JAYPEE UNIVERSITY OF INFORMATION TECHNOLOGY, WAKNAGHAT TEST -2 EXAMINATION- 2025

B.Tech-VIII Semester Civil Engineering

COURSE CODE (CREDITS):18B1WCE831 (3)

MAX. MARKS: 25

COURSE NAME: ADVANCED REINFORCED CONCRETE DESIGN

COURSE INSTRUCTORS: Dr. KAUSHAL KUMAR

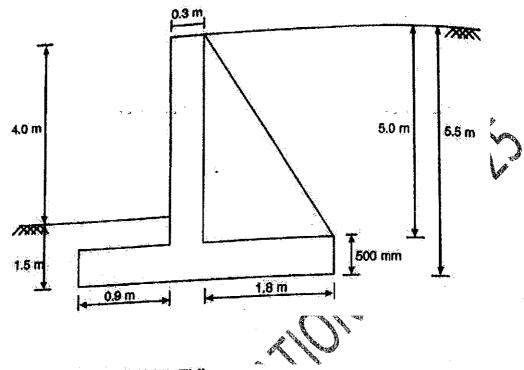
MAX. TIME: 1 Hour 30 Min

Note: (a) All questions are compulsory.

(b) IS 3370:2009 is allowed

Q.No	Question	, co	Marks
Q1	In respect to the design of Retaining walls, what is shear key? How is it designed?	3	3
Q2	Draw a neat sketch of various forces acting on underground water tank.	4	2
Q3	Calculate the forces in a cantilever retaining wall to retain horizontal earthen embankment of height 4 m above the ground level. The earthen backfill is having a density of 18 kN/ml and angle of internal friction as 30°. The safe bearing capacity of the soil is 180 kN/m². The coefficient of friction between soil and concrete is assumed to be 0.45. Use M20 concrete and Fe 415 steel. While designing a counter for retaining wall to retain 4 m earth above ground level. The top of the earth is to be level. The density of earth is 15 kN/m². The angle of internal friction of soil is 30°. The safe bearing capacity of soil is 200 kN/m² and the coefficient of friction between soil and wall is 0.6. The preliminary profile and forces are given in page 2, theck the stability and design the stem.	3	10
Q4	Design a circular tank with flexible base for a tank of 1,00,000 litre tapacity. The depth of water in the tank is 5 m. Use M25 concrete and Re 415 steel. Take unit weight of water as 9.8 kN/m². Permissible tensile stress in steel = 130 MPa & Permissible direct tensile stress in concrete = 1.3 MPa for M25 concrete. OR Design a circular water tank with fixed base, resting on the ground, for a capacity of 500 kl. The depth of water in tank is 5 m and a free board of 200 mm is to be provided. Use M30 concrete and Fe 415 steel. Use IS code method.	4	10

Data for Q3 (b):



Forces Acting on the Retaining Wall

Force (Type)	Force (kN)	Distance from toe edge m	Moment about toe edge (kNm)
1. Overturning force	$\frac{1}{2} \times \left(\frac{1}{3} \times 15 \times 5.5\right) 5.5$	$\frac{H}{3} = \frac{5.5}{3} = 1.833$	138.65
$P_h = \frac{1}{2}(K_a \gamma H)H$	⊭ 75.625		
	$F_S = 75.625 \mathrm{kN}$		$M_0 = 138.65$
2. Restoring forces			
(i) Weight of backfill (W _i)	15 × 5 × 1.8 ≅ 135	$3.0 - \frac{1.8}{2} = 2.1$	283.5
(ii) Weight of stem (W_2)	$0.3 \times 5.0 \times 25 = 37.5$	$0.9 + \frac{0.3}{2} = 0.915$	34:31
III) Weight of base slab (W3)	0.5×3×25 = 37.5	$\frac{3.0}{2} = 1.5$	56.25
	$\Sigma W = 210 \text{ kN}$		$M_R = 374.06 \text{ kN}$

Tension in Circular Ring Wall, Fixed base, Free top and Subjected to Triangular Load

		Coefficient at Point								
農	0.011	0.1#	0.24	0.3 H	0.4#	0.5#	0,617	0711	0.837	
(a)	(2)	(3)	(6)	(5)	(6)	Ø	- (8)	(9)	(10)	
0.4	+0,149	+0.134	+0.120	+0.101	+0.082	+0.066	+0.049	+0,029	+0.014	+0.004
0.8	+0.363	+0.239	+0.215	+0.109	+0.160	+0.130	+0.096	+0.063	+0.034	+0.010
1.2	+0.283	+0.271	+0.254	+0.234	+0,209	+0:180	+0.142	+0.099	+0.054	+0.016
1.6	+0.265	+0.268	+0.268	+0.266	+0.250	+0,226	+0.185	+0.134	+0.075	+0.023
2.0	+0,234	+0.251	+0.273	+0,285	+0.285	+0.274	+0,232	+0.172	+0.104	+0.0.0
3.0	+0.134	+0.203	+0.267	+0.322	+0.357	+0.362	+0,330	+0.262	+0.157	+0.052
4.0	+0.067	+0.164	+0.256	+0.339	+0.403	+0.429	+0.409	+0.334	+0.210	+0.073
5.0	+0.025	+0.137	+0,245	+0.346	+0.428	+0.477	+0.469	+0,398	+0.259	+0.092
6.0	+0.018	+0.119	+0.234	+0.344	+0.441	+0.504	+0.514	+0.447	+0.301	+0.112
8.0	-0.001	+0.104	+0.218	+0.335	+0.443	+0.534	+0.575	+0.530	+0.381	+0.151
10.0	-0.001	+0.098	+0.208	+0.323	+0.437	+0.542	+0.608	+0.589	+0.440	+0.179
12.0	-0.005	+0.097	+0.202	+0.312	+0.429	+0.543	+0.628	+0.633	+0.494	+0.211
14.0	-0.002	+0.098	+0.200	+0.306	+0.420	+0.539	+0.639	+0.666	+0.541	+0.241
16.0	0.000	+0.099	+0.199	+0.304	+0.412	+0.531	+0.641	+0.687	+0.582	+0.265

Moments in Circular Ring Wall, Fixed base, Free top and Subjected to Triangular Load

					coefficient	s at Põhit		a de la composição de l	iren (
H	0.1 <i>H</i>	0.247	03 H ,	0.48	0017		0711	1037		* (V) : . (V			
(1)	Ø	(3)	(4)	(5)	(6)	(7)	(8)	. (9))	(10)				
0.4	+0.0005	+0.0014	+0.0021	+0.0007	-0.0042	-0.0150	-0.0302	-0.0529	-0.0816	-0.1205			
0.8	+0.0011	+0.0037	+0.0063	+0.0080	+0.0070	+0,0023	-0,0068	-0.0024	-0.0465	-0.0795			
1.2	+0.0012	+0.0042	+0.0077	+0.0103	+0.0112	+0.0090	+0.0022	-0.0108	-0.0311	-0.0602			
1:6	+0.0011	+0.0041	+0.0075	+0.0107	+0.0121	+0,0111	+0.0058	-0.0051	-0.0232	-0.0505			
2.0	+0.0010	+0.0035	+0.0068	+0.0099	+0.0120	+0.0115	+0.0075	-0.0021	-0.0185	-0.0436			
3.0	+0.0006	+0.0024	+0.0047	+0.0071	+0.0090	+0.0097	+0.0077	+0.0012	-0.0119	-0.0333			
4.0	+0.0003	+0.0015	+0.0028	+0.0047	+0.0066	+0.0077	+0.0069	+0.0023	-0.0080	-0.0268			
5.0	+0.0002	+0.0008	+0.0016	+0.0029	+0.0046	+0.0059	+0.0059	+0.0028	-0.0058	-0.0222			
6.0	+0.0001	+0.0003	+0.0008	+0.0019	+0.0032	+0.0046	+0.0051	+0.0029	-0.0041	-0.0187			
8.0	0.0000	+0.0001	+0.0002	+0.0008	+0.0016	+0.0028	+0.0038	+0.0029	-0.0022	-0.0146			
10.0	0.0000	0.0000	+0.0001	+0.0004	+0.0007	+0.0019	+0.0029	+0.0028	-0.0012	-0.0122			
12.0	0.0000	+0.0001	+0.0001	+0.0002	+0.0003	+0.0013	+0.0023	+0.0026	-0.0005	-0.0104			
14.0	0.0000	0.0000	0.0000	0.0000	+0.0001	+0.0008	+0.0019	+0.0023	0.0001	-0.0090			
16.0	0.0000	0.0000	-0.0001	-0.0002	-0.0001	+0.0004	+0.0013	+0.0019	+0.0001	-0.0079			

Shear at the base of cylindrical section

SECTION WAS PROVIDED	in the second se	Name of the state	以冷静
<u>H</u>	Triangular, load	Triangular on rectai	
1. 27	fixed three	load hinged bas	(2) (2) (2) (2) (3) (4) (4) (4) (5) (5) (5) (6) (6) (6) (6) (6) (6) (6) (6) (6) (6
0.4	+0,436	+0,245	7. 7. (2. 0. 1. (2.)
0.8	+0.374	+0.234	
1.2	+0.339	+0.220	
1.6	+0.317	+0.204	
2.0	+0.299	+0.189	
₹	1.	248 147 (c) (44 50)	
3.0 4.0	+0,262	+0.158	
4.0	+0.236	+0.137	
5.0	+0.213	+0:121	1
6.0	+0.197	+0,110	
8.0	+0.174	+0.096	40 2.74
10.0	+0.158	+0.087	
12.0	40.145	+0.079	
14.0	40.135	+0.073	
16.0	+0.127	+0,068	

Note: +ve sign indicates shear acting inward.