |
| Add for Contractor's Profit on Energy | @ $10 \%$ | 128434.026 |
| Add for Contractor's Overheads | @ $5 \%$ | 64217.013 |
| Total cost of Materials |  | $\mathbf{1 4 8 9 8 3 4 . 7 0 2}$ |

## B. MACHINERY:

| S.N | Description | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Air compressor 15 cmm | Hour | 1.5 | 119 | 178.5 |
|  | Fuel charges | Hour | 1.5 | 800 | 1200 |
| 2 | Pump 10 hp | Hour | 1.5 | 5 | 7.5 |
|  | Fuel charge | Hour | 1.5 | 64 | 96 |
| 3 | Jack hammer | Hour | 6 | 16 | 96 |
|  | Fuel charges | Hour | 6 | 8 | 48 |
| 4 | Pusher leg | Hour | 6 | 9 | 54 |
|  | Fuel charges | Hour | 6 | 6 | 36 |
| 5 | Drilling jumbo | Hour | 4 | 370 | 1480 |
|  | Fuel charges | Hour | 4 | 41 | 164 |
| 6 | Sundries (lathe, etc $)$ | LS | 7 | 44 | 308 |
|  |  |  |  | Total | 3668 |


| Add for small Tools and Plants | @ 1\% | 36.68 |
| :--- | :--- | :--- |
| Add for Contractor's Profit on Energy | @ 10\% | 185.20 |


| Add for Contractor's Overheads | $@ 5 \%$ | 183.40 |
| :--- | :--- | :--- |
| Total hire charges on machinery |  | $\mathbf{4 0 7 3 . 2 8}$ |

## C.LABOUR

| S.N | Description | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Crew for Air compressor | Hour | 1.5 | 101 | 151.5 |
| 2 | Crew for pump | Hour | 1.5 | 45 | 67.5 |
| 3 | Crew for Jack hammer | Hour | 6 | 188 | 1128 |
| 4 | Crew for Drilling jumbo | Hour | 4 | 101 | 404 |
| 5 | Fitte | Day | 0.5 | 254.73 | 127.37 |
| 6 | Gas cutter | Day | 0.5 | 254.73 | 127.37 |
| 7 | Turner | Day | 1 | 253.73 | 254.73 |
| 8 | Khalasi $(2 \times 0.5)$ | Day | 1 | 241.23 | 241.23 |
| 9 | Hammerman | Day | 0.5 | 241.73 | 120.87 |
| 10 | Heavy mazdoor | Day | 2 | 238.73 | 477.46 |
|  |  |  |  | Total | 3100.02 |


| Add for small Tools and Plants | @ $1 \%$ | 31.00 |
| :--- | :--- | :--- |
| Add for Contractor's Profit | @ $10 \%$ | 310.00 |
| Add for hidden cost on Labour | @ $15 \%$ | 465.00 |
| Add for additional hidden cost on labour | @ $10 \%$ | 310.00 |
| Add for Contractor's Overheads | @ $5 \%$ | 155.00 |
| Total cost of labour |  | $\mathbf{4 3 7 1 . 0 2}$ |

### 3.30 Abstract of cost details of Rock bolt support in DT - 1 by Drill \& Blast method

For DT - 1

| For Good and fair Rock |  |
| :--- | :--- |
| A. Cost of Materials | 2866031.736 |
| B. Hire charges of Machinery | 4073.28 |
| C. Cost of Labour | 4371.02 |
|  | $\mathbf{2 8 7 4 4 7 6 . 0 3 6}$ |


| Add for Air and Water line | @ $0.80 \%$ | 22995.808 |
| :--- | :--- | :--- |
| Add for Lighting | $@ 1.80 \%$ | 51740.568 |
| Add for Ele sub-station / Demand charges | @ $3.80 \%$ | 10923.0894 |
| Add for other enabling works | $@ 1.70 \%$ | 48866.092 |
| TOTAL |  | $\mathbf{0 0 9 0 0 1 . 5 9 3}$ |
| Add for 1 km rehandling lead charges |  |  |
| For steel 150 kg | @ 218.40 per tonne <br> $(0.15 \times 218.40)$ | 32.76 |
| Total cost for | $\mathbf{5 6 6 4} \mathbf{~ R m}$ | $\mathbf{0 0 9 0 3 4 . 3 5 3}$ |


| For Poor and V. Poor Rock |  |
| :--- | :--- |
| A. Cost of Materials | 1097677.178 |
| B. Hire charges of Machinery | 4073.28 |
| C. Cost of Labour | 4371.02 |
|  | $\mathbf{1 1 0 6 1 2 1 . 4 7 8}$ |


| Add for Air and Water line | @ $0.80 \%$ | 8848.9718 |
| :--- | :--- | :--- |
| Add for Lighting | @ $1.80 \%$ | 19910.1866 |
| Add for Eletrical sub-station / Demand <br> charges | @ $3.80 \%$ | 42032.616 |
| Add for other enabling works | $@ 1.70 \%$ | 18804.0651 |
| TOTAL |  | 1195717.318 |
| Add for 1 km rehandling lead charges | @218.40 per tonne <br> $(0.15 \times 218.40)$ | 32.76 |
| For steel 150 kg | $\mathbf{2 5 1 6 ~ R m ~}$ |  |
| Total cost for | $\mathbf{1 1 9 5 7 5 0 . 0 7 8}$ |  |

Total cost for Rock bolt support work in (Good \& Fair Rock + Poor \& Very Poor Rock):

Total cost for Rock bolt support work (3009034.353+1195750.078) : 4204784.431

### 3.31 Abstract of cost details of Rock bolt support in DT- 2 by Drill \& Blast method

## For DT- 2

| For Good and fair Rock |  |
| :--- | :--- |
| A. Cost of Materials | 3388494.155 |
| B. Hire charges of Machinery | 4073.28 |
| C. Cost of Labour | 4371.02 |
| TOTAL | $\mathbf{3 3 9 6 9 3 8 . 4 5 5}$ |


| Add for Air and Water line | @ $0.80 \%$ | 27175.507 |
| :--- | :--- | :--- |
| Add for Lighting | @ $1.80 \%$ | 61144.892 |
| Add for Ele sub-station / Demand charges | @ $3.80 \%$ | 129083.661 |
| Add for other enabling works | @ $1.70 \%$ | 57747.953 |
| TOTAL |  | $\mathbf{3 6 7 2 0 9 0 . 5 0 1}$ |
| Add for 1 km rehandling lead charges |  |  |
| For steel 150 kg | @ $218.40 \quad$ per <br> tonne $(0.15 \times 218.40)$ | 32.76 |
| Total cost for | $\mathbf{6 6 2 4} \mathbf{~ R m}$ | $\mathbf{3 6 7 2 1 2 3 . 2 6 1}$ |


| For Poor and V. Poor Rock |  |
| :--- | :--- |
| A. Cost of Materials | 1489834.702 |
| B. Hire charges of Machinery | 4073.28 |
| C. Cost of Labour | 4371.02 |
| TOTAL | $\mathbf{1 4 9 8 2 7 9 . 0 0 2}$ |


| Add for Air and Water line | @ $0.80 \%$ | 11986.232 |
| :--- | :--- | :--- |
| Add for Lighting | @ $1.80 \%$ | 26969.022 |
| Add for Eletrical sub-station / Demand <br> charges | @ 3.80\% | 56934.602 |


| Add for other enabling works | @ $1.70 \%$ | 25470.743 |
| :--- | :--- | :--- |
| TOTAL |  | 1619639.601 |
| Add for 1 km rehandling lead charges |  |  |
| For steel 150 kg | @ 218.40 per tonne <br> $(0.15 \times 218.40)$ | 32.76 |
| Total cost for | $\mathbf{2 9 4 4} \mathbf{~ R m}$ | $\mathbf{1 6 1 9 6 7 2 . 3 6 1}$ |

Total cost for Rock bolt support work in (Good \& Fair Rock + Poor \& V. Poor Rock):
Total cost for Rock bolt support work ( $3672123.261+1619672.361$ ): $\quad \mathbf{5 2 9 1 7 9 5 . 6 2 2}$

### 3.32 Cost estimation in kerb and invert lining for Diversion tunnel by Drill \& Blast method

ITEM: Providing and laying insitu vibrated M-20 grade cement concrete using $\mathbf{4 0} \mathbf{~ m m}$ clean, hard, graded aggregates crushed from tunnel excavated rock for kerb and Invert lining. Cement content 270 kg per $\mathrm{m}^{3}$

## Cost of shuttering:

Consider 1 shutter and 1 soldier set:
Shutter size: $800 \mathrm{~mm} \times 1200 \mathrm{~mm}$, Soldier length: 2.3 m , Shutter area $: 1.20 \mathrm{~m}^{2}$

| 4 mm thick plate $1.5 \mathrm{~m}^{2}$ | @ 31.5 kg per $\mathrm{m}^{2}$ | $(1.5 \times 31.5)$ | 47.25 kg |
| :--- | :--- | :--- | :---: |
| $50 \times 50 \mathrm{x} 6 \mathrm{~mm}$ angle 6.5 m <br> length | @ 3.5 kg per m | $(6.5 \times 3.5)$ | 22.75 kg |
| 50 x 6 mm flat 2.0 m length | @ 2.5 kg per m | $(2 \times 2.5)$ | 5.0 kg |
| ISLC 2002.5 m length | @ 8.0 kg per m | $(2.5 \times 8)$ | 20.0 kg |
| 6 mm plate $0.05 \mathrm{~m}^{2}$ | @ 47.5 kg per $\mathrm{m}^{2}$ | $(0.05 \times 47.5)$ | 2.375 kg |
| Cost of 4 mm plate 47.25 kg | @ 51.14 per kg | $(47.25 \times 51.14)$ | 2416.365 |
| Cost of 6.5 m angle 22.75 <br> kg | @ 49.14 per kg | $(22.75 \times 49.14)$ | 1117.935 |
| Cost of 2 m flat 5 kg | @ 51.14 per kg | $(5 \times 51.14)$ |  |
| Cost of 2.5 m soldier 20 kg | @ 49.14 per kg | $(20 \times 49.14)$ | 982.8 |
| Cost of 6 mm plate 2.375 kg | @ 51.14 per kg | $(2.375 \times 51.14)$ | 121.457 |


| TOTAL |  | 4894.257 |
| :--- | :--- | :--- |


| Add wastage | @ $2.5 \%$ | 122.356 |
| :--- | :--- | :---: |
| Add for bolts \& nuts | $@$ <br> $(0.5 \times 90)$ | 45.00 |
| Add for <br> shutter | fabrication of $; 90.00 / \mathrm{kg}$ <br> $(47.25+22.75+5+20+2.375) \times 16$ | 1558 |
| TOTAL |  | $\mathbf{6 6 1 9 . 6 1 3}$ |
| Less salvage value | $@ 10 \%$ | -661.9613 |
| TOTAL |  | $\mathbf{5 9 5 7 . 6 5 1}$ |


| Use rate of shutters |  |  |
| :--- | :--- | :---: |
| Use rate of shutters considering average 40 uses |  | 126.47 |
| Add for repairs/ replacements etc | $@ 15 \%$ | 18.97 |
| Add for binding wire/ temperary supports etc | $@ 5 \%$ | 6.32 |
| Add for shutter oil at 0.2 litre per $m^{2}$ | $@ 35.00$ <br> $(0.2 \times 35)$ | 7.00 |
| TOTAL |  | $\mathbf{1 5 8 . 7 7}$ |


| Effective area of shutter \& soldier with 10 cm margin at top and bottom | $: 1.00 \mathrm{~m}^{2}$ |
| :--- | :--- |
| Cost of shuttering for concrete per $\mathrm{m}^{2}$ | $: \mathbf{1 5 8 . 7 7}$ |
| Erection \& dismantling shuttering : |  |
| Fitters 1 Carpentor and 5 mazdoors erect $50 \mathrm{~m}^{2}$ shuttering / day. |  |
| Cost of dismantling assumed at $50 \%$ of erection charges. |  |
| Area of shuttering with supports considered. | $: 100 \mathrm{~m}^{2}$ |


| Cleaning, conveying, erecting and oiling |  |  |  |
| :--- | :--- | :---: | :---: |
| Fitter shuttering 4 Nos | @ 244.23 per day | $(4 \times 244.23)$ | 976.92 |
| Carpentor 2 Nos | @ 244.23 per day | $(2 \times 244.23)$ | 488.46 |
| Heavy mazdoor 10 Nos | @ 238.73 per day | $(10 \times 238.73)$ | 2387.30 |
|  |  |  |  |
| Dismantling and stacking |  |  |  |


| Fitter shuttering 2 Nos | @ 244.23 per day | $(2 \times 244.23)$ | 488.46 |
| :--- | :--- | :--- | :--- |
| Carpentor 1 Nos | @ 244.23 per day | $(1 \times 244.23)$ | 244.23 |
| Heavy mazdoor 5 Nos | @ 238.73 per day | $(5 \times 238.73)$ | 1193.65 |
| TOTAL |  |  | $\mathbf{5 7 7 9 . 0 2}$ |

Labour charges for erecting and dismantling shuttering per $m^{2}$

## DATA: Concrete mix details for $\mathbf{5 0 - 7 0} \mathbf{~ m m}$ slump:

For $1 m^{3}$ cement concrete :-Coarse aggregates: $0.85 m^{3}(1350 \mathrm{~kg})$ Blending ratio : 50:30:20 Fine aggregate : $0.41 m^{3}(665 \mathrm{~kg}) \quad$ Cement : $270 \mathrm{~kg} \quad$ Super plasticizer : 0.81 litre

Wastage : $1 \%$ for cement and $2 \%$ for coarse \& fine aggregates.
Consider $2 \mathrm{~m}^{3}$ capacity agitator car for conveying concrete.
Cycle time for one round trip:

| Turning and spotting | 2 minutes |
| :--- | :---: |
| Loading 4 mixes of $0.5 \mathrm{~m}^{3} @ 5$ min per mix | 20 minutes |
| Running time from batching plant to placing point average 1 km | 10 minutes |
| Unloading concrete | $\mathbf{1 5}$ minutes |
| Return trip to batching Plant | $\mathbf{1 0}$ minutes |
| Total cycle time for round | 57 minutes |

Deploy 2 Agitator cars for conveying concrete.
The rate of concreting for 2 agitator cars with $50 \mathrm{~min} / \mathrm{hr}$ working: $3.50 \mathrm{~m}^{3}$ per hour

| Progress per shift of 8 hours | $\mathbf{( 8 \times 3 . 5 0})$ | $\mathbf{2 8} \mathrm{m}^{3}$ |
| :--- | :---: | :---: |
| Requirement of materials |  |  |
| Cement for mixture with $1 \%$ wastage | $(28 \times 270 \times 1.01)$ | 7636 kg |
| Cement for incidentals @ $1 \mathrm{~kg} / \mathrm{m}^{3}$ | $(28 \times 1)$ | 28 kg |
| Coarse aggregate $40-20 \mathrm{~mm}$ size range | $(28 \times 0.85 \times 0.5 \times 1.02)$ | $12.15 \mathrm{~m}^{3}$ |
| Coarse aggregate $20-10 \mathrm{~mm}$ size range | $(28 \times 0.85 \times 0.3 \times 1.02)$ | $7.30 \mathrm{~m}^{3}$ |
| Coarse aggregate $10-4.75 \mathrm{~mm}$ size | $(28 \times 0.85 \times 0.2 \times 1.02)$ | $4.85 \mathrm{~m}^{3}$ |
| Fine aggregate | $(28 \times 0.41 \times 1.02)$ | $11.70 \mathrm{~m}^{3}$ |
| Super plasticiser | $(28 \times 0.81 \times 1.02)$ | 23.00 litres |

## 2. Requirement of machinery :

Deploy $6 \mathrm{~m}^{3}$ per hour rated capacity batching plant for 8 hours production of concrete.
Deploy 2 Nos $2 m^{3}$ capacity agitator cars for 8 hours conveying concrete.
Deploy 1 Needle vibrater 40 mm dia for 8 hours vibrating concrete.
Deploy 1 Pump 10 hp for 4.00 hour for water required for concrete mixing / curing / cleaning

## 3. Formwork \& scaffolding:

For kerb / bed concreting average 1 shuttering is required per cum of concrete.
Requirement of shuttering for $28 \mathrm{~m}^{3}$ concrete $: 28 \mathrm{~m}^{2}$

## 4. Requirement of workforce ( other than machinery crew ) :

Consider batching of materials and conveyance \& laying of concrete by manual labour.

| Maistry (1 @ batching plant and 1 @ placing point) | 2 Nos. |
| :--- | :--- |
| Mason Class - I | 1 No. |
| Mason Class - II | 1 No. |


| Cement handling mazdoor |  |
| :--- | :---: |
| for loading cement to Batching Plant bin | 2 Nos <br> Heavy mazdoor |
| for remixing \& filling mortar pans | 2 Nos |
| for loading mortar pan | 2 Nos |
| for laying concrete | 2 Nos |
| for cleaning bed and assisting Mason | 1 Nos |
| for miscellaneous works at Batching Plant | 1 Nos |
| Light mazdoor |  |
| for conveying concrete $\quad$ @ $2 m^{3}$ per day | 14 Nos |
| for cleaning, curing \& miscellaneous | 1 Nos |

## 5. Re-handling lead for materials:

As cement store can be located close to Batching Plant.
Consider 2 cement handling mazdoors for loading cement to Batching Plant bin.
As coarse and fine aggregates can be stocked near the Batching Plant

Consider 4 heavy and 4 light mazdoors for loading Coarse Aggregate to Batching Plant bins@ $6 m^{3}$ per day
Consider 2 heavy and 2 light mazdoors for loading Fine Aggregate to BP bins @ $6 m^{3}$ per day
RATE ANALYSIS
UNIT
: $\mathbf{2 8 . 0 0} \mathrm{m}^{3}$

## A.MATERIALS:

| S.N | Perticulars | Unit | Quantity |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Rate in INR | Amount in INR |  |  |  |  |
| 1 | Cement 43 Gr | kg | 7636 | 7.5 | 57270 |
|  | Cement for incidentals @ $1 \mathrm{~kg} / \mathrm{cum}$ | kg | 28 | 7.5 | 210 |
| 2 | Fine aggregate ( screened ) | cum | 11.7 | 730 | 8541 |
| 3 | Coarse aggregate $40-20 \mathrm{~mm}$ | cum | 12.15 | 740 | 8991 |
|  | Coarse aggregate $20-10 \mathrm{~mm}$ | cum | 7.3 | 950 | 6935 |
|  | Coarse aggregate $10-4.75 \mathrm{~mm}$ | cum | 4.85 | 1160 | 5626 |
| 4 | Super plasticiser | ltr | 23 | 105 | 2415 |
| 5 | Use rate of shuttering for kerb / bed | sqm | 28 | 158.77 | 4445.45 |
|  | Supports for shuttering @ $5 \%$ |  |  |  | 222.27 |
| 6 | Sundries | LS | 2 | 44 | 88 |
|  |  |  |  | Total | 94743.72 |


| Add for small Tools and Plants | $@ 1 \%$ | 947.744 |
| :--- | :--- | :---: |
| Add for Contractor's Profit | $@ 10 \%$ | 9474.37 |
| Add for Contractor's Overheads | $@ 5 \%$ | 4737.19 |
| Total cost of materials |  | $\mathbf{1 0 9 9 0 2 . 7 2}$ |

## B.Machinery

| S.N | Description | Unit | Quantity | Rate inINR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Batching plant 6 cum / hr rated capacity | Hour | 8 | 144 | 1152 |
|  | Fuel charges | Hour | 8 | 160 | 1280 |
| 2 | Agitator car 2 cum (2 Nos ) | Hour | 16 | 708 | 11328 |
|  | Fuel charges | Hour | 16 | 832 | 13312 |
| 3 | Needle Vibrator | Hour | 8 | 8 | 64 |
|  | Fuel charges | Hour | 8 | 6 | 48 |
| 4 | Pump 10 hp | Hour | 4 | 5 | 20 |
|  | Fuel charges | Hour | 4 | 64 | 256 |
| 5 | Sundries | LS | 2 | 44 | 88 |
|  |  |  |  | Total | 27548 |


| Add for small Tools and Plants | @ 1\% | 275.48 |
| :--- | :--- | :---: |
| Add for Contractor's Profit on Energy | @ 10\% | 1498.40 |
| Add for Contractor's Overheads | @ 5\% | 1377.40 |
| Total hire charges of Machinery |  | $\mathbf{3 0 6 9 9 . 2 8}$ |

## C.LABOUR

| S.N | Description | Unit | Quantity | Rate inINR | Quantity in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Crew for Batching plant | Hour | 8 | 181 | 1448 |
| 2 | Crew for Agitator car | Hour | 16 | 151 | 2416 |
| 3 | Crew for vibrator | Hour | 8 | 90 | 720 |
| 4 | Crew for pump | Hour | 4 | 45 | 180 |
| 5 | Masom Class - 1 | Day | 1 | 256.73 | 256.73 |
| 6 | Masom Class - 2 | Day | 1 | 244.23 | 244.23 |
| 7 | Hammerman for scaling bed | Day | 1 | 241.73 | 241.73 |
| 8 | Maistry | Day | 2 | 241.23 | 482.46 |
| 9 | Cement handling mazdoor |  |  |  |  |
|  | for loading cement to BP bin | Day | 2 | 239.73 | 479.46 |
| 10 | Heavy mazdoor |  |  |  |  |
|  | for miscellaneous work at BP | Day | 1 | 238.73 | 238.73 |
|  | for scaling \& cleaning bed | Day | 1 | 238.73 | 237.73 |
|  | for loading CA to BP bins | Day | 4 | 238.73 | 954.92 |
|  | for loading FA to BP bin | Day | 2 | 238.73 | 477.46 |
|  | for laying concrete | Day | 6 | 238.73 | 1432.38 |
| 11 | Light mazdoor |  |  |  |  |
|  | for loading CA to BP bins | Day | 4 | 237.23 | 948.92 |
|  | for loading FA to BP bin | Day | 2 | 237.23 | 474.46 |
|  | for conveying concrete | Day | 14 | 237.23 | 3321.22 |
|  | for curing / miscellaneous | Day | 1 | 237.23 | 237.23 |
| 12 | Labour charges for shuttering | sqm | 28 | 57.79 | 1618.13 |
|  | Labour charges for supports @ 5 \% |  |  |  | 80.91 |
|  |  |  |  | Total | 16491.69 |


| Add for small Tools and Plants | @ 1\% | 164.92 |
| :--- | :--- | :---: |
| Add for Contractor's Profit | @ $10 \%$ | 1649.17 |
| Add for hidden cost on Labour | @ $15 \%$ | 2473.75 |
| Add for additional hidden cost on labour | $@ 10 \%$ | 1649.17 |
| Add for Contractor's Overheads | $@ 5 \%$ | 824.58 |
| Total cost of Labour |  | $\mathbf{2 3 2 5 3 . 2 9}$ |

### 3.33 Abstract of cost details of Kerb \& Invert lining for Diversion tunnel by Drill \& Blast method

| A. Cost of Materials | 109902.72 |
| :--- | :---: |
| B. Hire charges of Machinery | 30699.28 |
| C. Cost of Labour | 23253.29 |
| TOTAL | $\mathbf{1 6 3 8 5 5 . 2 8}$ |
| Add for Air and Water line @ $0.80 \%$ | 1310.84 |
| Add for Lighting | @ $1.80 \%$ |
| Add for Electrical sub-station / Demand charges @ 3.80\% | 2924.40 |
| Add for other enabling works $\quad$ @ $1.70 \%$ | 6226.50 |
| Total cost for $\mathbf{2 8 . 0 0} \mathbf{m}^{\mathbf{3}}$ | 2785.54 |
| Rate per $\boldsymbol{m}^{\mathbf{3}}$ | $\mathbf{1 7 7 1 2 7 . 5 6}$ |

Total cost for Kerb and Invert Lining in DT $-1(4+4+3.1)=11.1 \mathrm{~m}^{2} \times 472 \mathrm{~m} \times 6326$ $=33143179.2$

Total cost for Kerb and Invert Lining in DT $-2(4+4+3.1)=11.1 \mathrm{~m}^{2} \times 552 \mathrm{~m} \times 6326$ $=38760667.2$

### 3.34 Cost estimation for Overt lining in Diversion tunnel by Drill \& Blast method

ITEM. Providing and laying insitu vibrated M-20 grade cement concrete using $\mathbf{4 0} \mathbf{~ m m}$ clean, hard, graded aggregates crushed from tunnel excavated rock for Overt lining.
DATA. Concrete mix details per $\boldsymbol{m}^{3}$
for $80-100 \mathrm{~mm}$ slump:

| Cement 43 Grade | 300 kg |  |
| :--- | :--- | :---: |
| Fine aggregate | 680 kg per $\boldsymbol{m}^{\mathbf{3}}$ | $0.425 \boldsymbol{m}^{\mathbf{3}}$ |
| Coarse aggregate | 1265 kg per $\boldsymbol{m}^{\mathbf{3}}$ | $0.79 \boldsymbol{m}^{\mathbf{3}}$ |
| Blending ratio | $50: 30: 20$ |  |


| Concrete admixture (Super plasticiser) | 0.90 litre |
| :--- | :--- |
| Diameter of tunnel (finished) considered | 12.345 m |
| Hight of tunnel (finished) considered | 12.345 m |

Track mounted collapsible gantry considered for supporting sides and arch concrete.

## Assume 15 m long collapsible type steel gantry:

| Quantity of concrete per gantry considering 1.0 m thick lining ( $16.54 \boldsymbol{m}^{3} \times 15 \mathrm{~m}$ ) | $248.1 \mathrm{~m}^{3}$ |
| :---: | :---: |
| Concrete for filling support reaches @ 45 \% | $14.75 \mathrm{~m}^{3}$ |
| Average quantity of concrete per gantry length of lining say | $248.1 \mathrm{~m}^{3}$ |
| Placing concrete for sides and arch | Placer pump |
| Cycle time for one round trip |  |
| Turning and spotting | 2 minute |
| Loading 4 mixes of $0.5 \boldsymbol{m}^{3}$ @ 5 minute per mix | 20 minute |
| Running time from Batching Plant to placing point average 1 km | 10 minute |
| Unloading concrete to placer drum | 24 minute |
| Return trip to BP | 10 minute |
| Total cycle time for round trip | 66 minute |
| Consider $2 m^{3}$ capacity agitator cars for conveying concrete. |  |
| Rate of concreting for 2 agitator cars with $50 \mathrm{~min} / \mathrm{hr}$ working $(2 \times 2 \times 60 \times 50 / 60 / 66)$ | $3.0 \mathrm{~m}^{3} / \mathrm{hr}$ |
| Progress per shift of 8 working hours (8 $\times 3.00$ ) | $24 \mathrm{~m}^{3}$ |
| Time required for concreting one gantry length (48/3) | 16 hours |
| Cycle time of various operations for concreting |  |
| Cleaning bed for laying track line | 2.0 hour |
| Dismantling \& extending track line | 4.0 hour |
| Releasing / moving / aligning gantry | 4.0 hour |
| Cleaning \& Oiling gantry / Bulk head fixing | 4.0 hour |
| Placer pipe assembling for different positions | 6.0 hour |
| Concreting $48 \mathrm{~m}^{3} @ 3.00 \mathrm{~m}^{3}$ per hour | 16.0 hour |
| Miscellaneous / Break downs / pipe clogging etc | 4.0 hour |


| Setting time before release of gantry | 12.0 hour |
| :--- | :--- |

Considering cleaning / scaling bed / track dismsntling and erection are carried out as parallel activities during setting time of concrete, the total cycle time for one gantry length concreting will be about 48 hours.

Out of 6 shifts ( 48 hours ) 3 shifts are considered as concreting shifts and 3 shifts are considered as preparatory shifts.

| Requirement of materials |  |  |
| :--- | :---: | :---: |
| Cement for mix with $1 \%$ wastage | $(248.1 \times 300 \times 1.01)$ | 75174.3 kg |
| Cement for incidentals @ $1 \mathrm{~kg} / \mathrm{m}^{3}$ | $(248.1 \times 1)$ | 248.1 kg |
| Coarse aggregate $40-20 \mathrm{~mm}$ size range | $(248.1 \times 0.79 \times 0.5 \times 1.02)$ | $99.9594 \mathrm{~m}^{3}$ |
| Coarse aggregate $20-10 \mathrm{~mm}$ size range | $(248.1 \times 0.79 \times 0.3 \times 1.02)$ | $59.9756 \mathrm{~m}^{3}$ |
| Coarse aggregate $10-4.75 \mathrm{~mm}$ size | $(248.1 \times 0.79 \times 0.2 \times 1.02)$ | $39.9837 \mathrm{~m}^{\mathbf{3}}$ |
| Fine aggregate | $(248.1 \times 0.425 \times 1.02)$ | $107.5513 \mathrm{~m}^{\mathbf{3}}$ |
| Super plasticiser | $(248 \times 0.90 \times 1.02)$ | 227.7558 liters |

## 2. Requirement of machinery:

Deploy $6 \mathrm{~m}^{3}$ per hour rated capacity batching plant for 16 hours for production of concrete.

Deploy 2 Nos $2 m^{3}$ capacity agitator cars for 16 hours for conveying concrete.
Deploy 8.5 cmm air compressor for 16 hours for supplying air to placer pump.
Deploy pneumatically operated placer pump for 16 hours for pumping concrete.
Deploy 1 Needle vibrater 40 mm dia for 16 hours for vibrating concrete.
Deploy 1 Pump 10 hp for 8 hours for water required for concrete mixing / curing / cleaning

## 3. Formwork \& scaffolding :

| Track mounted collapsible gantry for supporting sides concrete | $100 \mathrm{~m}^{2}$ |
| :--- | :--- |
| End shuttering (front face) | $6 \mathrm{~m}^{2}$ |

## 4. Requirement of workforce (other than machinery crew) :

Consider batching of materials and conveyance \& laying of concrete by manual labour.

| Maistry | (1 @ batching plant and $1 @$ placing point for 2 shifts) | 4 Nos. |
| :--- | :--- | :--- |


| Mason Class - 1 (1 in each shift for 2 shifts) | 2 Nos. |
| :--- | :--- |
| Foreman | 1 Nos. |
| Surveyor | 1 Nos. |
| Stone chiseller Class - 2 | 0.5 Nos. |
| Fitter shuttering | 1 Nos. |
| Helper shuttering | 1 Nos. |
| Khalasi | 2 Nos |
| Heavy mazdoor |  |
| for miscellaneous works at BP ( 1 in each shift for 2 shifts ) | 2 Nos. |
| for miscellaneous works at placer point ( 1 in each shift for 2 shifts ) | 2 Nos. |
| Light mazdoor |  |
| for cleaning, curing \& miscellaneous ( 1 in each shift for 2 shifts ) | 2 Nos. |

## 5. Re-handling lead for materials:

Consider 4 cement handling mazdoor ( 2 in each shift) for loading cement to BP bin.
Consider 6 heavy and 6 light mazdoor ( 3 each in each shift) for loading CA to BP bins.
Consider 4 heavy and 4 light mazdoor ( 2 each in each shift) for loading FA to BP bins.

## RATE ANALYSIS

## UNIT

: $\mathbf{2 4 8 . 1} \mathrm{m}^{\mathbf{3}}$

## A.MATERIALS:

| S.N | Perticulars | Unit | Quantity |  | Rate in INR Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Cement 43 Gr | kg | 75174.3 | 7.5 | 563807.25 |
|  | Cement for incidentals @ $1 \mathrm{~kg} / \mathrm{cum}$ | kg | 248.1 | 7.5 | 1860.75 |
| 2 | Fine aggregate ( screened ) | cum | 107.531 | 730 | 78512.449 |
| 3 | Coarse aggregate $40-20 \mathrm{~mm}$ | cum | 99.9594 | 740 | 73969.956 |
|  | Coarse aggregate $20-10 \mathrm{~mm}$ | cum | 59.9756 | 950 | 56976.82 |
|  | Coarse aggregate $10-4.75 \mathrm{~mm}$ | cum | 39.9837 | 1160 | 46381.092 |
| 4 | Super plasticiser | ltr | 227.756 | 105 | 23914.359 |
| 5 | Use rate of end shuttering | sqm | 6 | 158.77 | 952.6 |
| 6 | Use rate of steel gantry | sqm | 100 | 176.95 | 17695.03 |
| 7 | Sundries ( placer pipe etc ) | LS | 5 | 44 | 220 |
|  |  |  |  | Total | 864290.306 |

Add for small Tools and Plants
@ 1\% $\quad 8642.9030$

| Add for Contractor's Profit on Energy | @ $10 \%$ | 86492.0306 |
| :--- | :--- | :--- |
| Add for Contractor's Overheads | @ $5 \%$ | 43214.5153 |
| Total cost of Materials |  | $\mathbf{1 0 0 2 5 7 6 . 7 4 5}$ |

## B.MACHINERY:

| S.N | Description | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Air compressor 8.5 cmm | Hour | 16 | 119 | 1904 |
|  | Fuel charges @ 75 \% load | Hour | 12 | 360 | 4320 |
| 2 | Batching plant 6 cum / hr rated capacity | Hour | 16 | 144 | 2304 |
|  | Fuel charges | Hour | 16 | 160 | 2560 |
| 3 | Agitator car 2 cum ( 2 Nos ) | Hour | 32 | 708 | 22656 |
|  | Fuel charges | Hour | 32 | 832 | 26624 |
| 4 | Concrete placer pump | Hour | 16 | 147 | 2352 |
|  | Fuel charges | Hour | 16 | 6 | 96 |
| 5 | Needle Vibrator / Shutter vibrator | Hour | 16 | 8 | 128 |
|  | Fuel charges | Hour | 16 | 6 | 96 |
| 6 | Pump 10 hp | Hour | 8 | 5 | 40 |
|  | Fuel charges | Hour | 8 | 64 | 512 |
| 7 | Sundries | LS | 2 | 44 | 88 |
|  |  |  |  | Total | 63680 |


| Add for small Tools and Plants | @ 1\% | 636.80 |
| :--- | :--- | :--- |
| Add for Contractor's Profit on Energy | @ $10 \%$ | 3429.60 |
| Add for Contractor's Overheads | @ 5\% | 3184 |
| Total hire charges of Machinery |  | $\mathbf{7 0 9 3 0 . 4 0}$ |

## C.LABOUR

| S.N | Description | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Crew charges for Air compressor | Hour | 16 | 94 | 1504 |
| 2 | Crew charges for Batching plant | Hour | 16 | 181 | 2896 |
| 3 | Crew charges for Agitator car | Hour | 32 | 151 | 4832 |
| 4 | Crew charges for placer pump | Hour | 16 | 48 | 768 |
| 5 | Crew charges for vibrato | Hour | 16 | 90 | 1440 |
| 6 | Crew charges for Pump | Hour | 8 | 45 | 360 |
| 7 | Stone chiseller Class - 1 |  |  |  |  |
|  | for scaling \& cleaning | Day | 0.5 | 241.73 | 120.87 |
| 8 | Surveyer |  |  |  |  |
|  | for laying / aligning track | Day | 0.5 | 284.73 | 142.37 |
|  | for moving / positioning gantry | Day | 0.5 | 284.73 | 142.37 |
| 9 | Foreman |  |  |  |  |
|  | for laying / aligning track | Day | 0.5 | 276.73 | 138.37 |
|  | for releasing / moving gantry | Day | 0.5 | 276.23 | 138.37 |
| 10 | Khalasi |  |  |  |  |
|  | for releasing / moving gantry ( $4 \times 0.5$ ) | Day | 2 | 241.23 | 482.46 |
| 11 | Fitter shuttering |  |  |  |  |
|  | for bulk head / placer pipe fixing ( $0.5 \times 2$ | Day | 1 | 244.23 | 244.23 |
| 12 | Helper shuttering |  |  |  |  |
|  | for bulk head / placer pipe fixing ( $0.5 \times 2$ | Day | 1 | 239.73 | 239.73 |
| 13 | Cement handling mazdoor |  |  |  |  |
|  | for loading cement to BP bin ( $2 \times 2$ ) | Day | 4 | 239.73 | 958.92 |
| 14 | Heavy mazdoor |  |  |  |  |
|  | for loading CA to BP bins | Day | 6 | 238.73 | 1432.38 |
|  | for loading FA to BP bin | Day | 4 | 238.73 | 954.92 |
|  | for miscellaneous works of BP ( $1 \times 2$ ) | Day | 2 | 238.73 | 477.46 |
|  | for misc works @ placer point ( $1 \times 2$ ) | Day | 2 | 238.73 | 477.46 |
| 15 | Mason Class-1 |  |  |  |  |
|  | for Laying concrete by placer ( $1 \times 2$ ) | Day | 2 | 256.73 | 513.46 |
| 16 | Light mazdoor |  |  |  |  |
|  | for loading CA to BP bins | Day | 6 | 237.23 | 1423.38 |
|  | for loading FA to BP bin | Day | 4 | 237.23 | 948.92 |
|  | for curing / miscellaneous | Day | 2 | 237.23 | 474.46 |
| 17 | Maistry ( $2 \times 2$ ) | Day | 4 | 241.23 | 964.92 |
|  |  |  |  | Total | 22075.05 |


| Add for small Tools and Plants | @ $1 \%$ | 220.75 |
| :--- | :--- | :--- |
| Add for Contractor's Profit | @ $10 \%$ | 2207.5 |


| Add for hidden cost on Labour | @ $15 \%$ | 3311.25 |
| :--- | :--- | :--- |
| Add for additional hidden cost on labour | @ $10 \%$ | 2207.5 |
| Add for Contractor's Overheads | @ $5 \%$ | 1103.75 |
| Total cost of Labor |  | $\mathbf{3 1 1 2 5 . 7}$ <br> $\mathbf{9}$ |

### 3.35 Abstract of cost details for Overt lining in Diversion tunnel by Drill \& Blast method

| A. Cost of Materials | 1002576.745 |  |
| :--- | :--- | :--- |
| B. Hire charges of Machinery | 70930.40 |  |
| C. Cost of Labour | 31125.79 |  |
| TOTAL | $\mathbf{1 1 0 4 6 3 2 . 9 3 5}$ |  |
| Add for Air and Water line $0.80 \%$ | 8837.0635 |  |
| Add for Lighting | @ 1.80 | 19883.3928 |
| Add for Electrical sub-station charges @ 3.80\% | 41976.0516 |  |
| Add for other enabling works @ $1.70 \%$ | 18778.7599 |  |
| Total cost for $\mathbf{2 4 8 . 1} \mathbf{m}^{\mathbf{3}}$ | 1194108.202 |  |
| Cost for per $\boldsymbol{m}^{\mathbf{3}}$ | $\mathbf{4 8 1 3 . 0 1 1 7}$ |  |

Total cost for Overt Lining $\left(16.54 \mathrm{~m}^{2}\right) \times(472 \mathrm{~m}) \times(4813.0117) \quad: 37574604.78$
Total cost in DT- 1 (Excavation + Rock bolt support + Kerb \& Invert Lining + Overt Lining):
( $90 \%$ without rib support $+10 \%$ with rib support + Good \& Fair rock + Poor \& Very Poor rock + Kerb \& Invert lining + Overt lining):
$(20952655.98+3570035.866+3009034.353+1195750.078+33143179.2+$ $37574604.78)=\mathbf{9 9 4 4 5 2 6 0 . 2 6}$

Total cost in DT- 2 (Excavation + Rock bolt support + Kerb \& Invert Lining + Overt Lining):

Length of DT - 2 :552 m
$90 \%$ consideration without rib support:
Cost: $\quad\left(401.0047 \times 496.8 \mathrm{~m} \times 123 \mathrm{~m}^{2}\right) \quad=24503953.6$
$10 \%$ consideration with rib support:
Cost: $\quad\left(614.9297 \times 55.2 \mathrm{~m} \times 123 \mathrm{~m}^{2}\right) \quad=4175126.691$
Kerb and Invert Lining:
Cost: $\quad(4+4+3.1) \times(552 \mathrm{~m}) \times(6326) \quad=38760667.2$

Overt Lining:
Cost: $\quad\left(16.54 \mathrm{~m}^{2}\right) \times 552 \mathrm{~m} \times 4813.0117 \quad=\mathbf{4 3 9 4 3 1 8 1 . 8 6}$
( $90 \%$ without rib support $+10 \%$ with rib support + Good \& Fair rock + Poor \& Very Poor rock + Kerb \& Invert lining + Overt lining) :
$(24503953.6+4175126.691+3672123.261+1619672.361+38760667.2+43943181.86)$
$=116674725$

Total cost in DT- 2
: 116674725

Total cost of Diversion Tunnel (99445260+116674725)
: 216119985

### 3.36 Cost estimation in Pressure shaft by Drill \& Blast method

ITEM: Excavation for tunnel in the case of Diversion Tunnel by heading and benching.

| DATA Size of tunnel assumed (finished section) | 7.645 m dia |
| :--- | :--- |
| Shape of tunnel assumed for excavation | Horse-shoe shaped |
| Height of tunnel assumed (finished section) | 7.645 m dia |


| Length of Pressure Shaft $\quad(211+197+184+172) \mathrm{m}$ | 764 m |
| :--- | :--- |
| Thickness of lining | 0.70 m |
| Diameter of tunnel upto pay line for excavation | 7.645 m |

## Consideration for $\mathbf{3} \mathbf{m}$ pull length:

## Checking alignment and marking hole locations:

Use drilling jumbo for 1 hour for marking hole locations.

## Drilling holes.

The depth of hole for 3.0 m pull is considered at 2.0 m

| Heading portion |  |
| :---: | :---: |
| Area of excavation upto payline | $34.0369 \mathrm{~m}^{2}$ |
| Drilling depth | 2.0 m |
| No. of holes considering 2.0 holes per $m^{2} \quad(34.0369 \times 2.0)$ | 69 Nos |
| Drilling depth for 69 holes ( $69 \times 2.0 \times 1.1)$ | 151.8 m |
| Benching portion |  |
| Area of excavation upto payline | $13.8665 \mathrm{~m}^{2}$ |
| Drilling depth | 2.0 m |
| No. of holes considering 2.0 holes per $m^{2} \quad(13.8665 \times 2.0)$ | 28 Nos |
| Drilling depth for 80 holes ( $28 \times 2.0 \times 1.1$ ) | 61.6 m |
| Total depth of drilling (151.8+61.6) | 213.4 m |
| Loading explosive and blasting |  |
| Total area of excavation (34.0369+13.8665) | $47.9034 \mathrm{~m}^{2}$ |
| Depth of pull per blast for 2.0 m deep holes | 3.0 m |
| Quantity of in-situ excavation per blast (47.9034×3.0) | $143.7102 \mathrm{~m}^{3}$ |
| Quantity of explosive small dia per blast @ 0.8 kg per $m^{3}(143.7102 \times 0.8)$ | 114.96 kg |
| Quantity of explosive for secondary blasting @ 10 \% | 11.49 kg |
| Quantity of delay detonators per blast (69+28) | 97 Nos. |
| Quantity of electric detonators for secondary blasting (LS) | 10 Nos. |
| Detonating fuse coil | 213.4 Rm |

## Requirement of materials

| Explosive small dia $\quad(114.96+11.49)$ | 126.45 kg |
| :--- | :--- | :--- |
| Elecic short delay detonators $\quad(69+28)$ | 97 Nos |
| Electric detonators for secondary blasting | 10 Nos |

RATE ANALYSIS
UNIT
: $143.7102 \mathrm{~m}^{3}$

## A.MATERIALS

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| 1 | Small dia explosive | kg | 126.45 | 60 | 7587 |
| 2 | Delay detonators | Nos | 97 | 20 | 1940 |
| 3 | Electric detonator | Nos | 10 | 12 | 120 |
| 4 | Detonating fuse coil | Rm | 213.4 | 9 | 1920.6 |
| 5 | Use rate of drill rod 2.0 m long | Rm | 214 | 47.83 | 10235.62 |
|  | Reconditioning charges @ $10 \%$ |  |  |  | 1023.562 |
| 6 | Use rate of air hose | Hour | 32 | 6.25 | 200 |
| 7 | Use rate of water hose | Hour | 32 | 5.78 | 185 |
| 8 | Sundries (paint / template etc ) | LS | 9 | 44 | 396 |
|  |  |  |  | Total | 23607.782 |


| Add for small Tools and Plants | @ 1 | 236.077 |
| :--- | :--- | :--- |
| Add for Contractor's Profit | @ $10 \%$ | 2360.778 |
| Add for Contractor's Overheads | @ $5 \%$ | 1180.389 |
| Total cost of Material |  | $\mathbf{2 7 3 8 5 . 0 2 6}$ |
| Add for Air and Water line | @ $0.80 \%$ | 743.967 |
| Add for Ventilation | @ $6.0 \%$ | 5579.759 |

### 3.37 Abstract of cost details of 3m Pull length in Pressure shaft by Drill <br> \& Blast method

| A.Cost of Materials | 27385.026 |
| :--- | :--- |
| B.Hire charges of Machinery | 37868.2 |
| C.Cost of Labour | 27742.7634 |
| TOTAL | $\mathbf{9 2 9 9 5 . 9 8 9 4}$ |
| Add for Lighting $1.80 \%$ | 1673.927 |
| Add for Electrical sub-station / Demand charges @ $3.80 \%$ | 3533.847 |
| Add for other Enabling works | @ $1.70 \%$ |


| Total cost for $143.7102 \mathrm{~m}^{3}$ | 106108.4204 |
| :--- | :--- |


| Rate per $\boldsymbol{m}^{\mathbf{3}}$ | $\mathbf{7 3 8 . 3 4 9}$ |
| :--- | :--- |
| For $\mathbf{1}$ cycle (3 m pull length) rate per $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{7 3 8 . 3 4 9}$ |
| Total length of Pressure Shaft $\quad \mathbf{( 2 1 1 + 1 9 7 + \mathbf { 1 8 4 } + \mathbf { 1 7 2 } \mathbf { ) }}$ | $\mathbf{7 6 4} \mathbf{~ m}$ |
| $\mathbf{9 0} \%$ considered without rib support |  |
| Total length in case of without rib support | 687.6 m |
| Total cost $\mathbf{( 7 3 8 . 3 4 9 \times \mathbf { 6 8 7 . 6 } \mathbf { ~ m } \times \mathbf { 4 7 . 9 0 3 4 } \mathbf { m } ^ { \mathbf { 2 } } \mathbf { ) }}$ | $\mathbf{2 4 3 2 0 0 1 8 . 3 4}$ |

## Consideration for 1.5 m pull length:

| Heading portion |  |
| :---: | :---: |
| Area of excavation upto payline | $34.0369 \mathrm{~m}^{2}$ |
| Drilling depth | 1.0 m |
| No. of holes considering 2.0 holes per $m^{2} \quad(34.0369 \times 2.0)$ | 69 Nos |
| Drilling depth for 165 holes $\quad(\mathbf{6 9 \times 1 . 0 \times 1 . 1 )}$ | 75.9 m |
| Benching portion |  |
| Area of excavation upto payline | $13.8665 \mathrm{~m}^{2}$ |
| Drilling depth | 1.0 m |
| No. of holes considering 2.0 holes per $m^{2} \quad(13.8665 \times 2.0)$ | 28 Nos |
| Drilling depth for 80 holes $\quad \mathbf{( 2 8 \times 1 . 0 \times 1 . 1 )}$ | 30.8 m |
| Total depth of drilling $\quad \mathbf{( 7 5 . 9 + 3 0 . 8 ) ~ m}$ | 106.7 m |
| Loading explosive and blasting |  |
| Total area of excavation | $47.9034 \mathrm{~m}^{2}$ |
| Depth of pull per blast for 1.0 m deep holes | 1.5 m |
| Quantity of in-situ excavation per blast (47.9034×1.5) | $71.8551 \mathrm{~m}^{3}$ |
| Quantity of explosive small dia per blast @ 0.8 kg per $m^{3}(71.8551 \times 0.8)$ | 57.4840 kg |
| Quantity of explosive for secondary blasting @ $10 \%$ | 5.7484 kg |
| Quantity of delay detonators per blast (69+28) | 97 Nos. |


| Quantity of electric electric detonators for secondary blasting (LS) | 10 Nos. |
| :--- | :---: |
| Detonating fuse coil | 213.4 Rm |
| Requirement of materials |  |
| Explosive small dia $\quad \mathbf{( 5 7 . 4 8 4 0 + 5 . 7 4 8 4 )}$ | $\mathbf{6 3 . 2 3 2 4} \mathbf{~ k g}$ |
| Elecic short delay detonators $\quad \mathbf{( 6 9 + 2 8 )}$ | $\mathbf{9 7} \mathbf{N o s}$ |
| Electric detonators for secondary blasting | $\mathbf{1 0} \mathbf{N o s}$ |
| Fuse coil | $\mathbf{2 1 3 . 4} \mathbf{~ R m}$ |

## RATE ANALYSIS UNIT : 71.8551 $\mathrm{m}^{\mathbf{3}}$

## A.MATERIALS

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Small dia explosive | kg | 63.232 | 60 | 3793.944 |
| 2 | Delay detonators | Nos | 97 | 20 | 1940 |
| 3 | Electric detonator | Nos | 10 | 12 | 120 |
| 4 | Detonating fuse coil | Rm | 213.4 | 9 | 1920.6 |
| 5 | Use rate of drill rod 2.0 m long | Rm | 200 | 47.83 | 9566 |
|  | Reconditioning charges @ $10 \%$ |  |  |  | 956.6 |
| 6 | Use rate of air hose | Hour | 32 | 6.25 | 200 |
| 7 | Use rate of water hose | Hour | 32 | 5.78 | 185 |
| 8 | Sundries ( paint / template etc ) | LS | 9 | 44 | 396 |
|  |  |  |  | Total | 19078.144 |


| Add for small Tools and Plants | $@$ 1 | 190.781 |
| :--- | :--- | :---: |
| Add for Contractor's Profit | $@ 10 \%$ | 1907.814 |
| Add for Contractor's Overheads | $@ 5 \%$ | 953.907 |
| Total cost of Material |  | $\mathbf{2 2 1 3 0 . 6 4 6}$ |

### 3.38 Abstract of cost details for 1.5 m pull length in Pressure shaft by Drill \& Blast method

| A.Cost of Materials | 22130.646 |
| :--- | :--- |
| B.Hire charges of Machinery | 37868.2 |
| C.Cost of Labour | 27742.7634 |


| TOTAL | 87741.6094 |
| :---: | :---: |
| Add for Air and Water line @ 0.80 \% | 701.932 |
| Add for Ventilation @ 6.0\% | 5264.496 |
| Add for Lighting @ 1.80 \% | 1579.348 |
| Add for Ele sub-station / Demand charges @ 3.80 \% | 3334.181 |
| Add for other Enabling works @ 1.70 \% | 1491.607 |
| Total cost for $71.8551 \mathrm{~m}^{\mathbf{3}}$ | 100113.173 |
| Rate per $\mathrm{m}^{3}$ | 1393.264 |


| For 1 cycle ( 1.5 m pull length) rate per $\mathrm{m}^{\mathbf{3}}$ | 1393.264 |
| :---: | :---: |
| Total length of Pressure Shaft ( $211+197+184+172)$ m | 764 m |
| 10 \% considered with rib support |  |
| Total length in case of without rib support | 76.4 m |
| Total cost ( $\left.1393.264 \times 76.4 \mathrm{~m} \times 47.9034 \mathrm{~m}^{2}\right)$ | 5099095.118 |
| Total cost in Excavation for Pressure Shaft    <br> $\mathbf{( 2 4 3 2 0 0 1 8 . 3 4 + 5 0 9 9 0 9 5 . 1 1 8 )}$    | 29419113.46 |

### 3.39 Cost estimation for rock bolts support work in Pressure shaft by Drill \& Blast method

## Rock bolt calculation:

Distance in Good $\operatorname{Rock}(15 \%)+$ Fair $\operatorname{Rock}(60 \%)$ of $(211+197+184+172=764 \mathrm{~m})$ : 573 m

In 3 m stretch 17 Nos of Rock bolt is required.
So rock bolt only needed in Heading.
So 9 Nos of Rock bolt is required

| Nos of cycle in Pressure Shaft for rock bolt | $(573 \mathrm{~m} / 3 \mathrm{~m})$ | $: 191$ Nos |
| :--- | :--- | :--- |
| Nos of rock bolt in 573 m | $(191 \times 9)$ | $: 1719$ Nos |


| For Good and Fair Rock |  |
| :--- | :--- |
| Length of rock bolt excluding threaded portion for 1719 bolts (1719×4) | 6876 m |


| Quantity of drilling for 1416 bolts | 764 m |
| :---: | :---: |
| Rate of drilling for rock bolts including shifting | $4 \mathrm{~m} / \mathrm{hr}$ |
| Time for drilling 6876 m with 4 jack hammers (6876 / 4 / 4) say | $429.75$ <br> hour |
| For Poor and V. Poor Rock |  |
| Distance in Poor Rock(15\%) + V.Poor Rock(10\%) of m | 191 m |
| In 3 m stretch 22 Nos of Rock bolt is required. |  |
| So rock bolt only needed in Heading. |  |
| So 11 Nos of Rock bolt is required |  |
| Nos of cycle in Pressure Shaft for rock bolt (191m/3m) | 63.66 Nos |
| Nos of rock bolt in 191 m | 700 Nos |
| Length of rock bolt excluding threaded portion for 700 bolts (700×4) | 2800 m |
| Quantity of drilling for 700 bolts | 764 m |
| Rate of drilling for rock bolts including shifting | $4 \mathrm{~m} \text { per }$ <br> hour |
| Time for drilling 2516 m with 4 jack hammers ( $2800 / 4 / 4$ ) say | 175 hour |


| Requirement of materials (for Good(15\%) And Fair Rock (60) |  |
| :---: | :---: |
| Quantity of 25 mm dia bars for (1719) bolts with $2.5 \%$ wastage $(1719 \times 4.15 \times 3.85 \times 1.025)$ | 28151.955 kg |
| Quantity of washer for 1719 bolts with $2.5 \%$ wastage $(1719 \times 4 \times 0.2 \times 0.2 \times 78.5 \times 1.025)$ | 22130.406 kg |
| Quantity of nuts for 1719 bolts (1719 $\times 2 \times 0.2)$ | 687.6 kg |
| Quantity of grout capsule for 1719 bolts (1719 x 1) | 1719 Nos |
| Requirement of materials (for Poor (15\%) And V. Poor Rock (10\%)) |  |
| Quantity of 25 mm dia bars for (700) bolts with $2.5 \%$ wastage $(700 \times 4.15 \times 3.85 \times 1.025)$ | 11463.856 kg |
| Quantity of washer for 700 bolts with $2.5 \%$ wastage $(700 \times 4 \times 0.2 \times 0.2 \times 78.5 \times 1.025)$ | 9011.8 kg |
| Quantity of nuts for 700 bolts $\quad(700 \times 2 \times 0.2)$ | 280 kg |


| Quantity of grout capsule for 700 bolts $\quad(700 \times 1)$ | 700 Nos |
| :--- | :--- | :--- |

RATE ANALYSIS (Good \&Fair Rock) UNIT : 6876.0 Rm

## A.MATERIALS

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rein.Steel with 2.5 \% wastage | kg | 28151.96 | 48.48 | 1364806.778 |
| 2 | Steel plate for washers | kg | 22130.41 | 51.14 | 1131748.963 |
| 3 | Resin bond cement grout capsule | Nos | 1719 | 65 | 111735 |
| 4 | M S Nuts for bolts | kg | 687.6 | 90 | 61884 |
| 5 | Use rate of drill rod | Rm | 6876 | 47.83 | 328879.08 |
|  | Reconditioning charges @ $10 \%$ |  |  |  | 32887.908 |
| 6 | Use rate of air hose 4 Nos | Hour | 6 | 6.25 | 37.5 |
| 7 | Use rate of water hose 4 Nos | Hour | 6 | 5.78 | 34.69 |
| 8 | Sundries(gas for cutting etc) | LS | 5 | 44 | 220 |
|  |  |  |  | Total | 3032233.919 |


| Add for small Tools and Plants | @ 1\% | 30322.339 |
| :--- | :--- | :---: |
| Add for Contractor's Profit | @ $10 \%$ | 303223.391 |
| Add for Contractor's Overheads | @ 5\% | 151611.696 |
| Total cost of Materials |  | $\mathbf{3 5 1 7 3 9 1 . 3 4 5}$ |
| RATE ANALYSIS (Poor \& V. Poor Rock) | UNIT | $\mathbf{~ 2 8 0 0 . 0 ~ R m}$ |

## A.MATERIALS:

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rein.Steel with 2.5 \% wastage | kg | 11463.9 | 48.48 | 555767.738 |
| 2 | Steel plate for washers | kg | 9011.8 | 51.14 | 460863.452 |
| 3 | Resin bond cement grout capsule | Nos | 700 | 65 | 45500 |
| 4 | M S Nuts for bolts | kg | 280 | 90 | 25200 |
| 5 | Use rate of drill rod | Rm | 2800 | 47.83 | 133924 |
|  | Reconditioning charges @ 10\% |  |  |  | 13392.4 |
| 6 | Use rate of air hose 4 Nos | Hour | 6 | 6.25 | 37.5 |
| 7 | Use rate of water hose 4 Nos | Hour | 6 | 5.78 | 34.69 |
| 8 | Sundries(gas for cutting etc) | LS | 5 | 44 | 220 |
|  |  |  |  | Total | 1234939.78 |


| Add for small Tools and Plants | @ 1\% | 12349.397 |
| :--- | :--- | :--- |
| Add for Contractor's Profit | @ 10\% | 123439.978 |
| Add for Contractor's Overheads | @ 5\% | 61746.989 |


| Total cost of Materials |  | 1432476.144 |
| :--- | :--- | :--- |

### 3.40 Abstract of cost details for Rock bolt support in Pressure shaft by Drill \& Blast method

| For Good and fair Rock |  |
| :--- | :---: |
| A. Cost of Materials | 3517391.345 |
| B. Hire charges of Machinery | 4073.28 |
| C. Cost of Labour | 4371.02 |
| TOTAL | $\mathbf{3 5 2 5 8 3 5 . 6 4 5}$ |
| Add for Air and Water line @ $0.80 \%$ | 28206.685 |
| Add for Lighting | @ $1.80 \%$ |
| Add for Ele sub-station / Demand charges @ 3.80\% | 63465.041 |
| Add for other enabling works @ $1.70 \%$ | 133981.754 |
| TOTAL | 59939.205 |
| Add for 1 km rehandling lead charges | $\mathbf{3 8 1 1 4 2 8 . 3 3}$ |
| For steel 150 kg @ 218.40 per tonne $(0.15 \times 218.40)$ |  |
| Total cost for 6876 Rm | 32.76 |


| For Poor and V. Poor Rock |  |
| :--- | :---: |
| A. Cost of Materials | 1432476.144 |
| B. Hire charges of Machinery | 4073.28 |
| C. Cost of Labour | 4371.02 |
| TOTAL | $\mathbf{1 4 4 0 9 2 0 . 4 4 4}$ |
| Add for Air and Water line $0.80 \%$ | 11527.363 |
| Add for Lighting | @ $1.80 \%$ |
| Add for Eletrical sub-station / Demand charges @ $3.80 \%$ | 25936.567 |
| Add for other enabling works | @ $1.70 \%$ |
| TOTAL | 54754.976 |
| Add for 1 km rehandling lead charges | 24495.647 |
| For steel 150 kg @ 218.40 per tonne $(0.15 \times 218.40)$ | 1557634.997 |

Total cost for Rock bolt support work in (Good \& Fair Rock + Poor \& Very Poor Rock):
Total cost for Rock bolt support work (3811461.09+1557667.757):
5369128.847

### 3.41 Cost estimation for kerb \& invert lining in Pressure shaft by Drill \& Blast method

$$
\text { Rate per } m^{3} \quad: 6326.00
$$

Total cost for Kerb and Invert Lining $(1.3+1.3+1.3)=3.9 \mathrm{~m}^{2} \times 764 \mathrm{~m} \times 6326=$ 18848949.6

### 3.42 Cost estimation for overt lining in Pressure shaft by Drill \& Blast method

| Assume 15 m long collapsible type steel gantry |  |
| :---: | :---: |
| Quantity of concrete per gantry considering 0.7 m thick lining ( $9.79 \boldsymbol{m}^{2} \times 15 \mathrm{~m}$ ) | $146.85 \mathrm{~m}^{3}$ |
| Concrete for filling support reaches @ 45 \% | $66.082 \mathrm{~m}^{3}$ |
| Average quantity of concrete per gantry length of lining say | $146.85 \mathrm{~m}^{3}$ |
| Requirement of materials |  |
| Cement for mix with 1 \% wastage ( $146.85 \times 300 \times 1.01$ ) | 4495.55 kg |
| Cement for incidentals @ 1 kg per $\mathrm{m}^{3} \quad(146.85 \times 1)$ | 146.85 kg |
| Coarse aggregate $40-20 \mathrm{~mm}$ size range ( $146.85 \times 0.79 \times 0.5 \times 1.02$ ) | $59.165 \mathrm{~m}^{3}$ |
| Coarse aggregate $20-10 \mathrm{~mm}$ size range ( $146.85 \times 0.79 \times 0.3 \times 1.02$ ) | $35.499 \mathrm{~m}^{\mathbf{3}}$ |
| Coarse aggregate $10-4.75 \mathrm{~mm}$ size $\quad(146.85 \times 0.79 \times 0.2 \times 1.02)$ | $23.666 \mathrm{~m}^{3}$ |
| Fine aggregate ( $146.85 \times 0.425 \times 1.02)$ | $63.659 \mathrm{~m}^{\mathbf{3}}$ |
| Super plasticiser ( $146.85 \times 0.90 \times 1.02)$ | 143.808 litres |

## A.MATERIALS:

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Cement 43 Gr | kg | 4495.6 | 7.5 | 33716.625 |
|  | Cement for incidentals @ 1 kg per cum | kg | 146.85 | 7.5 | 1101.375 |
| 2 | Fine aggregate ( screened ) | cum | 63.659 | 730 | 46471.07 |
| 3 | Coarse aggregate $40-20 \mathrm{~mm}$ | cum | 59.165 | 740 | 43782.1 |
|  | Coarse aggregate $20-10 \mathrm{~mm}$ | cum | 35.499 | 950 | 33724.05 |
|  | Coarse aggregate 10-4.75 mm | cum | 23.666 | 1160 | 27452.56 |
| 4 | Super plasticiser | litre | 143.81 | 105 | 15099.84 |
| 5 | Use rate of end shuttering | sqm | 6 | 158.77 | 952.6 |
| 6 | Use rate of steel gantry | sqm | 100 | 176.95 | 17695.03 |
| 7 | Sundries ( placer pipe etc ) | LS | 5 | 44 | 220 |
|  |  |  |  | Total | 220215.25 |


| Add for small Tools and Plants | @ 1\% | 2202.152 |
| :--- | :--- | :--- |
| Add for Contractor's Profit on Energy | @ $10 \%$ |  |
| Add for Contractor's Overheads | @ $5 \%$ | 22021.525 |
| Total cost of Materials |  | 11010.762 |

### 3.43 Abstract of cost details for Overt lining in Pressure shaft by Drill \& Blast method

| A. Cost of Materials | 255449.689 |  |
| :--- | :---: | :---: |
| B. Hire charges of Machinery | 70930.40 |  |
| C. Cost of Labour | 31125.79 |  |
| TOTAL | $\mathbf{3 5 7 5 0 5 . 8 7 9}$ |  |
| Add for Air and Water line @ $0.80 \%$ | 2860.047 |  |
| Add for Lighting | @ 1.80 | 643510.582 |
| Add for Electrical sub-station charges @ $3.80 \%$ | 13585.223 |  |
| Add for other enabling works $\quad$ @ $1.70 \%$ | 607759.994 |  |
| Total cost for $\mathbf{1 4 6 . 8 5} \mathbf{m}^{\mathbf{3}}$ | $\mathbf{1 6 2 5 2 2 1 . 6 7 1}$ |  |


| Cost for per $\boldsymbol{m}^{3}$ | 11067.22 |
| :--- | :--- |

Total cost for Overt Lining $\left(9.79 \mathrm{~m}^{2}\right) \times(764 \mathrm{~m}) \times(11067.22)$ : 82777936.02

Total cost in Pressure Shaft (Excavation + Rock bolt support + Kerb \& Invert Lining + Overt Lining):
( $90 \%$ without rib support $+10 \%$ with rib support + Good \& Fair rock + Poor \& Very Poor rock + Kerb \& Invert lining + Overt lining):
$(24320018.34+5099095.118+3811461.09+1557667.757+18848949.6+82777936.02)$ $=136415128$

### 3.44 Cost estimation in Tailrace tunnel by Drill \& Blast method

ITEM: Excavation for tunnel in the case of Diversion Tunnel by heading and benching.

| DATA Size of tunnel assumed (finished section) | 9.645 m dia |
| :--- | :--- |
| Shape of tunnel assumed for excavation | Horse-shoe shaped |
| Height of tunnel assumed (finished section) | 9.645 m dia |
| Length of Pressure Shaft $\quad(502+490+475+460) \mathrm{m}$ | 1927 m |
| Thickness of lining | 0.70 m |
| Diameter of tunnel upto pay line for excavation | 9.645 m |

## Consideration for $\mathbf{3} \mathbf{m}$ pull length:

## Checking alignment and marking hole locations:

Use drilling jumbo for 1 hour for marking hole locations.

## Drilling holes.

The depth of hole for 3.0 m pull is considered at 2.0 m

| Heading portion |  |
| :--- | :---: |
| Area of excavation upto payline | $52.44 \mathrm{~m}^{2}$ |
| Drilling depth | 2.0 m |
| No. of holes considering 2.0 holes per $m^{2}$ | $(52.44 \times 2.0)$ |
| Drilling depth for 105 holes | 105 Nos |
| Benching portion | 231 m |
| Area of excavation upto payline | $23.21 \mathrm{~m}^{2}$ |
| Drilling depth | 2.0 m |


| No. of holes considering 2.0 holes per $m^{2} \quad(23.21 \times 2.0)$ | 47 Nos |
| :---: | :---: |
| Drilling depth for 47 holes $(47 \times 2.0 \times 1.1)$ | 103.4 m |
| Total depth of drilling (231+103.4) m | 334.4 m |
| Loading explosive and blasting |  |
| Total area of excavation | $75.65 \mathrm{~m}^{2}$ |
| Depth of pull per blast for 2.0 m deep holes | 3.0 m |
| Quantity of in-situ excavation per blast (75.65 $\times \mathbf{3 . 0}$ ) | $226.95 \mathrm{~m}^{3}$ |
| Quantity of explosive small dia per blast @ 0.8 kg per $m^{3}(226.95 \times 0.8)$ | 181.56 kg |
| Quantity of explosive for secondary blasting @ $10 \%$ | 18.156 kg |
| Quantity of delay detonators per blast (105+47) | 152 Nos |
| Quantity of electric detonators for secondary blasting (LS) | 10 Nos |
| Detonating fuse coil | 305 Rm |


| Requirement of materials $\quad(181.56+18.156)$ |  |
| :--- | :--- |
| Explosive small dia $\quad(105+47)$ | 199.716 kg |
| Elecic short delay detonators | 152 Nos |
| Electric detonators for secondary blasting | 10 Nos |
| Fuse coil | 305 Rm |

RATE ANALYSIS
UNIT
: $\mathbf{2 2 6 . 9 5} \mathrm{m}^{\mathbf{3}}$

## A.MATERIALS

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Small dia explosive | kg | 199.72 | 60 | 11983.2 |
| 2 | Delay detonators | Nos | 152 | 21 | 3192 |
| 3 | Electric detonator | Nos | 10 | 12 | 120 |
| 4 | Detonating fuse coil | Rm | 305 | 9 | 2745 |
| 5 | Use rate of drill rod 2.0 m long | Rm | 334.4 | 47.83 | 15994.352 |
|  | Reconditioning charges @ 10\% |  |  |  | 1599.435 |
| 6 | Use rate of air hose | Hour | 32 | 6.25 | 200 |
| 7 | Use rate of water hose | Hour | 32 | 5.78 | 185 |
| 8 | Sundries (paint / template etc ) | LS | 9 | 44 | 396 |
|  |  |  |  | Total | 36414.987 |


| Add for small Tools and Plants | @ 1 | 364.149 |
| :--- | :--- | :---: |
| Add for Contractor's Profit | @ $10 \%$ | 3641.498 |
| Add for Contractor's Overheads | @ $5 \%$ | 1820.749 |
| Total cost of Material |  | $\mathbf{4 2 2 4 1 . 3 8 3}$ |

### 3.45 Abstract of cost details for 3 m Pull length in Tailrace tunnel by Drill \& Blast method

| A. Cost of Materials | 42241.383 |
| :---: | :---: |
| B. Hire charges of Machinery | 37868.2 |
| C.Cost of Labour | 27742.7634 |
| TOTAL | 107852.346 |
| Add for Air and Water line @ 0.80 \% | 862.818 |
| Add for Ventilation @ 6.0 \% | 6471.140 |
| Add for Lighting @ 1.80\% | 1941.342 |
| Add for Electrical sub-station / Demand charges @ 3.80 \% | 4098.389 |
| Add for other Enabling works @ 1.70 \% | 183348.988 |
| Total cost for $226.95 \mathrm{~m}^{\mathbf{3}}$ | 304575.015 |
| Rate per $\mathrm{m}^{3}$ | 1342.035 |


| For $\mathbf{1}$ cycle (3 $\mathbf{m}$ pull length) rate per $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{1 3 4 2 . 0 3 5}$ |
| :--- | :--- |
| Total length of Tailrace Tunnel $\quad \mathbf{5 0 2 + \mathbf { 4 9 0 } + \mathbf { 4 7 5 } + \mathbf { 4 6 0 } )}$ | $\mathbf{1 9 2 7} \mathbf{~ m}$ |
| $\mathbf{9 0} \%$ considered without rib support |  |
| Total length in case of without rib support | 1734.3 m |
| Total cost $\left(\mathbf{1 7 3 4 . 3} \mathbf{~ m} \times \mathbf{7 5 . 6 5} \mathbf{m}^{\mathbf{2}} \times \mathbf{1 3 4 2 . 0 3 5 )}\right.$ | $\mathbf{1 7 6 0 7 4 7 1 6 . 9}$ |

## Consideration for 1.5 m pull length:

| Heading portion |  |
| :--- | :---: |
| Area of excavation upto payline | $52.44 \mathrm{~m}^{2}$ |
| Drilling depth | 1.0 m |
| No. of holes considering 2.0 holes per $\mathrm{m}^{2} \quad(52.44 \times 2.0)$ | 105 Nos |
| Drilling depth for 105 holes $\quad \mathbf{( 1 0 5} \times \mathbf{1 . 0} \times \mathbf{1 . 1})$ | $\mathbf{1 1 5 . 5} \mathbf{~ m}$ |
| Benching portion |  |
| Area of excavation upto payline | $23.21 \mathrm{~m}^{2}$ |
| Drilling depth | 1.0 m |
| No. of holes considering 2.0 holes per $\mathrm{m}^{2}$ | $(23.21 \times 2.0)$ |
| Drilling depth for 47 holes | $\mathbf{( 4 7 \times \mathbf { 1 . 0 } \times \mathbf { 1 . 1 } )}$ |
| Total depth of drilling | $\mathbf{5 1 . 7} \mathbf{~ m}$ |
| Loading explosive and blasting | $\mathbf{( 1 1 5 . 5 + 5 1 . 7 ) ~ \mathbf { ~ m }}$ |
| Total area of excavation | $\mathbf{1 0 6 . 7} \mathbf{~ m}$ |
| Depth of pull per blast forl.0 m deep holes |  |
| Quantity of in-situ excavation per blast $\quad \mathbf{( 7 5 . 6 5} \times \mathbf{1 . 5 )}$ | $75.65 \mathrm{~m}^{2}$ |


| Quantity of explosive small dia per blast @ 0.8 kg per $\mathrm{m}^{3}(113.475 \times 0.8)$ | 90.78 kg |
| :--- | :---: |
| Quantity of explosive for secondary blasting @ $10 \%$ | 9.078 kg |
| Quantity of delay detonators per blast (105+47) | 152 Nos. |
| Quantity of electric electric detonators for secondary blasting (LS) | 10 Nos. |
| Detonating fuse coil | 305 Rm |


| Requirement of materials $\quad \mathbf{( 9 8 . 7 8 + 9 . 0 7 8 )}$ |  |
| :--- | :--- |
| Explosive small dia $\quad \mathbf{1 0 7 . 8 5 8} \mathbf{~ k g}$ |  |
| Elecic short delay detonators $\quad$ (105+47) | $\mathbf{1 5 2}$ Nos |
| Electric detonators for secondary blasting | $\mathbf{1 0}$ Nos |
| Fuse coil | $\mathbf{3 0 5} \mathbf{~ R m}$ |

## RATE ANALYSIS

UNIT
: $\mathbf{1 1 3 . 4 7 5} \mathrm{m}^{\mathbf{3}}$

## A.MATERIALS

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Small dia explosive | kg | 107.86 | 60 | 6471.48 |
| 2 | Delay detonators | Nos | 152 | 20 | 3040 |
| 3 | Electric detonator | Nos | 10 | 12 | 120 |
| 4 | Detonating fuse coil | Rm | 305 | 9 | 2745 |
| 5 | Use rate of drill rod 2.0 m long | Rm | 106.7 | 47.83 | 5103.461 |
|  | Reconditioning charges @ $10 \%$ |  |  |  | 510.346 |
| 6 | Use rate of air hose | Hour | 32 | 6.25 | 200 |
| 7 | Use rate of water hose | Hour | 32 | 5.78 | 185 |
| 8 | Sundries (paint / template etc ) | LS | 9 | 44 | 396 |
|  |  |  |  | Total | 18771.287 |


| Add for small Tools and Plants | @ 1 | 187.712 |
| :--- | :--- | :---: |
| Add for Contractor's Profit | $@ 10 \%$ | 1877.128 |
| Add for Contractor's Overheads | $@ 5 \%$ | 938.564 |
| Total cost of Material |  | $\mathbf{2 1 7 7 4 . 6 9 1}$ |

### 3.46 Abstract of cost details for 1.5m Pull length in Tailrace tunnel by Drill \& Blast method

|  |  |
| :--- | :---: |
| A.Cost of Materials | 21774.691 |
| B.Hire charges of Machinery | 37868.2 |


| C.Cost of Labour | 27742.7634 |
| :---: | :---: |
| TOTAL | 87385.654 |
| Add for Air and Water line @ 0.80 \% | 699.085 |
| Add for Ventilation @ 6.0\% | 5243.139 |
| Add for Lighting @ 1.80 \% | 1572.941 |
| Add for Ele sub-station / Demand charges @ 3.80 \% | 3320.654 |
| Add for other Enabling works @ 1.70 \% | 1485.556 |
| Total cost for $113.475 \mathrm{~m}^{3}$ | 99707.029 |
| Rate per $m^{3}$ | 878.669 |
| For 1 cycle ( 1.5 m pull length) rate per $\mathrm{m}^{3}$ | 878.669 |
| Total length of Tailrace Tunnel ( $502+490+475+460) \mathrm{m}$ | 1927 m |
| $10 \%$ considered with rib support |  |
| Total length in case of without rib support | 192.7 m |
| Total cost (192.7 m $\left.\times 75.65 \mathrm{~m}^{2} \times 878.669\right)$ | 12809021.41 |
| Total cost in Excavation for Tailrace Tunnel (176074716.9+12809021.41) $=$ 188883738.3 |  |

### 3.47 Cost estimation for rock bolts support work in Tailrace tunnel by Drill \& Blast method

## Rock bolt calculation:

Distance in Good $\operatorname{Rock}(15 \%)+$ Fair $\operatorname{Rock}(60 \%)$ of $(502+490+475+460=1927 \mathrm{~m})$ :
1445.25 m

In 3 m stretch 20 Nos of Rock bolt is required.
So rock bolt only needed in Heading.
So 10 Nos of Rock bolt is required
Nos of cycle in Pressure Shaft for rock bolt $\quad(1445.25 \mathrm{~m} / 3 \mathrm{~m}) \quad: 482$ Nos
Nos of rock bolt in $1445.25 \mathrm{~m} \quad(482 \times 10): 4820$ Nos

| For Good and Fair Rock |  |
| :--- | :---: |
| Length of rock bolt excluding threaded portion for 4820 bolts <br> $(4820 \times 4)$ | 19280 m |


| Quantity of drilling for 4820 bolts | 19280 m |
| :---: | :---: |
| Rate of drilling for rock bolts including shifting | $4 \mathrm{~m} / \mathrm{hr}$ |
| Time for drilling 19280 m with 4 jack hammers (6876 / 4 / 4) say | 1205 hour |
| For Poor and V. Poor Rock |  |
| Distance in Poor Rock(15\%) + V.Poor Rock(10\%) of m | 481.75 m |
| In 3 m stretch 26 Nos of Rock bolt is required. |  |
| So rock bolt only needed in Heading. |  |
| So 13 Nos of Rock bolt is required |  |
| Nos of cycle in Pressure Shaft for rock bolt ( $481.75 \mathrm{~m} / 3 \mathrm{~m}$ ) | 161 Nos |
| Nos of rock bolt in 481.75 m (161×13) | 2093 Nos |
| Length of rock bolt excluding threaded portion for 2093 bolts (2093×4) | 8372 m |
| Quantity of drilling for 2093 bolts | 8372 m |
| Rate of drilling for rock bolts including shifting | 4 m per hour |
| Time for drilling 8372 m with 4 jack hammers ( $2800 / 4 / 4$ ) say | 524 hour |


| Requirement of materials (for Good(15\%) And Fair Rock (60\%)) |  |
| :---: | :---: |
| Quantity of 25 mm dia bars for (4820) bolts with $2.5 \%$ wastage $(4820 \times 4.15 \times 3.85 \times 1.025)$ | 78936.838 kg |
| Quantity of washer for 4820 bolts with $2.5 \%$ wastage $(4820 \times 4 \times 0.2 \times 0.2 \times 78.5 \times 1.025)$ | 62052.68 kg |
| Quantity of nuts for 4820 bolts ( $4820 \times 2 \times 0.2)$ | 1928 kg |
| Quantity of grout capsule for 4820 bolts ( $4820 \times 1$ ) | 4820 Nos |
| Requirement of materials (for Poor (15\%) And V. Poor Rock (10\%)) |  |
| Quantity of 25 mm dia bars for (2093) bolts with $2.5 \%$ wastage $(2093 \times 4.15 \times 3.85 \times 1.025)$ | 34276.930 kg |
| Quantity of washer for 2093 bolts with $2.5 \%$ wastage $(2093 \times 4 \times 0.2 \times 0.2 \times 78.5 \times 1.025)$ | 26945.282 kg |
| Quantity of nuts for 2093 bolts (2093x $2 \times 0.2)$ | 837.2 kg |


| Quantity of grout capsule for 2093 bolts $\quad$ (2093 x 1) | 2093 Nos |
| :--- | :--- | :--- |

RATE ANALYSIS (Good \&Fair Rock) UNIT : 19280 Rm

## A.MATERIALS

| S.N | Perticulars | Unit |  |  | Quantity |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rein.Steel with 2.5 \% wastage | kg | 34277 | 48.48 | 1661745.566 |
| 2 | Steel plate for washers | kg | 26945 | 51.14 | 1377981.721 |
| 3 | Resin bond cement grout capsule | Nos | 2093 | 65 | 136045 |
| 4 | M S Nuts for bolts | kg | 837.2 | 90 | 75348 |
| 5 | Use rate of drill rod | Rm | 19280 | 47.83 | 922162.4 |
|  | Reconditioning charges @ 10\% |  |  |  | 92216.24 |
| 6 | Use rate of air hose 4 Nos | Hour | 6 | 6.25 | 37.5 |
| 7 | Use rate of water hose 4 Nos | Hour | 6 | 5.78 | 34.69 |
| 8 | Sundries(gas for cutting etc) | LS | 5 | 44 | 220 |
|  |  |  |  | Total | 4265791.117 |


| Add for small Tools and Plants | @ 1\% | 42657.911 |
| :--- | :--- | :--- |
| Add for Contractor's Profit | @ $10 \%$ | 426579.111 |
| Add for Contractor's Overheads | @ $5 \%$ | 213289.555 |
| Total cost of Materials |  | $\mathbf{4 9 4 8 3 1 7 . 6 9 4}$ |

## B.MATERIALS:

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Rein.Steel with 2.5 \% wastage | kg | 34277 | 48.48 | 1661745.566 |
| 2 | Steel plate for washers | kg | 26945 | 51.14 | 1377981.721 |
| 3 | Resin bond cement grout capsule | Nos | 2093 | 65 | 136045 |
| 4 | M S Nuts for bolts | kg | 837.2 | 90 | 75348 |
| 5 | Use rate of drill rod | Rm | 8372 | 47.83 | 400432.76 |
|  | Reconditioning charges @ 10\% |  |  |  | 40043.276 |
| 6 | Use rate of air hose 4 Nos | Hour | 6 | 6.25 | 37.5 |
| 7 | Use rate of water hose 4 Nos | Hour | 6 | 5.78 | 34.69 |
| 8 | Sundries(gas for cutting etc) | LS | 5 | 44 | 220 |
|  |  |  |  | Total | 3691888.513 |


| Add for small Tools and Plants | @ 1\% | 36918.885 |
| :--- | :--- | :--- |
| Add for Contractor's Profit | @ $10 \%$ | 369188.851 |
| Add for Contractor's Overheads | $@ 5 \%$ | 184594.425 |
| Total cost of Materials |  | $\mathbf{4 2 8 2 5 9 0 . 6 7 5}$ |

### 3.48 Abstract of cost details for Rock bolt support in Tailrace tunnel by Drill \& Blast method

| For Good and fair Rock |  |
| :--- | :---: |
| A. Cost of Materials | 4948317.694 |
| B. Hire charges of Machinery | 4073.28 |
| C. Cost of Labour | 4371.02 |
| TOTAL | $\mathbf{4 9 5 6 7 6 1 . 9 9 4}$ |
| Add for Air and Water line @ $0.80 \%$ | 39654.095 |
| Add for Lighting $\quad$ @ $1.80 \%$ | 89221.715 |
| Add for Ele sub-station / Demand charges @ 3.80\% | 188356.955 |
| Add for other enabling works @ 1.70\% | 84264.953 |
| TOTAL | $\mathbf{5 3 5 8 2 5 9 . 7 1 2}$ |
| Add for 1 km rehandling lead charges |  |
| For steel 150 kg $@ 218.40$ per tonne $(0.15 \times 218.40)$ | 32.76 |
| Total cost for 19280 Rm | $\mathbf{5 3 5 8 2 9 2 . 4 7 2}$ |


| For Poor and V. Poor Rock |  |
| :---: | :---: |
| A. Cost of Materials | 4282590.675 |
| B. Hire charges of Machinery | 4073.28 |
| C. Cost of Labour | 4371.02 |
| TOTAL | 4291034.975 |
| Add for Air and Water line @ $0.80 \%$ | 34328.279 |
| Add for Lighting @ 1.80\% | 77238.629 |
| Add for Eletrical sub-station / Demand charges @ 3.80\% | 163059.329 |
| Add for other enabling works @ 1.70\% | 72947.594 |
| TOTAL | 4638608.806 |
| Add for 1 km rehandling lead charges |  |
| For steel 150 kg @ 218.40 per tonne ( $0.15 \times 218.40$ ) | 32.76 |
| Total cost for 8370 Rm | 4638641.566 |

Total cost for Rock bolt support work in (Good \& Fair Rock + Poor \& Very Poor Rock):
Total cost for Rock bolt support work (5358292.472+4638641.566) : 9996934.038

### 3.49 Cost calculation for kerb \& invert lining in Tailrace tunnel by Drill \& Blast method

$$
\text { Rate per } \boldsymbol{m}^{3} \quad: \mathbf{6 3 2 6 . 0 0}
$$

Total cost for Kerb and Invert Lining $(1.9+1.9+2.2)=6.0 \mathrm{~m}^{2} \times 1927 \mathrm{~m} \times 6326=$ 73141212.0

### 3.50 Cost estimation for Overt lining in Tailrace tunnel by Drill \& Blast method

| Assume $\mathbf{1 5} \mathbf{m}$ long collapsible type steel gantry |  |  |  |
| :--- | :--- | :--- | :---: | :---: |
| Quantity of concrete per gantry considering <br> $\operatorname{lining}\left(12.22 \mathbf{m}^{2} \times 15 \mathrm{~m}\right)$ | $1.0 \mathrm{~m} \quad$ thick | $183.3 \boldsymbol{m}^{\mathbf{3}}$ |  |
| Concrete for filling support reaches | @ $45 \%$ |  |  |
| Average quantity of concrete per gantry length of lining say | $\mathbf{1 8 3 . 3} \mathbf{m}^{\mathbf{3}}$ |  |  |


| Requirement of materials |  |  |
| :--- | :--- | :---: |
| Cement for mix with 1 \% wastage | $(183.3 \times 300 \times 1.01)$ | 55539.9 kg |
| Cement for incidentals @ 1 kg per $\mathrm{m}^{3}$ | $(183.3 \times 1)$ | 183.3 kg |
| Coarse aggregate $40-20 \mathrm{~mm}$ size range | $(183.3 \times 0.79 \times 0.5 \times 1.02)$ | $73.851 \mathrm{~m}^{3}$ |
| Coarse aggregate $20-10 \mathrm{~mm}$ size range | $(183.3 \times 0.79 \times 0.3 \times 1.02)$ | $44.310 \mathrm{~m}^{3}$ |
| Coarse aggregate $10-4.75 \mathrm{~mm}$ size | $(183.3 \times 0.79 \times 0.2 \times 1.02)$ | $29.540 \mathrm{~m}^{3}$ |
| Fine aggregate | $(183.3 \times 0.425 \times 1.02)$ | $79.460 \mathrm{~m}^{3}$ |
| Super plasticiser | $(183.3 \times 0.90 \times 1.02)$ | 168.269 litres |

## RATE ANALYSIS UNIT : $\mathbf{1 8 3 . 3} \mathrm{m}^{\mathbf{3}}$

## A.MATERIALS

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Cement 43 Grade | kg | 55540 | 7.5 | 416549.25 |
|  | Cement for incidentals @ 1 kg per cum | kg | 183.3 | 7.5 | 1374.75 |
| 2 | Fine aggregate ( screened ) | cum | 79.46 | 730 | 58005.8 |
| 3 | Coarse aggregate $40-20 \mathrm{~mm}$ | cum | 73.851 | 740 | 54649.74 |
|  | Coarse aggregate $20-10 \mathrm{~mm}$ | cum | 44.31 | 950 | 42094.5 |
|  | Coarse aggregate $10-4.75 \mathrm{~mm}$ | cum | 29.54 | 1160 | 34266.4 |
| 4 | Super plasticiser | litre | 168.27 | 105 | 17668.245 |
| 5 | Use rate of end shuttering | sqm | 6 | 158.77 | 952.6 |
| 6 | Use rate of steel gantry | sqm | 100 | 176.95 | 17695.03 |
| 7 | Sundries (placer pipe etc ) | LS | 5 | 44 | 220 |
|  |  |  |  | Total | 643476.315 |


| Add for small Tools and Plants | $@ 1 \%$ | 6434.763 |
| :--- | :--- | :---: |
| Add for Contractor's Profit on Energy | $@ 10 \%$ | 64347.631 |
| Add for Contractor's Overheads | $@ 5 \%$ | 32173.838 |
| Total cost of Materials |  | $\mathbf{7 4 6 4 3 2 . 5 4 7}$ |

### 3.51 Abstract of cost details for Overt lining in Tailrace tunnel by Drill \& Blast method

A. Cost of Materials
746432.547

| B. Hire charges of Machinery | 70930.40 |  |
| :--- | :--- | :--- |
| C. Cost of Labour | 31125.79 |  |
| TOTAL | $\mathbf{8 4 8 4 8 8 . 7 3 7}$ |  |
| Add for Air and Water line @ $0.80 \%$ | 6787.909 |  |
| Add for Lighting | @ 1.80 | 15272.797 |
| Add for Electrical sub-station charges @ $3.80 \%$ | 32242.572 |  |
| Add for other enabling works © $1.70 \%$ | 14424.308 |  |
| Total cost for $\mathbf{1 8 3 . 3} \mathbf{m}^{\mathbf{3}}$ | $\mathbf{9 1 7 2 1 6 . 3 2 3}$ |  |
| Cost for per $\boldsymbol{m}^{\mathbf{3}}$ | $\mathbf{5 0 0 3 . 9 0 7}$ |  |

Total cost for Overt Lining $\left(12.22 \mathrm{~m}^{2}\right) \times(1927 \mathrm{~m}) \times(5003.907) \quad: 117831701.8$
Total cost in Tailrace Tunnel (Excavation + Rock bolt support + Kerb \& Invert Lining + Overt Lining):
( $90 \%$ without rib support $+10 \%$ with rib support + Good \& Fair rock + Poor \& Very Poor rock + Kerb \& Invert lining + Overt lining) :
$(176074716.9+12809021.41+5358292.472+4638641.566+73141212+117831701.8)=$ 389853586.1

## EXCAVATION BY MECHANICAL METHOD

### 3.52 Cycle Time calculation for different activities for heading work in Diversion tunnel by Mechanical method <br> $1{ }^{\text {st }}$.Activity: Survey - 0.5 hours

$2^{\text {nd }}$. Activity: Time required for Excavation work $=\frac{\text { Excavated Quantity }}{\text { productivity of Roadheader }}$
Excavated quantity $=\mathrm{c} / \mathrm{s}$ area of tunnel $\times$ length of drill $=\left(\frac{\pi \times d^{2}}{4}\right) \times$ length of drill
$=\frac{\pi \times 8.0225^{2}}{4} \times 3=151.6458 \boldsymbol{m}^{3}$
$=$ Excavated quantity $=151.6458 \times 1.2(20 \%$ as over-break quantity $)$
$=182.0 m^{3}$ (Excavated quantity will be more because there wil be some voids in the quantity)

Time required for Excavated quantity $=\frac{\text { Excavated quantity }}{\text { Productivity of Roadheader }}=\frac{182 \mathrm{~m}^{3}}{15 m^{3} \text { per hour }}=12.0$ Hour
$3^{\text {rd }}$ Activity: Mucking time $=\frac{\text { Mucking quantity }}{\text { Productivity of Loader }}=\frac{182 \mathrm{~m}^{3}}{65 \mathrm{~m}^{3} \text { per hou }}=3.0$ hour
$4^{\text {th }}$ Activity: Scaling time -1.0 hours
$4^{\text {th }} \cdot$ Activity: Time required for shotcreting $=$

1. For Good Rock Shotcreting $(5 \mathrm{~cm})=0.5$ hour
2.For Fair Rock Shotcreting $(10 \mathrm{~cm})=1.0$ hour
3.For Poor Rock Shotcreting $(15 \mathrm{~cm})=2.0$ hour
4.For Very Poor Rock Shotcreting $(20 \mathrm{~cm})=2.5$ hour
$5^{\text {th }}$. Activity: Rock bolt drilling \& fixing:
For Good \& Fair Rock: Total rock bolt drilling fixing time $=(1+1)$ hour $=2.0$ hour
For Poor \& Very Poor Rock: Total rock bolt drilling fixing time $=(1.5+1.5)$ hour $=3.0$ hour

### 3.53 Cycle time for Heading in Diversion Tunnel

3 m pull length per cycle to be considered for heading without rib and 1.5 m pull length to be considered for heading with rib.

### 3.53.1. Cycle time for heading without rib support in Diversion tunnel

Table 3.49 Cycle time for heading without rib support in DT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 3 | m |
| 2 | Heading c/s area | 82.67 | sum |
| 3 | Excavation quantity | 248.01 | cum |
| 4 | Survey | 0.5 | Hour |
| 5 | Excavation time | 12 | Hour |
| 6 | Mucking | 3 | Hour |
| 7 | Scaling | 1 | Hour |
| 8 | shotcreting | 1 | Hour |
| 9 | Rockbolt drilling \& fixing | 2 | Hour |
|  | Total cycle time for 3m pull length | 19.5 | Hour |

### 3.53.2 Cycle time for heading with rib support in Diversion tunnel

Excavation with rib supporting is considered as $10 \%$ of total excavation in Diversion tunnel

Table 3.50 Cycle time for heading with rib support in DT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull Length | 1.5 | m |
| 2 | Heading c/s area | 82.67 | sqm |
| 3 | Excavation quantity | 124.005 | cum |
| 4 | Survey | 0.5 | Hour |
| 5 | Excavation time | 12 | Hour |
| 6 | Mucking | 3 | Hour |
| 7 | Scaling | 1 | Hour |
| 8 | Shotcreting | 2.5 | Hour |
| 9 | Rockbolt drilling \& fixing | 3 | Hour |
| 10 | Rib erection | 3 | Hour |
| 11 | Lagging fixing | 2.5 | Hour |
| 12 | Stopper fixing\&Back fill concrete | 4 | Hour |
|  | Total cycle time per 1.5m pull length | 31.5 | Hour |
|  | Total cycle time per 3m pull length | 63 | Hour |

## Time Schedule:

Among the total excavation $90 \%$ is considered as without rib supporting and $10 \%$ as with rib supporting.

Weighted average cycle time $=(19.5 \times 0.9)+(63 \times 0.1)=24$ hours per 3 m pull length

Progress per month $=\frac{26(\text { working day per month }) \times 22(\text { working hours per day }) \times 3 \mathrm{~m}(\text { pull length })}{24(\text { weighted cycle time in hours })}$
$=71.5 \mathrm{~m}$ per month

Time required for completion of heading work $=\frac{\text { Length of Diversion tunnel-1 }}{\text { Work progress per month }}$
$=\frac{472}{71.5 \mathrm{~m} \text { per month }}=6.60$ month $=198$ days
Time required for completion of heading work $=\frac{\text { Length of Diversion tunnel-2 }}{\text { Work progress per month }}$
$=\frac{552}{71.5 \mathrm{~m} \text { per month }}=7.72 \mathrm{month}=231$ days

### 3.54 Cycle time calculation for Benching in Diversion tunnel by Mechanical method

$1^{\text {st }}$. Activity: Surveying time -0.5 hours
$2^{\text {nd }}$. Activity: Excavation time $=\frac{\text { Excavation quantity }}{\text { productivity of Roadheader }}$

Excavated quantity $=\mathrm{C} / \mathrm{S}$ area of tunnel $\times$ length of drill
$=\left(\frac{\pi \times d^{2}}{4}\right) \times$ drill length $=\left(\frac{\pi \times 4.3225^{2}}{4}\right) \times 3 \mathrm{~m}=41.4690 \mathrm{~m}^{3}$

Excavated quantity $=41.4690 \times 1.2(20 \%$ as over-break quantity $)$
$=52.8277 m^{3}$ (Excavated quantity will be more because there will be some voids in the quantity)

Time required for Excavation quantity $=\frac{\text { Excavation quantity }}{\text { Productivity of Roadheader }}=\frac{52.8277 \mathrm{~m}^{3}}{15 \mathrm{~m}^{3} / \mathrm{hour}}=3.5$ hour $3^{\text {rd }}$. Activity Time required for Mucking quantity $=\frac{\text { Mucking quantity }}{\text { Productivity of Loader }}=\frac{52.8277 \mathrm{~m}^{3}}{65 \mathrm{3} / \mathrm{hour}}=1.0$ hour
$4^{\text {th }}$. Activity: Scaling time $=0.5$ hour
$5^{\text {th }}$.Activity: Time required for shotcreting $=$

1. For Good Rock Shotcreting $(5 \mathrm{~cm})=0.5$ hour
2.For Fair Rock Shotcreting $(10 \mathrm{~cm})=0.5$ hour
3.For Poor Rock Shotcreting $(15 \mathrm{~cm})=1.0$ hour
4.For Very Poor Rock Shotcreting $(20 \mathrm{~cm})=1.5$ hour
3.54.1 Cycle time for benching without rib support in Diversion tunnel

Table 3.51 Cycle time for benching without rib in DT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 3 | m |
| 2 | Benching c/s area | 40.23 | sqm |
| 3 | Excavation quantity | 120.69 | cum |
| 4 | Survey | 0.5 | Hour |
| 5 | Excavation time | 3.5 | Hour |
| 6 | Mucking | 1 | Hour |
| 7 | Scaling | 0.5 | Hour |
| 8 | shotcreting | 0.5 | Hour |
|  | Total cycle time for 3m pull length | 6 | Hour |

### 3.54.2 Cycle time for benching with rib support in Diversion tunnel

Table 3.52 Cycle time for benching with rib in DT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 1.5 | m |
| 2 | Benching c/s area | 40.23 | sqm |
| 3 | Excavation quantity | 60.345 | cum |
| 4 | Survey | 0.5 | Hour |
| 5 | Excavation time | 3.5 | Hour |
| 6 | Mucking | 1 | Hour |
| 7 | Scaling | 0.5 | Hour |
| 8 | Shotcreting | 1.5 | Hour |
| 9 | Rib erection | 2 | Hour |
| 10 | Lagging fixing | 1 | Hour |
| 11 | Backfill concreting | 1 | Hour |
|  | Total cycle time for 1.5 m pull length | 11 | Hour |
|  | Total cycle time for 3m pull length | 22 | Hour |

## Time Schedule:

Weighted average cycle time $=(6 \times 0.9)+(22 \times 0.1)=7.6$ hours per 3 m pull

Progress per month $=\frac{(26(\text { working day per month }) \times 22(\text { working hours per day }) \times 3 \mathrm{~m} \text { pull length })}{7.6(\text { weighted average cycle time in hours })}$
$=226 \mathrm{~m}$ per month

Time required for Completion of benching work $=\frac{\text { Tunnel length }-1}{\text { progress per month }}$
$=\frac{472}{226}=2.0$ month $=60$ days
Time required for Completion of benching work $=\frac{\text { Tunnel length }-2}{\text { progress per month }}$
$=\frac{552}{226}=2.44$ month $=72$ days
Table 3.53 Time duration for different rock conditions in Diversion tunnel- 1

| DT - 1 | Source | Good <br> Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | Inlet | 15 | 59 | 15 | 10 | 99 |
| Heading | Outlet | 15 | 59 | 15 | 10 | 99 |
| Benching | Inlet | 4 | 19 | 4 | 4 | 31 |


| Benching | Outlet | 4 | 19 | 4 | 4 | 31 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Kerb | Inlet | 3 | 13 | 3 | 2 | 21 |
| Kerb | Outlet | 3 | 13 | 3 | 2 | 21 |
| Overt | Inlet | 3 | 13 | 3 | 3 | 22 |
| Overt | Outlet | 3 | 13 | 3 | 3 | 22 |
| Invert | Inlet | 15 | 19 | 15 | 3 | 52 |
| Invert | Outlet | 15 | 19 | 15 | 3 | 52 |

Table 3.54 Time duration for different rock conditions in Diversion tunnel- 2

| DT - 2 | Source | Good <br> Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | Inlet | 17 | 69 | 17 | 11 | 114 |
| Heading | Outlet | 17 | 69 | 17 | 11 | 114 |
| Benching | Inlet | 5 | 22 | 5 | 3 | 35 |
| Benching | Outlet | 5 | 22 | 5 | 3 | 35 |
| Kerb | Inlet | 4 | 15 | 4 | 2 | 25 |
| Kerb | Outlet | 4 | 15 | 4 | 2 | 25 |
| Overt | Inlet | 4 | 15 | 4 | 2 | 25 |
| Overt | Outlet | 4 | 15 | 4 | 2 | 25 |
| Invert | Inlet | 5 | 23 | 5 | 4 | 37 |
| Invert | Outlet | 5 | 23 | 5 | 4 | 37 |

Table 3.55 Activities details of DT in case of Roadheader

| RHP - ROAD HEADER(50-50) |  | Classic WBS Layout |  |  |  | 28-Apr-17 18:48 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Activity ID | Activity Name | $\begin{array}{\|l\|} \hline \text { Original } \\ \text { Duration } \end{array}$ | Remaining Duration | Schedule \% Complete | Start | Finish | $\begin{aligned} & \text { Total } \\ & \text { Float } \end{aligned}$ |  |
| RHP - R | OAD HEADER(5) | 249 | 249 | 0\% | 15-May-17 | 14-Dec-17 | 0 |  |
| mobilis | ation | 30 | 30 | 0\% | 15-May-17 | 08-Jun-17 | 0 |  |
| A1290 | mobilisation | 30 | 30 | 0\% | 15-May-17 | 08-Jun-17 | 0 |  |
| DT por |  | 55 | 55 | 0\% | 08-Jun-17 | 26-Jul-17 | 0 |  |
| A1270 | dt portal inlet | 55 | 55 | 0\% | 08-Jun-17 | 26-Jul-17 | 0 |  |
| A1280 | dt portal outlet | 28 | 28 | 0\% | 08-Jun-17 | 03-Jul-17 | 0 |  |
| DIVER | SION TUNNEL 1 | 193 | 193 | 0\% | 21-Jun-17 | 05-Dec-17 | 11 |  |
| A1030 | Heading Inlet | 99 | 99 | 0\% | 21-Jun-17 | 14-Sep-17 | 11 |  |
| A1080 | Heading outlet | 99 | 99 | 0\% | 21-Jun-17 | 14-Sep-17 | 11 |  |
| A1040 | Benching Inlet | 31 | 31 | 0\% | 14-Sep-17 | 11-Oct-17 | 11 |  |
| A1090 | Benching outlet | 31 | 31 | 0\% | 14-Sep-17 | 11-Oct-17 | 11 |  |
| A1060 | Kerb inlet | 22 | 22 | 0\% | 02-Oct-17 | 20-Oct-17 | 11 |  |
| A1110 | kerb outlet | 22 | 22 | 0\% | 02-Oct-17 | 20-Oct-17 | 11 |  |
| A1070 | Overt inlet | 52 | 52 | 0\% | 20-Oct-17 | 05-Dec-17 | 11 |  |
| A1120 | overt outlet | 52 | 52 | 0\% | 20-Oct-17 | 05-Dec-17 | 11 |  |
| A1050 | Invert Inlet | 21 | 21 | 0\% | 07-Nov-17 | 24-Nov-17 | 22 |  |
| A1100 | Invert Outlet | 21 | 21 | 0\% | 07-Nov-17 | 24-Nov-17 | 22 |  |
| DIVERS | SION TUNNEL 2 | 204 | 204 | 0\% | 21-Jun-17 | 14-Dec-17 | 0 |  |
| A1170 | Heading Inlet | 114 | 114 | 0\% | 21-Jun-17 | 27-Sep-17 | 0 |  |
| A1220 | Heading outlet | 114 | 114 | 0\% | 21-Jun-17 | 27-Sep-17 | 0 |  |
| A1180 | Benching Inlet | 35 | 35 | 0\% | 27-Sep-17 | 27-Oct-17 | 0 |  |
| A1230 | Benching outlet | 35 | 35 | 0\% | 27-Sep-17 | 27-Oct-17 | 0 |  |
| A1200 | Kerb inlet | 25 | 25 | 0\% | 16-Oct-17 | 06-Nov-17 | 0 |  |
| A1250 | kerb outlet | 25 | 25 | 0\% | 16-Oct-17 | 06-Nov-17 | 0 |  |
| A1210 | Overt inlet | 37 | 37 | 0\% | 06-Nov-17 | 07-Dec-17 | 0 |  |
| A1260 | overt outlet | 37 | 37 | 0\% | 06-Nov-17 | 07-Dec-17 | 0 |  |
| A1190 | Invert Inlet | 25 | 25 | 0\% | 22-Nov-17 | 14-Dec-17 | 0 |  |
| A1240 | Invert Outlet | 25 | 25 | 0\% | 22-Nov-17 | 14-Dec-17 | 0 |  |



Fig 3.11 Network diagram of Diversion tunnel in case of Roadheader
3.55 Cycle time calculation for different activities for heading work in Pressure shaft by Mechanical method
$1^{\text {st }}$ Activity: Survey -0.5 hours
$2^{\text {nd }}$. Activity: Time required for Excavation work $=\frac{\text { Excavation Quantity }}{\text { productivity of Roadheader }}$
Excavated quantity $=\frac{\mathrm{C} / \mathrm{s} \text { area of tunnel }}{\text { length of drill }}=\left(\frac{\pi \times d^{2}}{4}\right) \times$ length of drill
$=\frac{\pi \times 5.2725^{2}}{4} \times 3=65.5004 \mathrm{~m}^{3}$
$=$ Excavated quantity $=65.5004 \times 1.2(20 \%$ as over-break quantity $)$
$=78.6005 m^{3}$ (Excavated quantity will be more because there wil be some voids in the quantity)

Time required for Excavated quantity $=\frac{\text { Excavated quantity }}{\text { Productivity of Roadheader }}=\frac{78.6005 \mathrm{~m}^{3}}{15{ }^{3}}$ per hour $=$ 5.0 hour
$3^{\text {rd }}$. Activity Time required for Mucking quantity $=\frac{\text { Mucking quantity }}{\text { Productivity of Loader }}=\frac{78.6005 \mathrm{~m}^{3}}{65 \mathrm{~m}^{3}}$ per hour $=1.5$ hour
$4^{\text {th }}$. Activity: Scaling time -0.5 hours
$5^{\text {th }}$. Activity: Time required for shotcreting $=$

1. For Good Rock Shotcreting $(5 \mathrm{~cm})=0.5$ hour
2. For Fair Rock Shotcreting $(10 \mathrm{~cm})=1.0$ hour
3. For Poor Rock Shotcreting $(15 \mathrm{~cm})=1.5$ hour
4. For Very Poor Rock Shotcreting $(20 \mathrm{~cm})=2.0$ hour
$5^{\text {th }}$. Activity: Rock bolt drilling \& fixing:
For Good \& Fair Rock $=1.5$ hour
For Poor \& V. Poor Rock $=1.5$ hour

### 3.56 Cycle time for Heading

3 m pull length per cycle to be considered for heading without rib and 1.5 m pull length to be considered for heading with rib

### 3.56.1 Cycle time for heading without rib support in Pressure shaft

Table 3.56 Cycle time for heading without rib in PS

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Pull length | 3 | m |
| 2 | Heading c/s area | 34.0369 | sqm |
| 3 | Excavation quantity | 102.11 | cum |
| 4 | Survey | 0.5 | Hour |
| 5 | Excavation time | 5 | Hour |
| 6 | Mucking | 1.5 | Hour |
| 7 | Scaling | 0.5 | Hour |
| 8 | shotcreting | 1 | Hour |
| 9 | Rockbolt drilling \& fixing | 1.5 | Hour |
|  | Total cycle time for 3m pull length | 10 | Hour |

3.56.2 Cycle time for heading with rib support in Pressure shaft
Table 3.57 Cycle time for heading with rib in PS

Table 3.57 Cycle time for heading with rib in PS

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull Length | 1.5 | m |
| 2 | Heading c/s area | 34.0369 | sqm |
| 3 | Excavation quantity | 51.055 | cum |
| 4 | Survey | 0.5 | Hour |
| 5 | Excavation time | 5 | Hour |
| 6 | Mucking | 1.5 | Hour |
| 7 | Scaling | 0.5 | Hour |
| 8 | Shotcreting | 2 | Hour |
| 9 | Rockbolt drilling \& fixing | 1.5 | Hour |
| 10 | Rib erection | 2 | Hour |
| 11 | Lagging fixing | 2.5 | Hour |
| 12 | Stopper fixing\&Back fill concrete | 2.5 | Hour |
|  | Total cycle time per 1.5m pull length | 18 | Hour |
|  | Total cycle time per 3m pull length | 36 | Hour |

## Time Schedule:

Among the total excavation $90 \%$ is considered as without rib supporting and $10 \%$ as with rib supporting.

Weighted average cycle time $=(10 \times 0.9)+(36 \times 0.1)=12.6$ hours per 3 m pull length
Progress per month $=\frac{26(\text { working day per month }) \times 22(\text { working hours per day }) \times 3 \mathrm{~m}(\text { pull length })}{12.6(\text { weighted cycle time in hours })}$
$=136 \mathrm{~m}$ per month

Time required for completion of heading work $=\frac{\text { Length of Pressure Shaft }}{\text { Work progress per month }}$
$=\frac{211+197+184+172=764 \mathrm{~m}}{136 \mathrm{~m} \text { per month }}=5.61$ month $=168$ days

### 3.57 Cycle time calculation for Benching in Pressure shaft

$1^{\text {st }}$. Activity: Surveying time -0.5 hours
$2^{\text {nd }}$. Activity: Excavation time $=\frac{\text { Excavated quantity }}{\text { productivity of Roadheader }}$

Excavated quantity $=$ Cross-sectional area of tunnel $\times$ length of drill
$=\left(\frac{\pi \times d^{2}}{4}\right) \times$ drill length $=\left(\frac{\pi \times 2.3725^{2}}{4}\right) \times 3 \mathrm{~m}=13.2624 \mathrm{~m}^{3}$

Excavated quantity $=13.2624 \times 1.2(20 \%$ as over-break quantity $)$
$=15.9149 \mathrm{~m}^{3}$ (Excavated quantity will be more than because there will be some voids in the quantity)

Time required for Excavated quantity $=\frac{\text { Excavated quantity }}{\text { Productivity of Roadheader }}=\frac{15.9149 \mathrm{~m}^{3}}{15 \mathrm{~m}^{3}}$ per hour $=$ 1.0 hour

Time required for Mucking quantity $=\frac{\text { Mucking quantity }}{\text { Productivity of Loader }}=\frac{15.9149 \mathrm{~m}^{3}}{65 \mathrm{~m}^{3}}$ per hour $=0.5$ hour
$3^{\text {rd }}$. Activity: Scaling time $=0.5$ hour
$4^{\text {th }}$.Activity: Time required for shotcreting $=$
1.For Good Rock Shotcreting $(5 \mathrm{~cm})=0.5$ hours
2.For Fair Rock Shotcreting $(10 \mathrm{~cm})=0.5$ hours
3.For Poor Rock Shotcreting $(15 \mathrm{~cm})=0.5$ hour
4.For Very Poor Rock Shotcreting $(20 \mathrm{~cm})=1.0$ hours

### 3.57.1 Cycle time for benching without rib support in Pressure shaft Table 3.58 Cycle time for benching without rib in PS

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 3 | m |
| 2 | Benching c/s area | 13.8665 | sqm |
| 3 | Excavation quantity | 41.599 | cum |
| 4 | Survey | 0.5 | Hour |
| 5 | Excavation time | 1 | Hour |
|  | Mucking | 0.5 | Hour |
| 6 | Scaling | 0.5 | Hour |
| 7 | shotcreting | 0.5 | Hour |
|  | Total cycle time for 3m pull length | 3 | Hour |

### 3.57.2 Cycle time for benching with rib support in Pressure shaft

Table 3.59 Cycle time for benching with rib in PS

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 1.5 | m |
| 2 | Benching c/s area | 13.8665 | sqm |
| 3 | Excavation quantity | 20.799 | cum |
| 4 | Survey | 0.5 | Hour |
| 5 | Excavation time | 1 | Hour |
| 6 | Mucking | 0.5 | Hour |
| 7 | Scaling | 0.5 | Hour |
| 8 | Shotcreting in | 1 | Hour |
| 9 | Rib erection | 2 | Hour |
| 10 | Lagging fixing | 2.5 | Hour |
| 11 | Backfill concreting | 2 | Hour |
|  | Total cycle time for 1.5m pull length | 10 | Hour |
|  | Total cycle time for 3m pull length | 20 | Hour |

## Time Schedule:

Weighted average cycle time $=(3 \times 0.9)+(20 \times 0.1)=4.7$ hours per 3 m pull
Progress per month $=\frac{(26(\text { working day per month }) \times 22(\text { working hours per day }) \times 3 \mathrm{~m} \text { pull length })}{4.7(\text { weighted average cycle time in hours })}$ $=365 \mathrm{~m}$ per month

Time required for Completion of benching work $=\frac{\text { length of Pressure Shaft }}{\text { progress per month }}$
$=\frac{211+197+184+172=764 \mathrm{~m}}{365}=2.0$ month $=60$ days

Table 3.60 Activities duration for different rock conditions in PS - 1

| Pressure <br> Shaft - 1 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 7 | 28 | 7 | 4 | 46 |
| Benching | 2 | 10 | 2 | 2 | 16 |
| Kerb | 8 | 11 | 8 | 2 | 29 |
| Overt | 8 | 11 | 8 | 2 | 29 |
| Invert | 8 | 16 | 8 | 3 | 35 |

Table 3.61 Activities duration for different rock conditions in PS - 2

| Pressure <br> Shaft - 2 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 6 | 26 | 6 | 4 | 42 |
| Benching | 2 | 10 | 2 | 2 | 16 |
| Kerb | 2 | 11 | 2 | 1 | 16 |
| Overt | 2 | 11 | 2 | 1 | 16 |
| Invert | 4 | 15 | 4 | 2 | 25 |

Table 3.62 Activities duration for different rock conditions in PS - 3

| Pressure <br> Shaft $-\mathbf{3}$ | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 6 | 24 | 6 | 4 | 40 |
| Benching | 2 | 9 | 2 | 2 | 15 |
| Kerb | 2 | 10 | 2 | 1 | 15 |
| Overt | 2 | 10 | 2 | 1 | 15 |
| Invert | 4 | 14 | 4 | 2 | 24 |

Table 3.63 Activities duration for different rock conditions in PS - 4

| Pressure <br> Shaft $-\mathbf{4}$ | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 5 | 23 | 5 | 3 | 36 |
| Benching | 2 | 8 | 2 | 1 | 13 |
| Kerb | 2 | 9 | 2 | 1 | 14 |
| Overt | 2 | 9 | 2 | 1 | 14 |
| Invert | 3 | 13 | 3 | 2 | 21 |

Table 3.64 Activities duration of PS in case of Roadheader



Fig 3.12 Network diagram of Pressure shaft in case of Roadheader
3.58 Cycle time calculation for different activities for heading work in Tailrace tunnel by Mechanical method
$1^{\text {st }}$ Activity: Survey - 0.5 hours
$2^{\text {nd }}$. Activity: Time required for Excavation work $=\frac{\text { Excavated Quantity }}{\text { productivity of Roadheader }}$

Excavated quantity $=\frac{\mathrm{C} / \mathrm{S} \text { area of tunnel }}{\text { length of drill }}=\left(\frac{\pi \times d^{2}}{4}\right) \times$ length of drill
$=\frac{\pi \times 6.4725^{2}}{4} \times 3=98.7086 \boldsymbol{m}^{3}$
$=$ Excavated quantity $=98.7086 \times 1.2(20 \%$ as over-break quantity $)$
$=118.4503 \mathrm{~m}^{3}$ (Excavated quantity will be more than because there will be some voids in the quantity)

Time required for Excavated quantity $=\frac{\text { Excavated quantity }}{\text { Productivity of roadheader }}=\frac{118.4503 \mathrm{~m}^{3}}{15 \mathrm{3}}$ per hour $=$ 8.0 hour
$3^{\text {rd }}$. Activity Time required for Mucking quantity $=\frac{\text { Mucking quantity }}{\text { Productivity of Loader }}=\frac{118.4503 \mathrm{~m}^{3}}{653}$ per hour $=2.0$ hour
$4^{\text {th }}$. Activity: Scaling time -0.5 hours
$5^{\text {th }}$. Activity: Time required for shotcreting $=$

1. For Good Rock Shotcreting $(5 \mathrm{~cm})=0.5$ hour
2.For Fair Rock Shotcreting $(10 \mathrm{~cm})=1.0$ hour
2. For Poor Rock Shotcreting $(15 \mathrm{~cm})=1.5$ hour
4.For V. Poor Rock Shotcreting $(20 \mathrm{~cm})=2.0$ hour
$5^{\text {th }}$. Activity: Rock bolt drilling $\&$ fixing:
For Good \& Fair Rock = 1.5 hour
For Poor \& V.Poor Rock $=2.0$ hour

### 3.59 Cycle time for Heading in Tailrace tunnel

3 m pull length per cycle to be considered for heading without rib and 1.5 m pull length to be considered for heading with rib

### 3.59.1 Cycle time for heading without rib support in Tailrace tunnel Table 3.65 Cycle time for heading without rib in TRT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 3 | m |
| 2 | Heading c/s area | 52.44 | sqm |
| 3 | Excavation quantity | 157.32 | cum |
| 4 | Survey | 0.5 | Hour |
| 5 | Excavation time | 8 | Hour |
|  | Mucking | 2 | Hour |
| 6 | Scaling | 0.5 | Hour |
| 8 | shotcreting | 1 | Hour |
| 9 | Rockbolt drilling \& fixing | 1.5 | Hour |
|  | Total cycle time for 3m pull length | 13.5 | Hour |

3.59.2 Cycle time for heading with rib support in Tailrace tunnel

Table 3.66 Cycle time for heading with rib in TRT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull Length | 1.5 | m |
| 2 | Heading c/s area | 52.44 | sqm |
| 3 | Excavation quantity | 78.66 | cum |
| 4 | Survey | 0.5 | Hour |
| 5 | Excavation time | 8 | Hour |
| 6 | Mucking | 2 | Hour |
| 7 | Scaling | 0.5 | Hour |
| 8 | Shotcreting | 2 | Hour |
| 9 | Rockbolt drilling \& fixing | 2 | Hour |
| 10 | Rib erection | 2.5 | Hour |
| 11 | Lagging fixing | 2 | Hour |
| 12 | Stopper fixing\&Back fill concrete | 3 | Hour |
|  | Total cycle time per 1.5m pull length | 22.5 | Hour |
|  | Total cycle time per 3m pull length | 45 | Hour |

## Time Schedule:

Among the total excavation $90 \%$ is considered as without rib supporting and $10 \%$ as with rib supporting

Weighted average cycle time $=(13.5 \times 0.9)+(45 \times 0.1)=16.65$ hours per 3 m pull length
Progress per month $=\frac{(26(\text { working day per month }) \times 22(\text { working hours per day }) \times 3 \mathrm{~m} \text { pull length })}{16.65(\text { weighted cycle time in hours })}$
$=103 \mathrm{~m}$ per month
Time required for completion of Heading work $=\frac{\text { Lengt of Tail Race Tunnel }}{\text { Work progress per month }}$
$=\frac{(502+490+475+460=1927) \mathrm{m}}{(103 \mathrm{~m} \text { per month })}=18.70$ month $=561$ days

### 3.60 Cycle time calculation for Benching in Tailrace tunnel by Mechanical method

$1^{\text {st }}$. Activity: Surveying time -0.5 hours
$2^{\text {nd }}$. Activity: Excavation time $=\frac{\text { Excavated quantity }}{\text { productivity of Roadheader }}$

Excavated quantity $=\mathrm{C} / \mathrm{S}$ area of tunnel $\times$ length of drill
$=\left(\frac{\pi \times d^{2}}{4}\right) \times$ drill length $=\left(\frac{\pi \times 3.1735^{2}}{4}\right) \times 3 \mathrm{~m}=23.7294 \mathrm{~m}^{3}$
Excavated quantity $=23.7294 \times 1.2(20 \%$ as over-break quantity $)$
$=28.4753 \mathrm{~m}^{3}$ (Excavated quantity will be more because there will be some voids in the quantity)

Time required for Excavated quantity $=\frac{\text { Excavated quantity }}{\text { Productivity of Roadheader }}=\frac{28.4753 \mathrm{~m}^{3}}{15 \mathrm{~m}^{3}}$ per hour $=$ 2.0 hour
$3^{\text {rd }}$. Activity Time required for Mucking quantity $=\frac{\text { Mucking quantity }}{\text { Productivity of Loader }}=\frac{28.4753 \mathrm{~m}^{3}}{65 \mathrm{~m}^{3}}$ per hour $=0.5$ hour
$4^{\text {th }}$. Activity: Scaling time $=0.5$ hour
$4^{\text {th }} \cdot$ Activity: Time required for shotcreting $=$
1.For Good Rock Shotcreting $(5 \mathrm{~cm})=0.5$ hours
2.For Fair Rock Shotcreting $(10 \mathrm{~cm})=0.5$ hours
3.For Poor Rock Shotcreting $(15 \mathrm{~cm})=1.0$ hour

### 3.60.1 Cycle time for benching without rib support in Tailrace tunnel Table 3.67 Cycle time for benching without rib in TRT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 3 | m |
| 2 | Benching c/s area | 23.21 | sqm |
| 3 | Excavation quantity | 69.63 | cum |
| 4 | Survey | 0.5 | Hour |
| 5 | Excavation time | 2 | Hour |
|  | Mucking | 0.5 | Hour |
| 6 | Scaling | 0.5 | Hour |
| 8 | shotcreting | 0.5 | Hour |
|  | Total cycle time for 3m pull length | 4 | Hour |

### 3.60.2 Cycle time for benching with rib support in Tailrace tunnel <br> Table 3.68 Cycle time for benching with rib in TRT

| S.N | Description | Quantity | Units |
| :---: | :---: | :---: | :---: |
| 1 | Pull length | 1.5 | m |
| 2 | Benching c/s area | 23.21 | sqm |
| 3 | Excavation quantity | 34.815 | cum |
| 4 | Survey | 0.5 | Hour |
| 5 | Excavation time | 2 | Hour |
|  | Mucking | 0.5 | Hour |
| 6 | Scaling | 0.5 | Hour |
| 7 | Shotcreting | 1 | Hour |
| 9 | Rib erection | 2 | Hour |
| 10 | Lagging fixing | 1 | Hour |
| 11 | Backfill concreting | 1 | Hour |
|  | Total cycle time for 1.5 m pull length | 8.5 | Hour |
|  | Total cycle time for 3m pull length | 17 | Hour |

Time Schedule:
Among the total excavation $90 \%$ is considered as without rib supporting and $10 \%$ as with rib supporting

Weighted average cycle time $=(4.0 \times 0.9)+(17 \times 0.1)=5.3$ hours per 3 m pull length

Progress per month $=\frac{26(\text { working day per month }) \times 22(\text { working hours per day }) \times 3 \mathrm{~m}(\text { pull length })}{5.3(\text { Hour per } 3 \mathrm{~m} \text { pull })}$
$=324 \mathrm{~m}$ per month

Time required for completion of Benching work $=\frac{\text { Length of Tail Race Tunnel }}{\text { Work progress per month }}$
$=\frac{(502+490+475+460=1927) \mathrm{m}}{(324 \mathrm{~m} \text { per month })}$
$=6.0$ month $=180$ days

Table 3.69 Activities duration for different rock conditions in TRT - 1

| TRT - 1 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 22 | 87 | 22 | 14 | 145 |
| Benching | 7 | 28 | 7 | 7 | 49 |
| Kerb | 7 | 27 | 7 | 5 | 46 |
| Overt | 7 | 27 | 7 | 5 | 46 |
| Invert | 10 | 40 | 10 | 7 | 67 |

Table 3.70 Activities duration for different rock conditions in TRT - 2

| TRT - 2 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 21 | 85 | 21 | 14 | 141 |
| Benching | 7 | 27 | 7 | 4 | 45 |
| Kerb | 7 | 27 | 7 | 4 | 45 |
| Overt | 7 | 27 | 7 | 4 | 45 |
| Invert | 10 | 38 | 10 | 6 | 64 |

Table 3.71 Activities duration for different rock conditions in TRT - 3

| TRT - 3 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 21 | 83 | 21 | 14 | 139 |
| Benching | 6 | 26 | 6 | 4 | 42 |
| Kerb | 6 | 26 | 6 | 4 | 42 |
| Overt | 6 | 26 | 6 | 4 | 42 |
| Invert | 9 | 37 | 9 | 6 | 61 |

Table 3.72 Activities duration for different rock conditions in TRT - 4

| TRT - 4 | Good Rock | Fair Rock | Poor Rock | Very Poor <br> Rock | Total <br> Days |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Heading | 21 | 80 | 21 | 13 | 133 |
| Benching | 6 | 25 | 6 | 4 | 41 |
| Kerb | 6 | 25 | 6 | 4 | 41 |
| Overt | 6 | 25 | 6 | 4 | 41 |
| Invert | 9 | 36 | 9 | 6 | 60 |

Table 3.73 Activities duration of TRT in case of Roadheader



Fig 3.13 Network diagram of Tailrace tunnel in case of Roadheader

### 3.61 Cost estimation of diversion tunnel for Mechanical method

ITEM: Excavation for tunnel in the case of Diversion Tunnel by heading and benching.

| DATA Size of tunnel (finished section) | 12.345 m dia |
| :--- | :---: |
| Length of DT- 1 | 472 m |
| Length of DT- 2 | 552 m |
| Thickness of lining | 1.0 m |
| Diameter of tunnel upto pay line for excavation | 12.345 m |
| Consideration for 3 m pull length |  |
| Heading portion | $82.6734 \mathrm{~m}^{2}$ |
| Area of excavation upto payline |  |


| Benching portion |  |
| :--- | :---: |
| Area of excavation upto payline $\quad(24 \times 4+32 \times 5=256 \mathrm{~m})$ | $40.2379 \mathrm{~m}^{2}$ |
| Total depth of drilling $\quad \mathbf{( 8 2 . 6 7 + 4 0 . 2 3 ) \times \mathbf { 3 . 0 }}$ | $\mathbf{3 6 9} \mathbf{m}^{\mathbf{3}}$ |
| Quantity of in-situ excavation per cycle <br> $=(\mathbf{1 2 3} \times \mathbf{3 . 0})$ |  |

## RATE ANALYSIS

## A.MATERIALS

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Use rate of drill rod 2.0 m long | Rm | 256 | 47.83 | 12244.48 |
|  | Reconditioning charges @ $10 \%$ |  |  |  | 1224.448 |
| 2 | Use rate of air hose | Hour | 32 | 6.25 | 200 |
| 3 | Use rate of water hose | Hour | 32 | 5.78 | 184.96 |
| 4 | Sundries (paint / template etc ) | LS | 9 | 44 | 396 |
|  |  |  |  | Total | 14249.888 |


| Add for small Tools and Plants | @ 1 | 142.498 |
| :--- | :--- | :---: |
| Add for Contractor's Profit | @ $10 \%$ | 1424.988 |
| Add for Contractor's Overheads | $@ 5 \%$ | 712.494 |
| Total cost of Material |  | $\mathbf{1 6 3 8 7 . 3 7}$ |

## B.MACHINERY

| S.N | Description | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Roadheader machine | Per day | 4 | 31333.333 | 125333.332 |
|  | Fuel charges | Hour | 8 | 41 | 328 |
| 2 | Drilling jumbo | Hour | 9 | 370 | 3330 |
|  | Fuel charges | Hour | 9 | 41 | 369 |
| 3 | Convey mucker | Hour | 7 | 740 | 5180 |
|  | Fuel charges | Hour | 7 | 223 | 1561 |
| 4 | Dumper ( $2 \times 6.5$ hrs $)$ | Hour | 13 | 548 | 7124 |
|  | Fuel charges | Hour | 13 | 381 | 4953 |
| 5 | Pump 10 hp | Hour | 8 | 5 | 40 |
|  | Fuel charges |  | 8 | 64 | 512 |
|  |  |  |  | Total | 148730.332 |


| Add for small Tools and Plants | @ $1 \%$ | 1487.303 |
| :--- | :--- | :--- |


| Add for Contractor's Profit | $@$ @ $10 \%$ | 14873.033 |
| :--- | :--- | :---: |
| Add for Contractor's Overheads | $@$, $\%$ | 7436.516 |
| Total hire charges of Machinery |  | $\mathbf{1 7 2 5 2 7 . 1 8 4}$ |

## C.LABOUR

| S.N | Description | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Crew for Roadheader | Hour | 9 | 1200 | 10800 |
| 2 | Crew for Drilling jumbo | Hour | 8 | 101 | 808 |
| 3 | Crew for Convey mucker | Hour | 7 | 101 | 707 |
| 4 | Crew for Dumper | Hour | 13 | 121 | 1573 |
| 5 | Crew for Pump | Hour | 8 | 45 | 360 |
| 6 | Foreman | Day | 1 | 276.73 | 276.73 |
| 7 | Maistry 1 in each shift | Day | 3 | 243.23 | 729.69 |
| 8 | for pushing muck in heading portion | Day | 4 | 241.23 | 964.92 |
| 9 | for mucking shift 4 Nos | Day | 4 | 241.23 | 964.92 |
| 10 | Heavy mazdoor |  |  |  |  |
|  | for mucking shift 8 Nos | Day | 8 | 238.73 | 1909.84 |
| 11 | for other 2 shifts 2 No each shift | Day | 4 | 238.73 | 954.92 |
| 12 | Light mazdoor |  |  |  |  |
|  | for cleaning \& miscellaneous | Day | 3 | 238.23 | 714.69 |
|  |  |  |  | Total | 20763.71 |


| Add for small Tools and Plants | @ $1 \%$ | 207.637 |
| :--- | :--- | :--- |
| Add for Contractor's Profit | @ $10 \%$ | 2076.371 |
| Add for hidden cost on Labour | @ $15 \%$ | 3114.556 |
| Add for additional hidden cost on labour | @ $10 \%$ | 2076.371 |
| Add for Contractor's Overheads | @ $5 \%$ | 1038.185 |
| Total cost of labour |  | $\mathbf{2 9 2 7 6 . 8 3}$ |

### 3.62 Abstract of cost details for 3m Pull length in Diversion tunnel for Mechanical method

| A.Cost of Materials | 16387.37 |
| :--- | :---: |
| B.Hire charges of Machinery | 172527.184 |
| C.Cost of Labour | 29276.83 |
| TOTAL | $\mathbf{2 1 8 1 9 1 . 3 8 4}$ |
| Add for Air and Water line | 1745.531 |
| Add for Ventilation $0.80 \%$ | 13091.483 |
| Add for Lighting | @ $6.0 \%$ |
| Add for Electrical sub-station / Demand charges @ $3.80 \%$ | 3927.444 |
| Add for other Enabling works | 8291.272 |


| Total cost for $369 \mathrm{~m}^{3}$ | 248956.367 |
| :--- | :---: |
| Rate per $\boldsymbol{m}^{\mathbf{3}}$ | $\mathbf{6 7 4 . 6 7 8}$ |


| For 1 cycle (3 m pull length) rate per $\mathrm{m}^{3}$ | $\mathbf{6 7 4 . 6 7 8}$ |
| :--- | :---: |
| Total length of DT- 1 | 472 m |
| Total length of DT- 2 | 552 m |
| $90 \%$ considered without rib support |  |
| Total length in case of without rib support in DT -1 | 424.8 m |
| Total length in case of without rib support in DT -2 | 496.8 m |
| Total cost in DT $-1 \quad\left(674.678 \times 424.8 \mathrm{~m} \times 123 \mathrm{~m}^{2}\right)$ | $\mathbf{3 5 2 5 2 1 9 5 . 3 7}$ |
| Total cost in DT $-2 \quad\left(674.678 \times 496.8 \mathrm{~m} \times 123 \mathrm{~m}^{2}\right)$ | $\mathbf{4 1 2 2 7 1 4 3 . 7 4}$ |

## Consideration for 1.5 m pull length:

| Heading portion |  |
| :--- | :---: |
| Area of excavation upto payline | $82.6734 \mathrm{~m}^{2}$ |
| Benching portion |  |
| Area of excavation upto payline $\quad \mathbf{( 2 4 \times \mathbf { 4 } + \mathbf { 3 2 } \times \mathbf { 5 } = \mathbf { 2 5 6 } )}$ | $40.2379 \mathrm{~m}^{2}$ |
| Total depth of drilling $\quad(82.67+40.23=123)$ | $\mathbf{2 7 0 . 1} \mathbf{~ m}$ |
| Total area of excavation $\quad 123 \mathrm{~m}^{2}$ |  |
| Depth of pull per blast forl.0 m deep holes | 1.5 m |
| Quantity of in-situ excavation per cycle $\quad \mathbf{( 1 2 3} \times \mathbf{1 . 5})$ | $\mathbf{1 8 4 . 5} \mathbf{m}^{\mathbf{3}}$ |

## RATE ANALYSIS: <br> UNIT <br> : $184.5 \mathrm{~m}^{\mathbf{3}}$

### 3.63 Abstract of cost details for 1.5m Pull length in Diversion tunnel for Mechanical method

| A.Cost of Materials | 16387.37 |
| :--- | :---: |
| B.Hire charges of Machinery | 172527.184 |
| C.Cost of Labour | 29276.83 |
| TOTAL | $\mathbf{2 1 8 1 9 1 . 3 8 4}$ |
| Add for Air and Water line $@$ @ $0.80 \%$ | 1745.531 |
| Add for Ventilation $6.0 \%$ | 13091.483 |
| Add for Lighting | 3927.444 |
| Add for Electrical sub-station $/$ Demand charges @ $3.80 \%$ | 8291.272 |
| Add for other Enabling works | @ $1.70 \%$ |
| Total cost for $\mathbf{1 8 4 . 5} \mathbf{m}^{\mathbf{3}}$ | 3709.253 |
| Rate per $\mathbf{m}^{\mathbf{3}}$ | $\mathbf{2 4 8 9 5 6 . 3 6 7}$ |


| Total length of DT- 1 | 472 m |
| :--- | :--- |
| Total length of DT- 2 | 552 m |
| $\mathbf{1 0}$ \% considered with rib support |  |
| Total length in case of with rib support | 47.2 m |
| Total length in case of with rib support $\quad\left(1349.357 \times 47.2 \mathrm{~m} \times 123 \mathrm{~m}^{2}\right)$ | 55.2 m |
| Total cost in DT - $\quad\left(1349.357 \times 55.2 \mathrm{~m} \times 123 \mathrm{~m}^{2}\right)$ | $\mathbf{7 8 3 3 8 2 6 . 9 9 9}$ |
| Total cost in DT - $2 \quad \mathbf{9 1 6 1 5 9 4 . 2 8}$ |  |
| Total cost in Excavation for DT- $\quad(35252195.37+7833826.999)$ | $\mathbf{4 3 0 8 6 0 2 2 . 3 7}$ |
| Total cost in Excavation for DT- $2 \quad(41227143.74+9161594.28)$ | $\mathbf{5 0 3 8 8 7 3 8 . 0 2}$ |

Total cost for Rock bolt support work in DT - 1 (Good \& Fair Rock + Poor \& Very Poor Rock):

Total cost for Rock bolt support work in DT- 1 (3009034.353+1195750.078): 4204784.431

Total cost for Rock bolt support work in DT - 2 (Good \& Fair Rock + Poor \& V. Poor Rock):

Total cost for Rock bolt support work in DT - 2 (3672123.261+1619672.361): 5291795.622

Total cost for Kerb and Invert Lining in DT $-1(4+4+3.1)=11.1 \mathrm{~m}^{2} \times 472 \mathrm{~m} \times 6326$ $=33143179.2$

Total cost for Kerb and Invert Lining in DT $-2(4+4+3.1)=11.1 \mathrm{~m}^{2} \times 552 \mathrm{~m} \times 6326$ $=38760667.2$

Total cost for Overt Lining in DT - $1\left(16.54 \mathrm{~m}^{2}\right) \times(472 \mathrm{~m}) \times(4813.0117) \quad \mathbf{3 7 5 7 4 6 0 4 . 7 8}$
Total cost for Overt Lining in DT - $2\left(16.54 \mathrm{~m}^{2}\right) \times(552 \mathrm{~m}) \times(4813.0117): \mathbf{4 3 9 4 3 1 8 1 . 8 6}$
Total cost in DT- 1 (Excavation + Rock bolt support + Kerb \& Invert Lining + Overt Lining):
( $90 \%$ without rib support $+10 \%$ with rib support + Good \& Fair rock + Poor \& Very Poor rock + Kerb \& Invert lining + Overt lining):
$(35252195.37+7833826.99+3009034.353+1195750.078+33143179.2+37574604.78)=$
118008590.8

$$
\text { Total cost in DT - } 1
$$

: 118008590.8

Total cost in DT- 2 (Excavation + Rock bolt support + Kerb \& Invert Lining + Overt Lining):
( $90 \%$ without rib support $+10 \%$ with rib support + Good \& Fair rock + Poor \& Very Poor rock + Kerb \& Invert lining + Overt lining):
$(41227143.74+9161594.28+3672123.261+1619672.361+38760667.2+43943181.86)$
$=138384382.7$

Total cost in DT- 2
: 138384382.7
Total cost in Diversion Tunnel (118008590+138384382) :256392974

### 3.64 Cost estimation of Pressure shaft for Mechanical method

ITEM: Excavation for tunnel in the case of Pressure Shaft Tunnel by heading and benching.

| DATA Size of tunnel assumed (finished section) | 7.645 m dia |
| :---: | :---: |
| Length of Pressure Shaft ( $211+197+184+172) \mathrm{m}$ | 764 m |
| Thickness of lining | 0.70 m |
| Diameter of tunnel upto pay line for excavation | 7.645 m |
| Consideration for 3 m pull length |  |
| Heading portion |  |
| Area of excavation upto payline | $34.0369 \mathrm{~m}^{2}$ |
| Benching portion |  |
| Area of excavation upto payline | $13.8665 \mathrm{~m}^{2}$ |
| Total depth of drilling for Rock bolt $\quad(17 \times 4+22 \times 5=178 \mathrm{~m})$ | 178 m |
| $\left.\begin{array}{lccccc}\hline \text { Quantity } & \text { of } & \text { in-situ } \\ (34.0369+13.8665=47.9034 \times 3.0)\end{array}\right) ~$ excavation $\quad$ per $\quad$ cycle | $143.7102 \mathrm{~m}^{3}$ |

## A.MATERIALS:

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Use rate of drill rod 2.0 m long | Rm | 178 | 47.83 | 8513.74 |
|  | Reconditioning charges @ $10 \%$ |  |  |  | 851.374 |
| 2 | Use rate of air hose | Hour | 32 | 6.25 | 200 |
| 3 | Use rate of water hose | Hour | 32 | 5.78 | 184.96 |
| 4 | Sundries (paint / template etc ) | LS | 9 | 44 | 396 |
|  |  |  |  | Total | 10146.074 |


| Add for small Tools and Plants | @ 1 | 101.460 |
| :--- | :--- | :---: |
| Add for Contractor's Profit | @ $10 \%$ | 1014.607 |
| Add for Contractor's Overheads | $@ 5 \%$ | 507.303 |
| Total cost of Material |  | $\mathbf{1 1 6 6 7 . 9 8 4}$ |

### 3.64.1 Abstract of cost details for 3m Pull length of Pressure shaft for Mechanical method

| A.Cost of Materials | 11667.984 |
| :--- | :---: |
| B.Hire charges of Machinery | 172527.184 |
| C.Cost of Labour | 29276.83 |
| TOTAL | $\mathbf{2 1 3 4 7 1 . 9 9 8}$ |
| Add for Air and Water line | @ $0.80 \%$ |
| Add for Ventilation | @ $6.0 \%$ |
| Add for Lighting | $1.80 \%$ |
| Add for Electrical sub-station $/$ Demand charges @ $3.80 \%$ | 12808.775 |
| Add for other Enabling works | @ $1.70 \%$ |
| Total cost for $\mathbf{1 4 3 . 7 1 0 2} \mathbf{m}^{\mathbf{3}}$ | 8842.495 |
| Rate per $\mathbf{m}^{\mathbf{3}}$ | 311.935 |


| For 1 cycle (3 m pull length) rate per $\mathrm{m}^{3}$ | $\mathbf{1 6 9 4 . 8 8 0}$ |
| :--- | :--- |
| Total length of DT of Pressure Shaft $(211+197+184+172=764 \mathrm{~m})$ | 764 m |
| $90 \%$ considered without rib support |  |
| Total length in case of without rib support in Pressure Shaft | 687.6 m |
| Total cost in Pressure Shaft $\quad\left(1694.880 \times 687.6 \mathrm{~m} \times 47.9034 \mathrm{~m}^{2}\right)$ | $\mathbf{5 5 8 2 6 5 9 7 . 8 3}$ |

## Consideration for 1.5 m pull length:

| Heading portion |  |
| :--- | :--- |
| Area of excavation upto payline | $34.0369 \mathrm{~m}^{2}$ |


| Benching portion |  |
| :--- | :--- |
| Area of excavation upto payline $\quad(\mathbf{1 7} \times \mathbf{4}+\mathbf{2 2} \times \mathbf{5}=\mathbf{1 7 8 )}$ | $13.8665 \mathrm{~m}^{2}$ |
| Total depth of drilling $\quad(34.0369+13.8665=47.9043)$ | $\mathbf{1 7 8 . 0} \mathbf{~ m}$ |
| Total area of excavation | $17.9043 \mathrm{~m}^{2}$ |
| Depth of pull per blast for1.0 m deep holes |  |
| Quantity of in-situ excavation per cycle $\quad \mathbf{( 4 7 . 9 0 4 3} \times \mathbf{1 . 5})$ | $\mathbf{7 1 . 8 5 6} \mathbf{~ m}^{\mathbf{3}}$ |

RATE ANALYSIS:

### 3.64.2 Abstract of cost details for 1.5 m Pull length of Pressure shaft for Mechanical method

| A.Cost of Materials | 11667.984 |
| :---: | :---: |
| B. Hire charges of Machinery | 172527.184 |
| C.Cost of Labour | 29276.83 |
| TOTAL | 213471.998 |
| Add for Air and Water line @ $0.80 \%$ | 1745.531 |
| Add for Ventilation @ 6.0 \% | 13091.483 |
| Add for Lighting @ 1.80 \% | 3927.444 |
| Add for Electrical sub-station / Demand charges @ 3.80 \% | 8291.272 |
| Add for other Enabling works @ 1.70 \% | 3709.253 |
| Total cost for 71.856 m $^{3}$ | 243571.545 |
| Rate per $\mathrm{m}^{3}$ | 3389.717 |


| For 1 cycle ( 1.5 m pull length) rate per $\mathrm{m}^{3}$ | $\mathbf{3 3 8 9 . 7 1 7}$ |
| :--- | :--- |
| Total length of Pressure Shaft | $\mathbf{7 6 4} \mathbf{~ m}$ |
| $10 \%$ considered with rib support |  |
| Total length in case of with rib support | 76.4 m |
| Total cost in Pressure Shaft $\left(3389.717 \times 76.4 \mathrm{~m} \times 47.9043 \mathrm{~m}^{2}\right)$ | $\mathbf{1 2 4 0 5 9 8 6 . 3 3}$ |
| Total cost in Excavation for Pressure Shaft <br> $(55826597.83+12405986.33)$ | $\mathbf{6 8 2 3 2 5 8 4 . 1 6}$ |

Total cost for Rock bolt support work in Pressure Shafts (Good \& Fair Rock + Poor \& Very Poor Rock):
Total cost for Rock bolt support work in Pressure Shafts (3811461.09+1557667.757)

## $=5369128.847$

Total cost for Kerb and Invert Lining in Pressure Shaft $=\mathbf{1 8 8 4 8 9 4 9 . 6}$

Total cost in Pressure Shaft (Excavation + Rock bolt support + Kerb \& Invert Lining + Overt Lining):
( $90 \%$ without rib support $+10 \%$ with rib support + Good \& Fair rock + Poor \& Very Poor rock + Kerb \& Invert lining + Overt lining):
$(55826597.83+12405986.33+3811461.09+1557667.757+18848949.6+82777936.02)$
$=175228599$

Total cost in Pressure Shaft
$=175228599$

### 3.65 Cost estimation of Tailrace tunnel for Mechanical method

ITEM: Excavation for tunnel in the case of Diversion Tunnel by heading and benching.

| DATASize of tunnel assumed (finished section) | 9.645 m dia |
| :--- | :--- |
| Length of Tailrace Tunnel $(502+490+475+460) \mathrm{m}$ | 1927 m |
| Thickness of lining | 0.70 m |
| Diameter of tunnel upto pay line for excavation | 9.645 m |

## Consideration for $\mathbf{3} \mathbf{m}$ pull length:

| Heading portion |  |
| :---: | :---: |
| Area of excavation upto payline | $52.44 \mathrm{~m}^{2}$ |
| Benching portion |  |
| Area of excavation upto payline | $23.21 \mathrm{~m}^{2}$ |
| Total depth of drilling for Rock bolt work $\quad(20 \times 4+26 \times 5=210) \mathrm{m}$ | 210 m |
| Total area of excavation (52.44+23.21=75.65) | $75.65 \mathrm{~m}^{2}$ |
| Depth of pull per cycle for 2.0 m deep holes | 3.0 m |
| Quantity of in-situ excavation per cycle $\quad \mathbf{( 7 5 . 6 5 \times 3 . 0 )}$ | $226.95 \mathrm{~m}^{3}$ |
| RATE ANALYSIS UNIT | $6.95 \mathrm{~m}^{3}$ |

## A.MATERIALS

| S.N | Perticulars | Unit | Quantity | Rate in INR | Amount in INR |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Use rate of drill rod 2.0 m long | Rm | 210 | 47.83 | 10044.3 |
|  | Reconditioning charges @ | 10\% |  |  |  |
| 2 | Use rate of air hose | Hour | 32 | 6.25 | 1004.43 |
| 2 | Use rate of water hose | Hour | 2 | 5.78 | 11.56 |
| 3 | Usier |  |  |  |  |
| 4 | Sundries ( paint / template etc ) | LS | 9 | 44 | 396 |
|  |  |  |  | Total | 11656.29 |


| Add for small Tools and Plants | @ 1 | 116.562 |
| :--- | :--- | :---: |
| Add for Contractor's Profit | @ $10 \%$ | 1165.629 |
| Add for Contractor's Overheads | @ $5 \%$ | 582.814 |
| Total cost of Material |  | $\mathbf{1 3 5 2 1 . 2 9 5}$ |

### 3.65.1 Abstract of cost details for 3m Pull length of Tailrace tunnel for Mechanical method

| A.Cost of Materials | 13521.295 |
| :--- | :---: |
| B.Hire charges of Machinery | 172527.184 |
| C.Cost of Labour | 29276.83 |
| TOTAL | $\mathbf{2 1 5 3 2 5 . 3 0 9}$ |
| Add for Air and Water line | 1722.602 |
| Add for Ventilation $0.80 \%$ | 12919.518 |
| Add for Lighting | @ $6.0 \%$ |
| Add for Electrical sub-station $/$ Demand charges $1.80 \% 3875.855$ |  |
| Add for other Enabling works $1.80 \%$ | 8182.361 |
| Total cost for $\mathbf{2 2 6 . 9 5} \mathbf{~ m}^{\mathbf{3}}$ | 3660.530 |
| Rate per $\mathbf{m}^{\mathbf{3}}$ | @ |


| For 1 cycle ( 3 m pull length) rate per $\mathrm{m}^{3}$ | $\mathbf{1 0 8 2 . 5 5 6}$ |
| :--- | :--- |
| Total length of Tailrace Tunnel $(502+490+475+460=1927 \mathrm{~m})$ | $\mathbf{1 9 2 7} \mathbf{~ m}$ |
| $90 \%$ considered without rib support |  |
| Total length in case of without rib support in Pressure Shaft | 1734.3 m |
| Total cost in Tailrace Tunnel $\left(1082.556 \times 1734.3 \mathrm{~m} \times 75.65 \mathrm{~m}^{2}\right)$ | $\mathbf{1 4 2 0 3 1 1 2 5 . 3}$ |

## Consideration for 1.5 m pull length:

| Heading portion |  |
| :--- | :--- |
| Area of excavation upto payline | $52.44 \mathrm{~m}^{2}$ |
| Benching portion |  |
| Area of excavation upto payline | $23.21 \mathrm{~m}^{2}$ |
| Total depth of drilling for Rock bolt work $\mathbf{( 2 0 \times 4 + \mathbf { 2 6 } \times \mathbf { 5 } = \mathbf { 2 1 0 } \mathbf { ~ m } )}$ | $\mathbf{2 1 0} \mathbf{~ m}$ |
| Total area of excavation $\quad(52.44+23.21=75.65)$ | $75.65 \mathrm{~m}^{2}$ |
| Depth of pull per blast for1.0 m deep holes | 1.5 m |
| Quantity of in-situ excavation per cycle $\quad \mathbf{( 7 5 . 6 5} \times \mathbf{1 . 5})$ | $\mathbf{1 1 3 . 4 7 5} \mathbf{m}^{\mathbf{3}}$ |

RATE ANALYSIS:

| Total cost for $113.475 \mathrm{~m}^{3}$ | $\mathbf{2 4 5 6 8 6 . 1 7 5}$ |
| :--- | :--- |
| Rate per $\boldsymbol{m}^{3}$ | $\mathbf{2 1 6 5 . 1 1 2}$ |


| For 1 cycle $\left(1.5 \mathrm{~m}\right.$ pull length) rate per $\mathrm{m}^{3}$ | $\mathbf{2 1 6 5 . 1 1 2}$ |
| :--- | :--- |
| Total length of Tailrace Tunnel | $\mathbf{1 9 2 7} \mathbf{~ m}$ |
| $10 \%$ considered with rib support | 192.7 m |
| Total length in case of with rib support | $\mathbf{3 1 5 6 2 4 7 2 . 2 8}$ |
| Total cost in Tailrace Tunnel $\left(2165.112 \times 192.7 \mathrm{~m} \times 75.65 \mathrm{~m}^{2}\right)$ |  |

Total cost in Excavation for Tailrace Tunnel $(142031125.3+31562472.28)=\mathbf{1 7 3 5 9 3 5 9 7 . 6}$
Total cost for Rock bolt support work in Tailrace Tunnel (Good \& Fair Rock + Poor \& Very Poor Rock):

Total cost for Rock bolt support work in Tailrace Tunnel (5358292.472+4638641.566) =9996934.038

Total cost for Kerb and Invert Lining in Tailrace Tunnel $=\mathbf{7 3 1 4 1 2 1 2}$
Total cost for Overt Lining in Pressure Shaft $=\mathbf{1 1 7 8 3 1 7 0 1 . 8}$

Total cost in Tailrace Tunnel (Excavation + Rock bolt support + Kerb \& Invert Lining + Overt Lining):
( $90 \%$ without rib support $+10 \%$ with rib support + Good \& Fair rock + Poor \& Very Poor rock + Kerb \& Invert lining + Overt lining):
$(142031125.3+31562472.28+5358292.472+4638641.566+73141212+117831701.8)=$ 418754362.3

## Total cost in Tailrace Tunnel

: $\mathbf{4 1 8 7 5 4 3 6 2}$

### 3.66 Safety

1. Every Personnel working inside the tunnel shall wear personal protective equipment such as helmets, shoes, gloves and reflective bands etc.
2. In the location of drilling where personnel are employed to higher noise level, noise protection shall be provided.
3. Employees, working in places having an inherent danger of eye or face injury, shall be provided with protection glass, goggles or masks.
4. Stretchers, appliances for artificial breathing, oxygen flask, gas masks etc. shall be available in the front.
5. Fire extinguishers shall be provided at suitable locations in the tunnels where construction activity is carried out.
6. The electrical cables used shall be of waterproof and earthed.
7. Suitable communication system working in underground areas shall be provided for better communication during works.
8. An effective safety program should follow as
9. Planning to avoid hazards.
10. Detection of potential hazards.
11. Timely correction of hazards.
12. Dedication to the protection of the public and the worker.
13. Dedicated safety staff.

## CHAPTER 4

## CONCLUSION AND FUTURE SCOPE

### 4.1Conclusion

4.1.1 Conclusion in Schedule

## By Drill and Blast method

1. Diversion Tunnel requires 223 days to complete the excavation and lining work
2. Pressure Shaft requires 137 days to complete the excavation and lining work
3. Tailrace Tunnel requires 252 days to complete the excavation and lining work

## By Mechanical method

1. Diversion Tunnel requires 249 days to complete the excavation and lining work
2. Pressure Shaft requires 144 days to complete the excavation and lining work
3. Tailrace Tunnel requires 295 days to complete the excavation and lining work

Differences in Days in Tunnels

1. Difference in Diversion Tunnel $=23$ days
2. Difference in Pressure Shaft $=7$ days
3. Difference in Diversion Tunnel $=43$ days

Days comparison of both methods


|  | Diversion Tunnel | Pressure Shaft | Tailrace Tunnel |
| :--- | :---: | :---: | :---: |
| $\square$ Drill and Blast Method | 223 | 137 | 252 |
| $\square$ Mechanical Method | 249 | 144 | 295 |

Fig 4.1 Days comparison of both method adopted
Hence we can clearly say that in Mechanical method more number of days is required with respect to Drill and Blast method.

### 4.1.2 Conclusion in Cost

By Drill and Blast method

1. Cost in Diversion Tunnel $=216119985$
2. Cost in Pressure Shaft $=136415128$
3. Cost in Tailrace Tunnel $=389853586$

## By Mechanical method

1. Cost in Diversion Tunnel $=256392974$
2. Cost in Pressure Shaft $=175228599$
3. Cost in Tailrace Tunnel $=418754362$

## Differences in cost in Tunnels

1. Cost difference in Diversion tunnels $=40272989$
2. Cost difference in Pressure shaft $=38813471$
3. Cost difference in Tailrace tunnels $=28900776$

## Cost comparison of both methods



|  | Diversion Tunnel | Pressure Shaft | Tailrace Tunnel |
| :--- | :---: | :---: | :---: |
| $\square$ Drill and Blast Method | 216119985 | 136415128 | 389853586 |
| $\square$ Mechanical Method | 256392974 | 175228599 | 418754362 |

Fig 4.2 Cost comparison of both method adopted
Hence we can clearly say that in Mechanical method more number of costs is required with respect to Drill and Blast method.

### 4.2 Scope for future work

1. We can perform excavation work in hard strata by other method also like Cut and cover method, TBM method. But there are some restrictions in these methods.
2. Comparisons in the cost can be done in the case of other method adopted. So we can find which method is best suitable and economical.

## REFERENCES

1. Gerhard Girmscheid and Cliff Schexnayder, F.ASCE (2002), "Drill and Blast Tunneling Practices," Practice periodical on structural design and construction, 125-133
2. Roshni Bhoi, Dr. S.M. Ali, (2014), "Potential of Hydro Power Plant in India and its Impact on Environment," International Journal of Engineering Trends and Technology (IJETT), Volume-10, Number-3.
3. Sumit Bhardwaj, Manit Sharma, Sahil Deep Singh Bhau, (2015), "A Review on Baglihar Hydroelectric Project," SSRG International Journal of Civil Engineering (SSRG-IJCE) volume -2, Issue -3
4. M.S.Rahu (2014), "Case Study on Design and Construction of Tunnel," International Journal of Engineering Trends and Technology (IJETT), Volume-13
5. Harmelink D.J, and Rowings J.E. (1998), "Linear Scheduling Model:

Development of Controlling Activity Path," Journal of Construction Engineering and Management, 263-268.
6. Obedait, H. Al-Barqawi, T. Zayed, M. Amer (2006), "Productivity of Tunnel construction Using Road-header," $1^{\text {st }}$ International Construction Specialty Conference.
7. Lei Bei, Bingyu Ren, Denghua Zhong, Lianxing Hu. (2015), "Real-Time Construction Schedule Analysis of Long-Distance Diversion Tunnels Based on Lithological Predictions Using a Markov Process," Journal of Construction Engineering and Management, 141-144
8. Erion Periku, Algest Aha (2015), "Construction Time Analysis For Different Steps In Drill-And-Blast Method Of Hydro Power Tunnel Excavatio," Erion Periku Internaional Journal of Engineering Research and Applications, 95-101.
9. Study of 850 MW Ratle hydro electric project.
10. Project Quality Plan, Issue No 01, HCIIC/PQP/WP11
11. L\&T DRG No. 01202-BE-DIV-EXC-3003 to 3031
12. Schedule of Rates: Tunnel and allied works: for the year: 2014-15

